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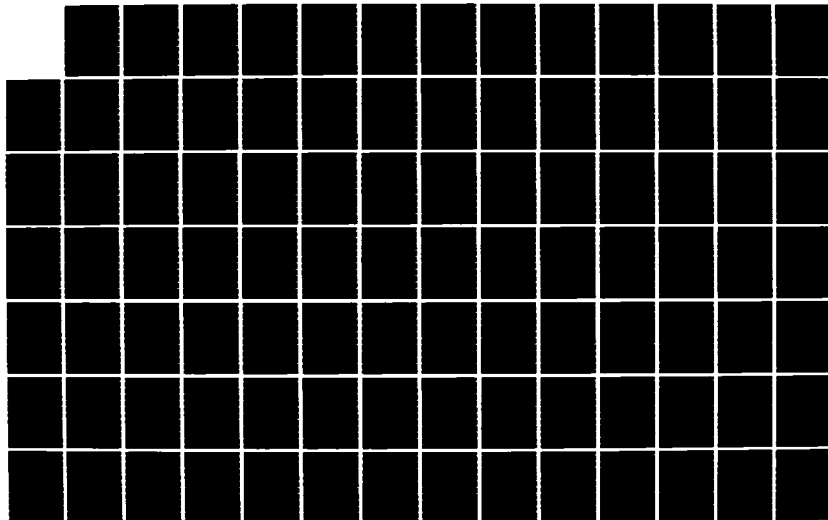
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**DNA-TR-85-312**

## **INFRARED ISSUES FOR THE NUCLEAR WINTER PHENOMENON**

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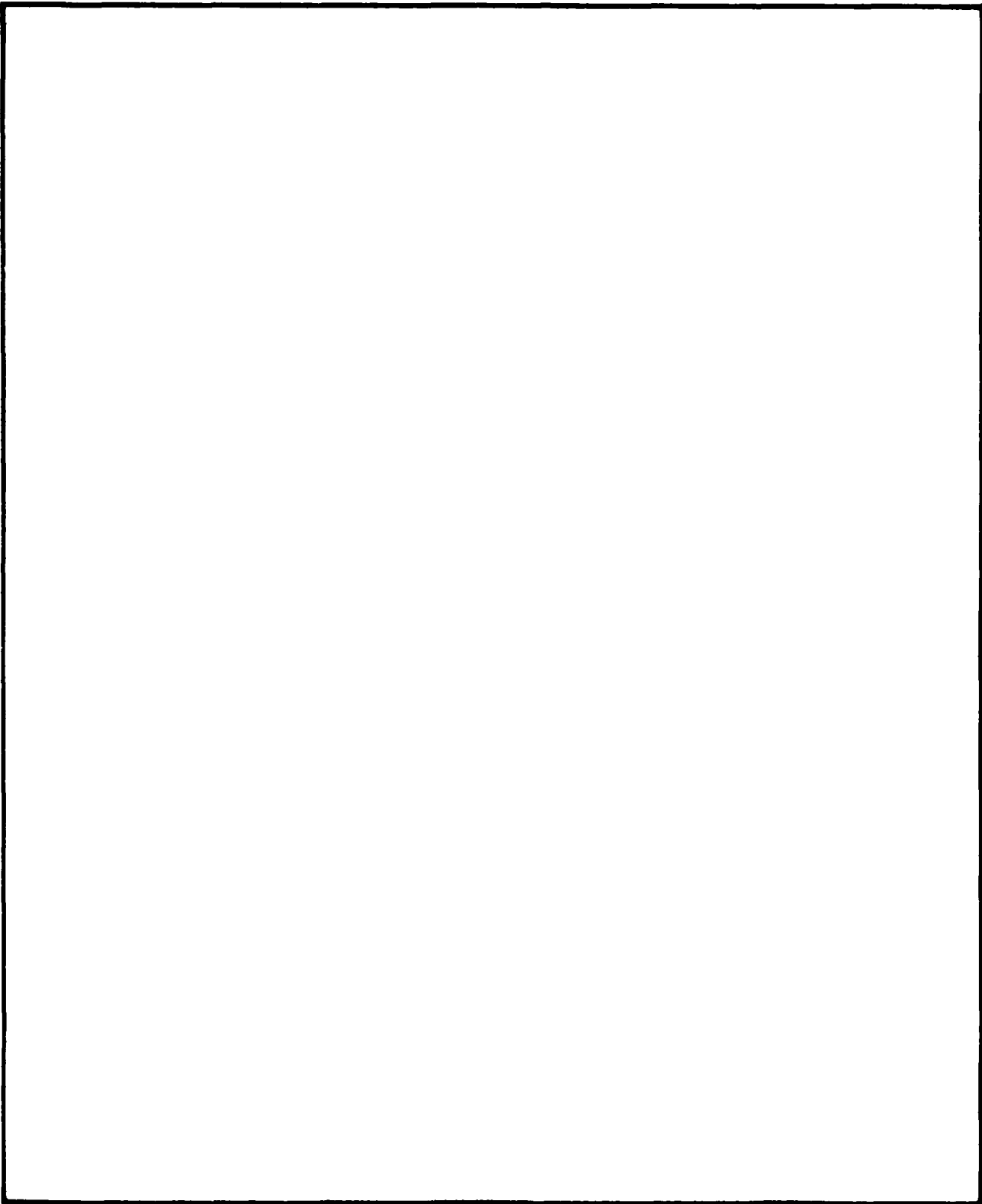
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19 ABSTRACT (Continue on reverse if necessary and identify by block number) Simple models of the nuclear winter phenomenon are used to study the possibility that the infrared radiators: hydrocarbons, CO <sub>2</sub> , NO <sub>2</sub> , H <sub>2</sub> O or condensed water (clouds), might have important effects. Most of these substances are found to be unimportant but water clouds, if they are present and it appears they might be, are found to be of great potential significance.			
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# CONVERSION TABLE

Conversion factors for U.S. customary  
to metric (SI) units of measurement.

To Convert From	To	Multiply By
angstrom	meters (m)	1.000 000 X E -10
atmosphere (normal)	kilo pascal (kPa)	1 013 25 X E +2
bar	kilo pascal (kPa)	1.000 000 X E +2
barn	meter <sup>2</sup> (m <sup>2</sup> )	1.000 000 X E -28
British thermal unit (thermochemical)	joule (J)	1.054 350 X E +3
calorie (thermochemical)	joule (J)	4.184 000
cal (thermochemical)/cm <sup>2</sup>	mega joule/m <sup>2</sup> (MJ/m <sup>2</sup> )	4.184 000 X E -2
curie	*giga becquerel (GBq)	3.700 000 X E +1
degree (angle)	radian (rad)	1.745 329 X E -2
degree Fahrenheit	degree kelvin (K)	$T_K = (T_F + 459.67)/1.8$
electron volt	joule (J)	1.602 19 X E -19
erg	joule (J)	1.000 000 X E -7
erg/second	watt (W)	1.000 000 X E -7
foot	meter (m)	3.048 000 X E -1
foot-pound-force	joule (J)	1.355 818
gallon (U.S. liquid)	meter <sup>3</sup> (m <sup>3</sup> )	3.785 412 X E -3
inch	meter (m)	2.540 000 X E -2
jerk	joule (J)	1.000 000 X E +9
joule/kilogram (J/kg) (radiation dose absorbed)	Gray (Gy)	1.000 000
kilotons	terajoules	4.183
kip (1000 lbf)	newton (N)	4.448 222 X E +3
kip/inch <sup>2</sup> (ksi)	kilo pascal (kPa)	6.894 757 X E +3
ktap	newton-second/m <sup>2</sup> (N-s/m <sup>2</sup> )	1.000 000 X E -2
micron	meter (m)	1.000 000 X E -6
mil	meter (m)	2.540 000 X E -5
mile (international)	meter (m)	1.609 344 X E +3
ounce	kilogram (kg)	2.834 952 X E -2
pound-force (lbf) (avoirdupois)	newton (N)	4.448 222
pound-force/inch	newton-meter (N-m)	1.129 848 X E -1
pound-force/inch <sup>2</sup>	newton-meter (N/m)	1.751 268 X E +2
pound-force/foot <sup>2</sup>	kilo pascal (kPa)	1.758 026 X E +2
pound-force/inch <sup>2</sup> (psi)	kilo pascal (kPa)	6.894 757
pound-mass (lbm) (avoirdupois)	kilogram (kg)	4.535 924 X E -1
pound-mass-foot <sup>2</sup> /moment of inertia	kilogram-meter <sup>2</sup> (kg-m <sup>2</sup> )	4.213 011 X E -2
pound-mass-foot <sup>3</sup>	kilogram-meter <sup>3</sup> (kg-m <sup>3</sup> )	1.601 846 X E +1
rad (radiation dose absorbed)	*Gray (Gy)	1.000 000 X E -2
roentgen	coulomb/kilogram (C/kg)	2.579 760 X E -1
shake	second (s)	1.000 000 X E -12
slug	kilogram (kg)	1.459 380 X E +1
torr (mm Hg, 0°C)	kilo pascal (kPa)	1.333 22 X E -1

\*1 Bq = 1 event/s  
\*\*1 Gy or 100 rads is the SI unit of absorbed radiation.



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## SECTION 1

### INTRODUCTION

In this report we shall use simple models to study the phenomenon which has come to be known as nuclear winter<sup>1</sup>. The models are time-independent, one-dimensional and allow solution in terms of closed form, analytic expressions. In view of the fact that time-dependent, multi-dimensional calculations of the phenomenon have been presented<sup>1</sup>, it is perhaps appropriate to motivate the use of the much simpler models. The models have several uses: 1) they allow one to develop an understanding of the phenomenon at a more fundamental level than may be possible with the use of large, complex computer simulations; 2) they allow one to examine the parameter space of the problem or to examine the importance of including a particular type of phenomenon in the calculations. Usually a simple inspection of the formulas will reveal the sensitivity to a parameter value or type of effect, at most a simple calculation will suffice. In this way they can point to interesting regions of the parameter space where more detailed calculations should be done or to the most important additions to make in improving the more complicated calculations; 3) the models and the physical intuition they allow one to develop are useful in developing "sub-grid" models: formulas which specify in large scale simulation codes the results of processes at scales smaller than the code can resolve.

The main use we shall make of the models in this report - the purpose for which we developed them - is to study the effects of infrared radiation, IR, on the nuclear winter phenomenon. In particular we shall consider whether or not the presence of such IR radiators as hydrocarbons,

NO<sub>2</sub>, CO<sub>2</sub>, water vapor or condensed water (clouds) can be of importance to the phenomenon and to consider the sensitivity of the phenomenon to reasonable variation in the IR properties of soot itself. We find that hydrocarbons, NO<sub>2</sub> and CO<sub>2</sub> are not of importance; this result is in agreement with the conclusions of other workers. Water vapor is unlikely to be of more than marginal importance to the temperature structure if one ignores convective instabilities; it may be of importance in determining the stability characteristics at the top of the soot layer. Variation in the IR properties of the soot itself across the range of reasonable expectation makes a significant difference in the results. Condensed water, if it is present, can play a significant, indeed a dominant, role in the phenomenon.

A water cloud mixed with the soot will alter the entire character of the temperature profile, changing it from one in which the temperature is hot at the top of the layer and cold at the earth's surface - as shown in previous calculations of the nuclear winter phenomenon and as shown in our calculations in the absence of condensed water - to one in which the temperature is cold at the top of the cloud-soot layer and hot at the earth's surface. Furthermore the clouds can be created by the amounts of water which are likely to be present. The question of whether or not there will be clouds is complicated. There exists a strong hysteresis effect: if the cloud is there it keeps the top of the layer cold which keeps the cloud there; if the cloud is not there the top of the layer is hot which keeps a cloud from forming. Most fire plumes are initially capped with condensation clouds<sup>2</sup>.

If the clouds persist for long periods of time they will almost certainly have a profound effect on the nuclear winter phenomenon. They will also affect the dynamics of the phenomenon at early times when the various individual plumes, some of which will probably have condensation clouds, some of which may not have condensation clouds, combine to form

the hemisphere-wide soot layer of nuclear winter. Even if the condensation clouds disappear before the late times their effects on the dynamics of the combining phase may have implications for removal rates of the soot and for the later location of the material. In turn, it is the outcome of these mixing processes, which the clouds will influence, which will determine whether or not there will be clouds at late times. Until careful calculations which include the effects of the clouds are made we do not believe that any calculation of the nuclear winter phenomenon can be completely credible: the presence of condensation clouds, which we have not been able to rule out, would alter the entire character of the event.

We also point out that the nuclear winter phenomenon is always warming over snowpack. This fact may influence global circulation patterns or may be important in other regards. The analysis of whether the warming effect over snowpack is of importance to the total phenomenon is beyond the scope of the present report.

The report is organized as follows: In Section 2 we document the data we found necessary to accumulate in order to specify the parameters or ranges for parameters in the model calculations. Much of this data was gleaned from other sources; some represent calculations we made ourselves. In Section 3 we present the model calculations - the main results of the study. The models are described in order of increasing complexity, first ignoring convective instabilities then including their effects in an approximate way. Concluding remarks are given in Section 4 and in Appendix E we make some remarks on calculating the development of the unstable interface at the top of the soot layer when no condensation cloud is present.



## SECTION 2

### GASEOUS AND PARTICULATE MATTER INJECTED INTO ATMOSPHERE BY MASSIVE BURNING, AND THEIR OPTICAL PROPERTIES

#### PRELIMINARY

One purpose of the present study is to investigate the possible amelioration of the predicted "nuclear winter" effects at the earth's surface by polyatomic molecules, injected into the atmosphere following massive burning, that might inhibit the escape to space of thermal radiation. For this purpose, we first performed a literature survey to determine the principal gaseous species produced by the burning, and to obtain estimates of the quantity of each injected. We then sought to determine, using band models and parameters from the literature where possible, the broad-band infrared (IR) emissivity and transmissivity for each of the species.

As a further aid in performing the work of this contract, we undertook calculations to estimate the broad-band IR emissivity, transmissivity, and reflectivity for particulate layers. These include water clouds, dust layers, soot (carbon) layers, and layers containing a mixture of water droplets and soot. We also performed calculations to determine the corresponding optical properties in the visible ( $0.55 \mu\text{m}$ ) for the same particulate layers.

This section describes the methodology employed in the foregoing studies and presents the results in graphical and tabular form. The results of the literature survey of injected species and their emission

factors are given first. This is followed by the optical properties of the gaseous species and, finally, by the optical properties of the particulate layers.

## MOLECULAR SPECIES INJECTED

A survey of the literature, including References 1 through 5, shows that the principal species injected into the atmosphere, as a consequence of forest and urban fires, are  $\text{CO}_2$ ,  $\text{CO}$ ,  $\text{H}_2\text{O}$ ,  $\text{NO}_x(\text{NO}_2 + \text{NO})$ , and hydrocarbons. A key item for each of the species is the "emission factor," which is the number of grams of the substance emitted per gram of fuel burned. These numbers are by no means unique for each of the species, as different measurements have revealed a range of values. Table 2-1 shows values for the emission factors, the associated references, and values adopted in this report.

There are many hydrocarbons, but we have assumed that they are dominated by six species and proportioned among them as shown in Table 2-2. The corresponding emission factors adopted, based on the total hydrocarbon emission factor and the relative abundances, are also shown in Table 2-2.

In Table 2-3 we compare, data permitting, the species content in the ambient atmosphere ( $30^\circ\text{N} - 70^\circ\text{N}$ ;  $0.88 \pi$  steradians) with the additional amount added from the burning of 4500 Tg fuel ( $1 \text{ Tg} \equiv 10^{12} \text{ g}$ ). This is the "baseline case" considered in Reference 2-1 and corresponds to 3750 Tg consumed in urban fires and 750 Tg in forest fires. The amounts added from the burning are based on the emission factors given in Tables 2-1 and 2-2. In both cases the amounts are given in terms of the total number of molecules and the vertical column number in units of atm cm at NTP. For the ambient atmosphere we have used the following:  $\text{CO}_2$  and  $\text{CO}$  mixing ratios of  $3 \times 10^{-4}$  and  $1.9 \times 10^{-7}$ , respectively, with the

Table 2-1. Emission factors for products of combustion.

Species	Emission Factor	Reference	Emission Factor Adopted
CO <sub>2</sub>	1 — 1.75 1.9 (Ponderosa Pine)	2-2 2-4	1.75
CO	.05 .01 — .25 .01 (Ponderosa Pine)	2-1 2-2 2-4	0.18
H <sub>2</sub> O	.25 — .75	2-2	0.75
NO <sub>x</sub>	$1.5 \times 10^{-3}$ $5 \times 10^{-4}$ — $4.5 \times 10^{-3}$ $4 \times 10^{-4}$ — $3.3 \times 10^{-2}$	2-1 2-2 2-3	$5 \times 10^{-3}$
hydrocarbons (total)	.02 $5 \times 10^{-3}$ — $2 \times 10^{-2}$ $4.5 \times 10^{-3}$ — $6.5 \times 10^{-3}$	2-1 2-2 2-4	$10^{-2}$

Table 2-2. Assumed distribution of hydrocarbons (Reference 2-4).

Species	Relative Abundance (%)	Emission Factor Adopted
CH <sub>4</sub> (methane)	30.8	$3.1 \times 10^{-3}$
C <sub>2</sub> H <sub>4</sub> (ethylene)	25.8	$2.6 \times 10^{-3}$
C <sub>2</sub> H <sub>2</sub> (acetylene)	22.3	$2.2 \times 10^{-3}$
C <sub>3</sub> H <sub>6</sub> (propylene)	7.1	$7.1 \times 10^{-4}$
C <sub>3</sub> H <sub>8</sub> (propane)	7.0	$7.0 \times 10^{-4}$
C <sub>2</sub> H <sub>6</sub> (ethane)	7.0	$7.0 \times 10^{-4}$

Table 2-3. Ambient atmospheric content and additions thereto in "baseline case".

Species	Content in Ambient Atmosphere (30°N-70°N)		Additions from 4500 Ig Fuel Burned (30°N-70°N)	
	Number of Molecules	Vertical Content (atm cm)	Number of Molecules	Vertical Content (atm cm)
CO <sub>2</sub>	$8.8 \times 10^{39}$	$2.9 \times 10^2$	$1.1 \times 10^{38}$	3.6
CO	$5.3 \times 10^{36}$	$1.7 \times 10^{-1}$	$1.7 \times 10^{37}$	$5.6 \times 10^{-1}$
H <sub>2</sub> O	$5.4 \times 10^{40}$	$1.8 \times 10^3$	$1.1 \times 10^{38}$	3.6
NO <sub>x</sub>	$4.9 \times 10^{34}$	$6.3 \times 10^{-4}$	$2.9 \times 10^{35}$ $9.4 \times 10^{35} *$	$9.7 \times 10^{-3}$ $3.1 \times 10^{-2} *$
CH <sub>4</sub>	$3.3 \times 10^{37}$	1.1	$5.2 \times 10^{35}$	$1.7 \times 10^{-2}$
C <sub>2</sub> H <sub>6</sub>	-	-	$2.5 \times 10^{35}$	$8.2 \times 10^{-3}$
C <sub>2</sub> H <sub>2</sub>	-	-	$2.3 \times 10^{35}$	$7.4 \times 10^{-3}$
C <sub>3</sub> H <sub>6</sub>	-	-	$4.6 \times 10^{34}$	$1.5 \times 10^{-3}$
C <sub>3</sub> H <sub>8</sub>	-	-	$4.3 \times 10^{34}$	$1.4 \times 10^{-3}$
C <sub>2</sub> H <sub>4</sub>	-	-	$6.3 \times 10^{34}$	$2.1 \times 10^{-3}$

\* Includes  $6.5 \times 10^{35}$  molecules introduced from fireballs in the baseline case (Ref. 2-1).

total concentration from Reference 2-6; the mid-latitude mean values for  $H_2O$  from Reference 2-6;  $NO_x$  and  $CH_4$  values from References 2-7 and 2-8. The ambient atmospheric content of the hydrocarbons, other than methane, is not readily available to us and so is not included in Table 2-3.

## BROAD-BAND IR PROPERTIES OF MOLECULAR SPECIES

Since thermal radiation from the earth approximates blackbody radiation, we are interested in determining the emission and absorption properties of the injected products of combustion averaged over a Planck spectrum. These average values are called "broad-band" IR properties of the molecules.

The effective radiating temperature of the earth lies between about 200 and 300 °K. At 300 °K the blackbody emission peaks at 10  $\mu m$ ; at 200 °K it peaks at about 15  $\mu m$ . So we are interested mainly in molecules that absorb in the long-wavelength infrared (LWIR) beyond about 6  $\mu m$ . All of the molecules listed in Table 2-3 satisfy this requirement except for CO whose fundamental band lies at about 4.7  $\mu m$ . Thus, although Table 2-3 indicates that massive burning may inject more CO into the atmosphere than is there under ambient conditions, its presence should not alter significantly the transport of thermal radiation through it, and so we delete it from further consideration. We shall also ignore  $CO_2$ . This is because, from Table 2-3, the amount injected by burning is only about 1 percent of the ambient content. With the exception of propylene ( $C_3H_6$ ), for which we could find no band-model data, estimates of the broad-band IR properties of the remaining molecules in Table 2-3 are given below. For  $NO_x$  we will include only  $NO_2$  because very little of the fundamental band of NO at 5.3  $\mu m$  extends into the LWIR region at ambient temperatures.

## NO<sub>2</sub>

The transmission of NO<sub>2</sub> in the  $\nu_2$  and  $\nu_3$  fundamental bands and the  $\nu_1 + \nu_3$  combination band, spanning the wavenumber interval 655 to 2950 cm<sup>-1</sup>, has been modeled by Pierluissi and Tomiyama (Reference 2-9) and can be written in the form

$$T = \exp(-10^{a_1 + a_2 X}) \quad (2-1)$$

where

$$X = c' + \log_{10} W \quad (2-2)$$

and

$$W = \left(\frac{P}{P_0}\right)^n \left(\frac{T_0}{T}\right)^m U \quad (2-3)$$

Here,  $P$  is the total air pressure,  $T$  is the temperature (°K),  $P_0$  and  $T_0$  (273 °K) are the corresponding STP values,  $U$  is the absorber thickness (atm cm),  $a_1$ ,  $a_2$ ,  $n$ ,  $m$  are constants given in Reference 2-1\*, and  $c'$  is tabulated in Reference 2-1 as a function of wavenumber  $\tilde{\nu}$ .

The spectral emissivity at wavenumber  $\tilde{\nu}$  is

$$\epsilon(\tilde{\nu}) = 1 - T(\tilde{\nu}) \quad (2-4)$$

and the broad-band emissivity,  $\bar{\epsilon}$ , is

$$\bar{\epsilon} = \frac{\int_0^{\infty} \epsilon(\tilde{\nu}) B(\tilde{\nu}) d\tilde{\nu}}{\int_0^{\infty} B(\tilde{\nu}) d\tilde{\nu}} \quad (2-5)$$

\* The value of  $a_1$  is erroneously given in Reference 2-1 as -0.25653. The correct value is 1.19711.

Here,  $B(\tilde{\nu})$  is the Planck function

$$B(\tilde{\nu}) = 2hc\tilde{\nu}^3(e^{1.435 \tilde{\nu}/T} - 1)^{-1} \quad . \quad (2-6)$$

We have evaluated  $\bar{\epsilon}$  numerically from Equation 2-5 using Equations 2-1 through 2-4, in which, for the nuclear winter application, we assumed an average  $\text{NO}_2$  layer height of 5 km with  $P = 540.5$  mb and  $T = 256$  °K. The calculations were performed for  $\text{NO}_2$  layer thickness ( $U$ ) ranging from  $10^{-4}$  to  $10^2$  atm cm. The results are shown in Figure 2-1.

For the maximum value of  $U$  for  $\text{NO}_2$  in Table 2-3, that incorporates contributions from fires and nuclear fireballs, the emissivity (Figure 2-1) is seen to be less than about  $6 \times 10^{-3}$ . This corresponds to a transmission of thermal radiation from the earth's surface of at least 99.4 percent.

## $\text{H}_2\text{O}$

The broad-band IR emissivity for water vapor, as reported by Staley and Jurica (Reference 2-10), is shown in Figure 2-2 for two different temperatures. In this figure the path length is in units of  $\text{gm cm}^{-2}$  of water vapor ( $1 \text{ gm cm}^{-2} \equiv 1.2438 \times 10^3 \text{ atm cm}$ ). For an atmospheric water-vapor content of  $1.8 \times 10^3 \text{ atm cm}$  (Table 2-3), corresponding to  $1.45 \text{ gm cm}^{-2}$ , the emissivity is seen to be about 0.63, corresponding to a transmission of thermal radiation of 37 percent. These values are for the ambient atmosphere. However, the additional amount of water vapor injected by the fires ( $3.6 \text{ atm cm}$ ) contributes only insignificant increments to the ambient emissivity and transmissivity.

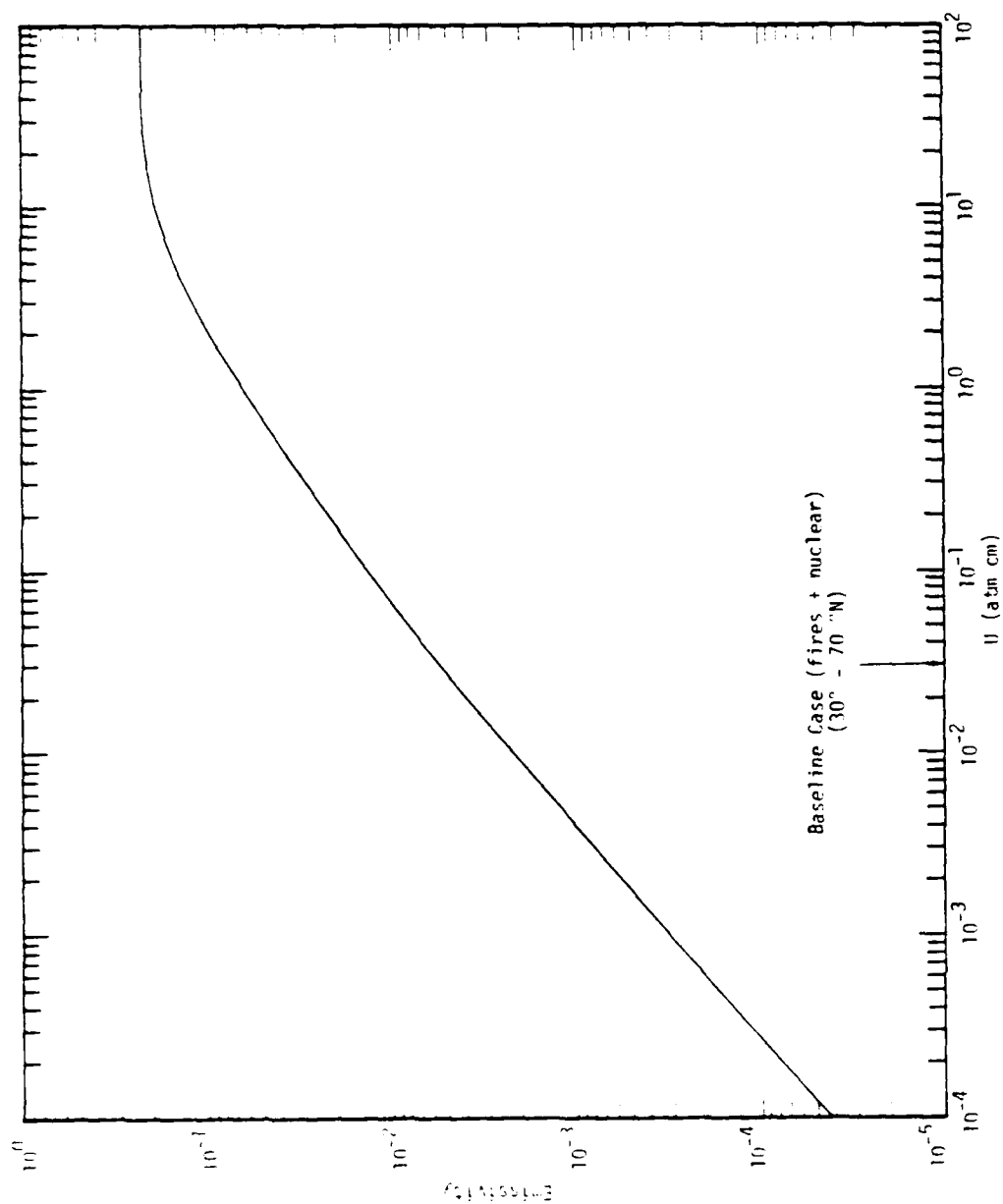


Figure 2-1. Broad-band infrared emissivity of  $\text{NO}_2$ .



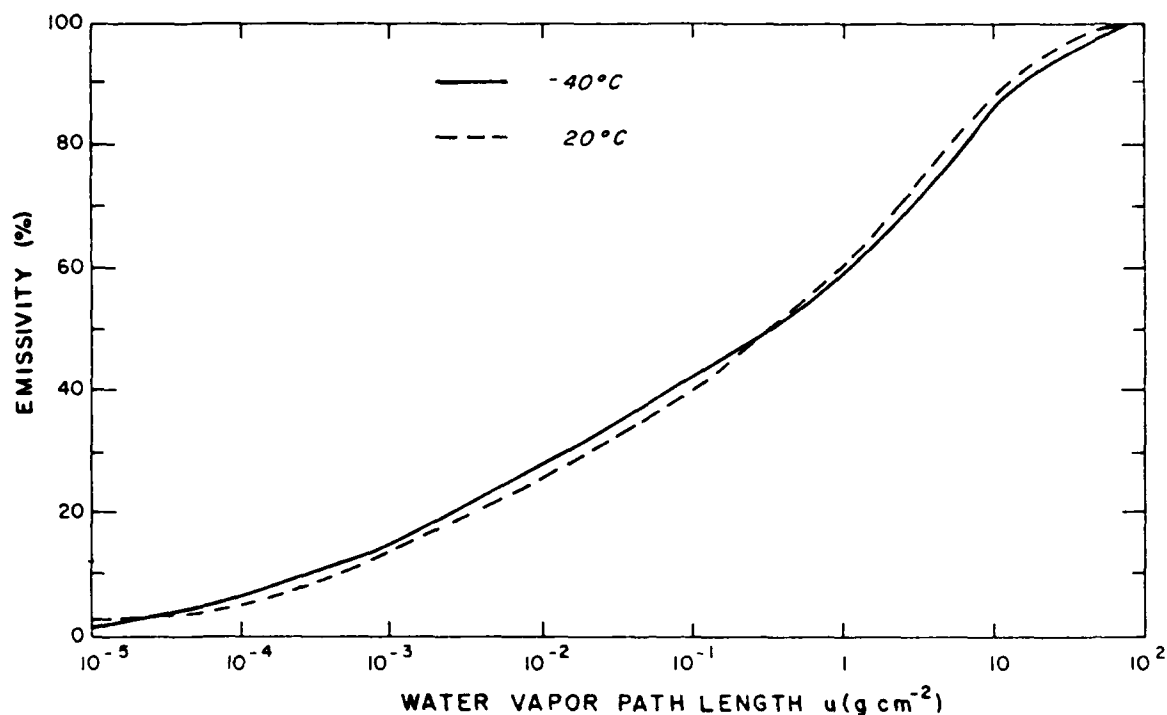


Figure 2-2. Broad-band IR emissivity for water vapor (from Reference 2-10).

### Hydrocarbons

Methane (CH<sub>4</sub>). For methane we use the band model developed by Jarem, et al. (Reference 2-11) which is formally similar to that described above for NO<sub>2</sub>. The transmission at wavenumber  $\tilde{\nu}$  is given by

$$\tau(\tilde{\nu}) = \exp[-10^{a(c'(\tilde{\nu}) + \log_{10} W)}] \quad (2-7)$$

where  $W$  is determined from Equation 2-3. The values of the parameters  $a$ ,  $n$ ,  $m$  are given in Reference 2-11 as are also the parameters  $c'(\tilde{\nu})$  for  $\tilde{\nu}$  ranging from 1085 to 3215 cm<sup>-1</sup>. This interval spans the region of the two IR-active fundamentals  $\nu_3$  (1306 cm<sup>-1</sup>) and  $\nu_4$  (3020 cm<sup>-1</sup>). Again, the spectral emissivity is given by Equation 2-4 and the broad-band emissivity by Equation 2-5.

The broad-band emissivity, at a temperature of 256 °K and total pressure of 0.54 atm, is shown in Figure 2-3 (along with results for the other hydrocarbons described below) as a function of path length (atm cm) through the methane layer. Arrows near the bottom of Figure 2-3 show the values of U from Table 2-3 corresponding to the fire contribution in the baseline case. For methane, the ambient value for U is also shown. It corresponds to an emissivity of about  $10^{-2}$ , which is equivalent to a transmissivity of 99 percent. The incremental amounts from the products of combustion are only about 0.1 percent.

Ethane ( $C_2H_6$ ). For ethane, we have been able to find absorption-coefficient data for only the  $\nu_9$  band centered at  $821.52 \text{ cm}^{-1}$  ( $12.2 \text{ }\mu\text{m}$ ). Although this is believed to be the major band of interest to us, the results obtained below should be considered as lower limits to the broad-band emissivity.

The spectral absorption-coefficient data for the  $\nu_9$  band, obtained by Varanasi, et al. (Reference 2-12), can be represented as

$$k_{\tilde{\nu}} = S \sqrt{\frac{a}{\pi}} \exp[-a(\tilde{\nu} - \tilde{\nu}_0)^2] \quad (\text{atm}^{-1} \text{ cm}^{-1}) \quad , \quad (2-8)$$

where

$$S = \int_{-\infty}^{\infty} k_{\tilde{\nu}} d(\tilde{\nu} - \tilde{\nu}_0) = 31 \left( \frac{300}{T} \right) (\text{atm}^{-1} \text{ cm}^{-1}) \quad ,$$

$$a = 5.79 \times 10^{-4} \text{ cm}^2 \quad ,$$

and

$$\tilde{\nu}_0 = 825 \text{ cm}^{-1} \quad .$$

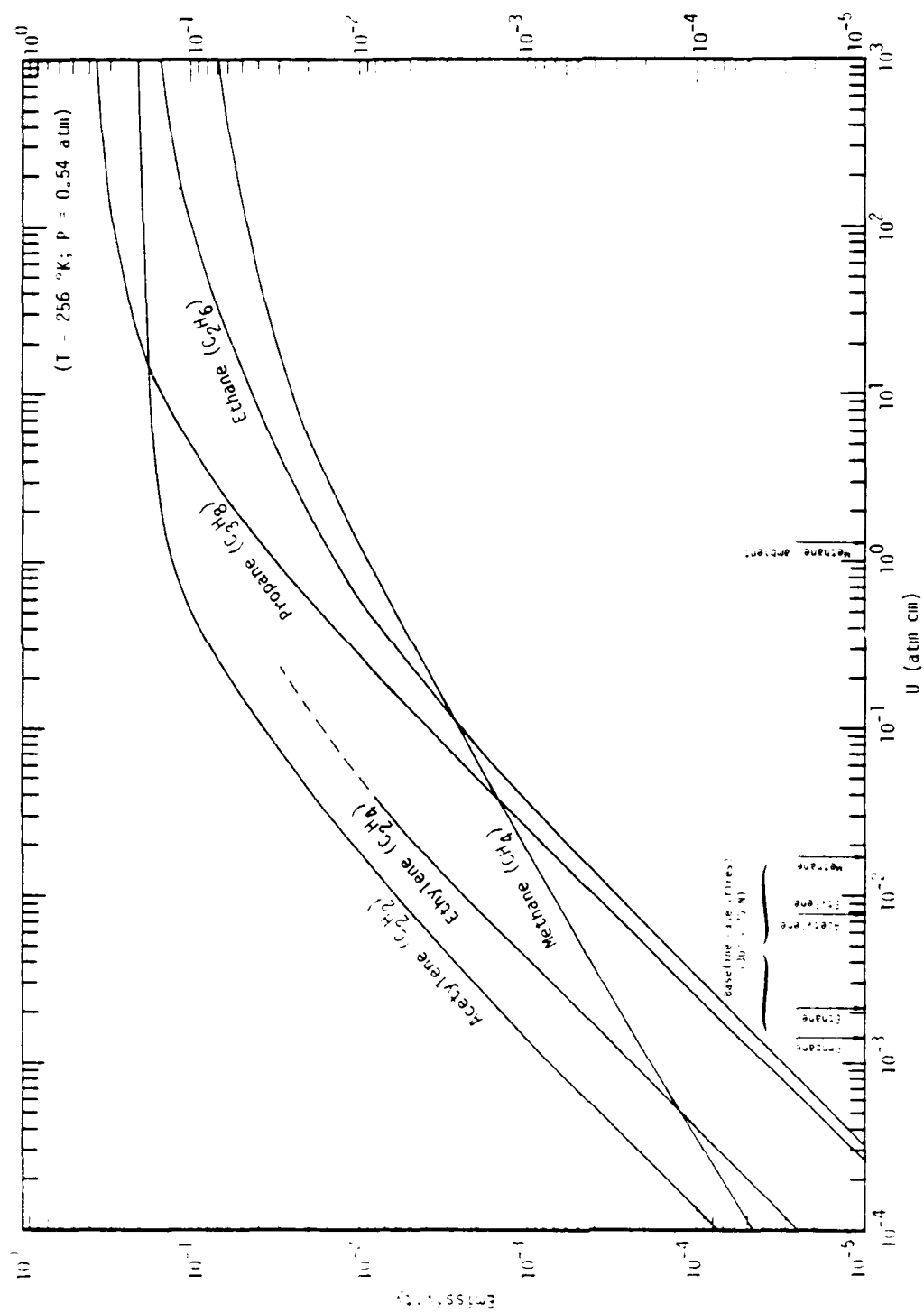


Figure 2-3. Broad-band infrared emissivity for selected hydrocarbons.

Assuming the statistical (Lorentz line) band model, the transmission is given by (Reference 2-13)

$$T(\tilde{\nu}) = \exp\left[-k_{\tilde{\nu}} U / \sqrt{1 + k_{\tilde{\nu}}^2 U^2 / (4a_c^2)}\right] \quad (2-9)$$

where, again,  $U$  (atm cm) is the absorber amount and

$$a_c = \gamma_c / d \quad (2-10)$$

Here,  $\gamma_c$  and  $d$  are, respectively, the mean (collision broadened) line width and mean line spacing.

For ethane, we take (Reference 2-12)

$$\gamma_c \approx 0.102 \left(\frac{300}{T}\right)^{1/2} P_{\text{atm}} \quad ; \quad d \approx 2.6 \text{ cm}^{-1} \quad (2-11)$$

where  $P_{\text{atm}}$  is the total pressure in atmospheres. Although  $a_c$  is generally a function of  $\tilde{\nu}$ , we assume it to be a constant. With the above parameter values, along with values for  $T$  and  $P_{\text{atm}}$  of 256 °K and 0.54 atm, respectively, Equations 2-4, 2-5, and 2-9 lead to the broad-band emissivity for ethane shown in Figure 2-3. For the amount of ethane injected into the atmosphere by massive burning ( $2.1 \times 10^{-3}$  atm cm), the emissivity is seen to be very small ( $6 \times 10^{-5}$ ), corresponding to almost complete transparency of the thermal radiation. It is unlikely that this result would be significantly different had the other bands of ethane been included.

Propane ( $C_3H_8$ ). For propane we use the band-model parameters of Giver, et al. (Reference 2-14). The spectral transmission can be represented by the expression

$$\tau(\tilde{\nu}) = \exp[-k_{\nu}U/\sqrt{1+k_{\nu}^2U/(\pi a_c)}] \quad (2-12)$$

where

$$a_c = a_c^0(\tilde{\nu}) P_{atm} \quad (2-13)$$

From plots of  $a_c^0(\text{atm}^{-1})$  and  $k_{\nu}(\text{atm}^{-1} \text{ cm}^{-1})$  as functions of  $\tilde{\nu}$  given in Reference 2-14, we have computed the spectral transmissivity and emissivity from Equations 2-12 and 2-4, respectively, and the broad-band IR emissivity from Equation 2-5, as functions of  $U$ . The results are shown in Figure 2-3.

From the amount of propane injected into the atmosphere in the baseline case ( $1.4 \times 10^{-3} \text{ atm cm}$ ), we see that the emissivity is nearly the same as that for ethane ( $6 \times 10^{-5}$ ) and that any decrease in the transmission of thermal radiation due to injected propane is quite negligible.

Acetylene ( $\text{C}_2\text{H}_2$ ). Integrated band intensities,  $S$ , at 300 °K have been measured for several bands of acetylene by Varanasi and Bangaru (Reference 2-15). These are shown in Table 2-4. Of the four shown, two are fundamentals and two are intercombination bands. The  $\nu_3$  fundamental and the  $\nu_2 + \nu_4 + \nu_5$  intercombination band severely overlap and are treated as a single band. We call this "band 3." The  $\nu_5$  fundamental and the  $\nu_4 + \nu_5$  intercombination band will be referred to as bands "1" and "2," respectively. Only for band 1 are spectral absorption coefficients given in Reference 2-15. To obtain the broad-band emissivity, including contributions from bands 2 and 3, we use an approximation developed in Appendix A.

Table 2-4. Band intensities for acetylene at 300 °K (Reference 2-15).

Band	Band Center (cm <sup>-1</sup> )	Wavelength (μm)	S (atm <sup>-1</sup> cm <sup>-2</sup> )
(1) $\nu_5$	729	13.7	729
(2) $\nu_4 + \nu_5$	1328	7.53	87
(3) $\left. \begin{array}{l} \nu_3 \\ \nu_2 + \nu_4 + \nu_5 \end{array} \right\}$	$\left. \begin{array}{l} 3295 \\ 3282 \end{array} \right\} 3290$	3.04	294

Consider first "band 1." As for the case of ethane, we write the spectral transmissivity in the form

$$T(\tilde{\nu}) = \exp[-k_{\tilde{\nu}} l / \sqrt{1 + k_{\tilde{\nu}}^2 l^2 / (4a_c)}] \quad (2-14)$$

where

$$a_c = \gamma_c / d = a_c^0 P_{\text{atm}} \quad (2-15)$$

We have been unable to find values of  $a_c^0$  for acetylene. However, for propane near 750 cm<sup>-1</sup>,  $a_c^0 \approx 1 \text{ atm}^{-1}$  (Reference 2-14), and we arbitrarily adopt this value here. Values for  $k_{\tilde{\nu}}$  (atm<sup>-1</sup> cm<sup>-1</sup>) from 650 to 810 cm<sup>-1</sup> are available from Reference 2-15. These, together with Equations 2-14, 2-15, 2-4, and 2-5, were used to compute the broad-band emissivity for the  $\nu_5$  band.

In Appendix A we show that if an absorbing layer is optically thin to a molecular band ( $k_{\tilde{\nu}} l \ll 1$ ), then the broad-band emissivity for that band is given by

$$\bar{\epsilon} \approx 1.53 B'(\tilde{\nu}_0)SU/T^4 \quad (2-16)$$

where

$$B'(\tilde{\nu}_0) = \tilde{\nu}_0^3 (e^{1.435 \tilde{\nu}_0/T} - 1)^{-1} \quad , \quad (2-17)$$

$\tilde{\nu}_0$  is the band-center wavenumber,  $S$  is the integrated band intensity ( $\text{atm}^{-1} \text{cm}^{-2}$ ), and  $U(\text{atm cm})$  is the layer thickness. It turns out that under nuclear-winter conditions, values of  $U$  for acetylene are sufficiently small (Table 2-3) that the layer is optically very thin and so the condition for applicability of Equation 2-16 is easily satisfied. Consequently, for bands 2 and 3, at a temperature of 256 °K, and with values for  $\tilde{\nu}_0$  and  $S$  from Table 2-4, Equation 2-16 leads to the result

$$\bar{\epsilon}_2 + \bar{\epsilon}_3 = 1.8 \times 10^{-2} U \quad . \quad (2-18)$$

Equation 2-12 for the spectral transmissivity is called the "curve of growth." For small values of  $k_{\nu}U$ , the exponent is linear in  $k_{\nu}U$ . But for large enough  $k_{\nu}U$  the exponent varies as the square root of  $k_{\nu}U$ . In the linear region it turns out, from our detailed calculations, or from Equation 2-16, that for "band 1" we can write

$$\bar{\epsilon}_1(k_{\nu}U \ll 1) = 7.3 \times 10^{-1} U \quad . \quad (2-19)$$

Comparing Equations 2-18 and 2-19 we see that the contribution to the broad-band emissivity from "band 1" is about 42 times greater than that from the sum of bands 2 and 3. Consequently, bands 2 and 3 can be ignored with very little error. This permits us to plot the broad-band emissivity for acetylene as a function of  $U$ , even to large values of  $U$ .

The results are shown in Figure 2-3. For the value of  $U$  in the baseline case ( $7.4 \times 10^{-3}$ ), we see that the emissivity is about  $5 \times 10^{-3}$ , which corresponds to a decrease in the transmission of only 0.5 percent.

Ethylene ( $C_2H_4$ ). We have found no band model nor spectral absorption coefficients in the literature for ethylene. However, Nakanaga, et al. (Reference 2-16) have measured integrated band intensities,  $S_i$ , for the  $\nu_7$ ,  $\nu_9$ ,  $\nu_{10}$ ,  $\nu_{11}$ , and  $\nu_{12}$  bands. The results are shown in Table 2-5. For sufficiently small values of  $U$ , we can determine the broad-band emissivity from the equation (Appendix A)

$$\bar{\epsilon} \approx 1.53 \sum_i R'(\tilde{\nu}_i) S_i U / T^4 \quad (2-20)$$

Table 2-5. Band intensities for ethylene (Reference 2-16).

Band	$\tilde{\nu}_i$ ( $cm^{-1}$ )	Wavelength ( $\mu m$ )	$S_i$ ( $atm^{-1} cm^{-2}$ )
$\nu_7$	949	10.54	376.9
$\nu_9$	3105	3.22	116.1
$\nu_{10}$	826	12.11	0.134
$\nu_{11}$	2989	3.35	63.9
$\nu_{12}$	1443	6.93	46.4

where the sum in Equation 2-20 is taken over all molecular bands and  $R'(\tilde{\nu}_i)$  is given by Equation 2-17. When the parameters from Table 2-5 are used in Equation 2-20, we obtain, for  $T = 256^\circ K$ ,

$$\bar{\epsilon}_{\text{ethylene}}^{\text{optically thin}} \approx 0.25 U \text{ atm cm} \quad (2-21)$$

which is plotted in Figure 2-3.



Equation 2-21 should be valid for the nuclear-winter application in which, for the baseline case,  $U \approx 8.2 \times 10^{-3}$  and so  $\bar{\epsilon} \approx 2 \times 10^{-3}$ . This corresponds to a decrease in the transmission of thermal radiation due to the ethylene layer of only 0.2 percent.

If we add the effects of all the hydrocarbons resulting from massive burning (baseline case), we find a total broad-band emissivity of about  $8.1 \times 10^{-3}$ . However, due to band overlap among the different species, the resultant emissivity will be somewhat less than this (see Appendix B). We therefore expect that the injected hydrocarbons will decrease the transmission of thermal radiation through the layer by less than 1 percent.

## BROAD-BAND IR PROPERTIES OF PARTICULATE LAYERS

In this subsection we describe calculations performed to estimate the broad-band IR properties of particulate layers of interest in the nuclear-winter problem. Of special relevance are the emissivity, transmissivity, and reflectivity of water clouds, dust layers, soot (carbon) layers, and layers containing a mixture of soot particles and water droplets. We first describe the method employed and then present the results for specific particle types.

### Method

We are interested in determining the broad-band IR emissivity,  $\bar{\epsilon}$ , transmissivity,  $\bar{T}$ , and reflectivity,  $\bar{R}$ , for particle layers of thickness  $U$  ( $\text{gm cm}^{-2}$ ). These quantities are related by the expression

$$\bar{\epsilon} + \bar{T} + \bar{R} = 1 \quad (2-22)$$

Here,  $\bar{\epsilon}$  is defined by the relation 2-5, and  $\bar{T}$  and  $\bar{R}$  are defined by corresponding expressions in which the spectral emissivity,  $\epsilon(\tilde{\nu})$ , is replaced by the spectral coefficients  $T(\tilde{\nu})$  and  $R(\tilde{\nu})$ , respectively.

Initially, we attempted to calculate the spectral coefficients  $\varepsilon(\tilde{\nu})$ ,  $T(\tilde{\nu})$ , and  $R(\tilde{\nu})$  using a Mie-scattering code, and a radiation transport algorithm similar to one in the RNSCOE and NORSE codes. However, we ran into numerical difficulties with the method, especially when considering mixtures of particles where, for certain values of  $U$  and density ratios of particle types, the sum 2-22 exceeded unity. Subsequently, we adopted an approximate procedure, summarized by Bartky and Bauer (Reference 2-17), for calculating the spectral coefficients in terms of the Mie-scattering cross sections that we obtained from our Mie code.

The appropriate formulas for the spectral coefficients, using the parallel beam or one-dimensional approximation, are as follows:

$$\varepsilon = 2\kappa[e^{k\tau}(k+\kappa) + e^{-k\tau}(k-\kappa) - 2k]/D \quad (2-23)$$

$$R = (k^2 - \kappa^2)(e^{k\tau} - e^{-k\tau})/D \quad (2-24)$$

$$T = 4\kappa k/D, \quad (2-25)$$

where

$$D = (k + \kappa)^2 e^{k\tau} - (k - \kappa)^2 e^{-k\tau} \quad (2-26)$$

$$k = \{\kappa[2(1 - \kappa)\beta + \kappa]\}^{1/2} \quad (2-27)$$

$$\kappa = \sigma_a/(\sigma_a + \sigma_s) = q_a/(q_a + q_s) \quad (2-28)$$

$$\alpha + \beta = 1 \quad (2-29)$$

and

$$\beta = 0.5 \int_{\pi/2}^{\pi} P(\theta) \sin\theta d\theta = 0.5 \int_{-1}^0 P(\mu) d\mu \quad (2-30)$$

Here,  $\sigma_a$  and  $\sigma_s$  are, respectively, the absorption and scattering cross sections ( $\text{cm}^2$ ),  $q_a$  and  $q_s$  are the related mass absorption and mass-scattering cross sections ( $\text{cm}^2 \text{ gm}^{-1}$ ),  $\alpha$  and  $\beta$  are the fractions of the radiation scattered forward and backward, respectively, at a single scattering, and  $P(\theta)$  is the scattering pattern normalized such that

$$0.5 \int_{-1}^1 P(\mu) d\mu = 1, \quad (2-31)$$

where  $\mu = \cos\theta$  and  $\theta$  is the scattering angle. The quantity  $\tau$  is the optical depth which, for a distance  $z$  into a medium of particle number density  $N$ , is given by

$$\tau = \int_0^z (\sigma_a + \sigma_s) N dz'. \quad (2-32)$$

Alternatively,

$$\tau = (q_a + q_s) l = q_e l, \quad (2-33)$$

where  $q_e$ , the sum of  $q_a$  and  $q_s$ , is the mass-extinction coefficient.

In computing the spectral coefficients  $\epsilon$ ,  $R$ , and  $T$  from Equations 2-23 to 2-25, the quantities required as input are the absorption and scattering cross sections (for determining  $\kappa$ ) and the scattering pattern  $P(\theta)$  (for determining  $\beta$ ). We have evaluated these quantities, averaged over specified particle-size distributions, from Mie codes developed originally by Thompson at General Electric Co., TEMPO, and described in Reference 2-18. Specifically, we have performed calculations for two different size distributions of water droplets, for a distribution of dust (basaltic glass) particles, for a distribution of soot (carbon)

particles, and for a combined distribution of water droplets and soot particles. The basic ingredient in these calculations is the complex refractive index of the particles as a function of wavelength. Values used for the real and imaginary components were obtained from References 2-19 to 2-21 and are tabulated in Appendix C.

For a mixture of soot particles and water droplets, we used the following expressions for the parameters  $\kappa$  and  $\beta$  that appear in the foregoing relations:

$$\kappa = \frac{(\rho^W/\rho^S)q_a^W + q_a^S}{(\rho^W/\rho^S)q_e^W + q_e^S} \quad (2-34)$$

$$\beta = \frac{(\rho^W/\rho^S)q_s^W\beta^W + q_s^S\beta^S}{(\rho^W/\rho^S)q_s^W + q_s^S} \quad (2-35)$$

$$\tau = q_e^W\tau^W + q_e^S\tau^S \quad (2-36)$$

Here,  $\rho^W$  and  $\rho^S$  are the mass density of water drops and soot particles, respectively. The other parameters have their usual meaning, with superscripts "s" and "w" referring, respectively, to soot particles and water droplets.

Particle Size Distributions. We assume the log-normal distribution of particle diameters,  $D$ :

$$f(D) = \frac{e^{-0.5[\ln(D/D_m)/\ln S]^2}}{\sqrt{2\pi} D \ln S} \quad (2-37)$$

where  $D_m$  and  $S$  are the mean diameter and standard-deviation parameters, respectively. The values used for  $D_m$  and  $S$  for each particle type are shown in Table 2-6. In the case of water droplets (clouds), calculations were made for two different distributions. The first distribution approximates measurements made on altostratus clouds (see Reference 2-22); the second contains a larger fraction of larger droplets. The dust and soot distributions are those used for the baseline calculations (Reference 2-1). For calculations involving a combination of soot and water droplets, distribution 1 for water was used. These distributions are shown in Figure 2-4.

Table 2-6. Log-normal parameters used in the Mie calculations.

Particle	$D_m(\mu m)$	$S$
water (1)	10.477	1.6
water (2)	17.918	1.4
dust (basaltic glass)	0.5	2.0
soot (carbon)	0.2	2.0

## Results

Figures 2-5 to 2-8 show the calculated broad-band IR properties for water clouds, dust layers, and soot layers as functions of the particle content ( $gm\ cm^{-2}$ ) along the path. Figure 2-9 shows the broad-band emissivity of a layer containing a mixture of soot particles and water drops (distribution 1) for selected values of the  $\rho^w/\rho^s$  ratio. More complete results for this case, including the transmissivities and reflectivities, are given in Table C-4 of Appendix C.

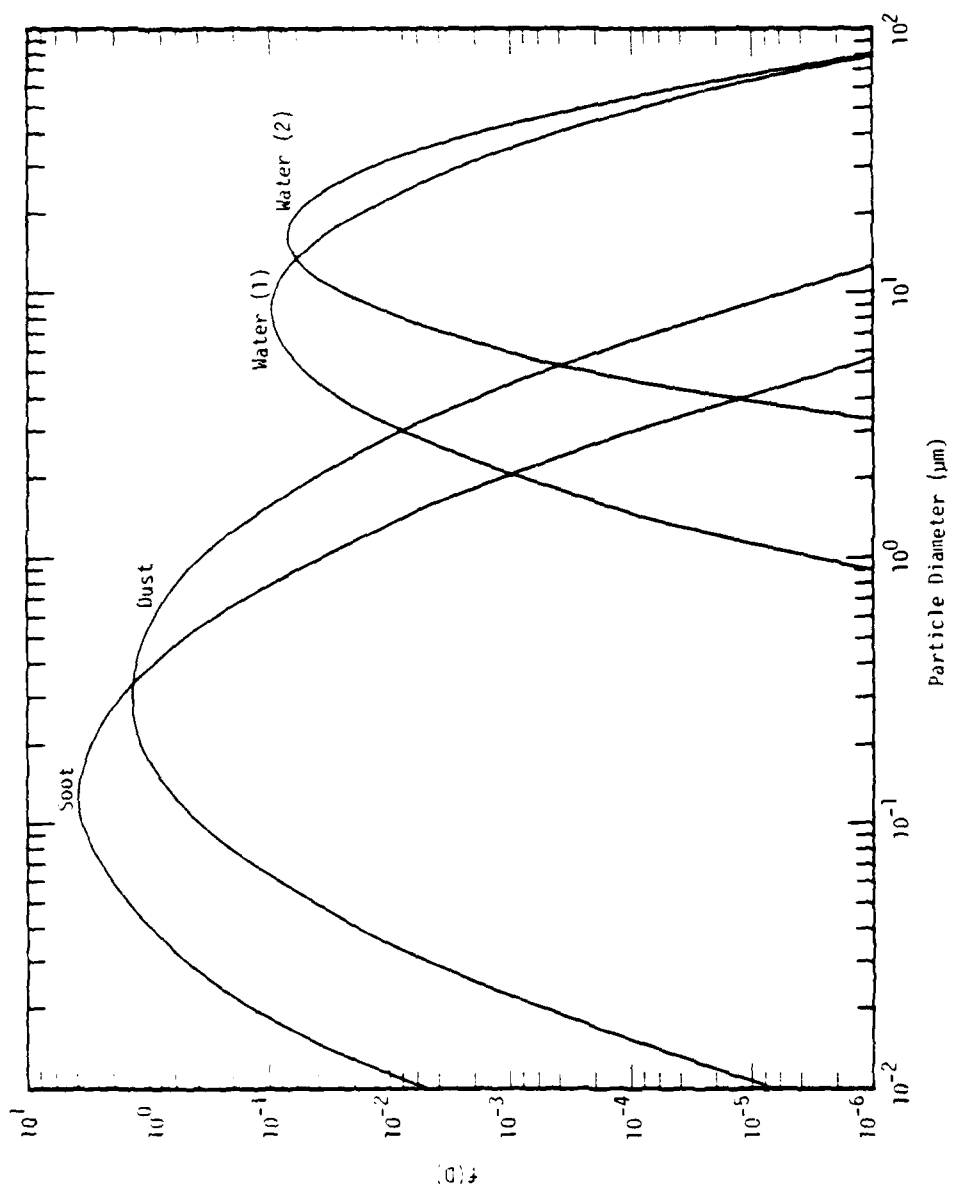


Figure 2-4. Particle size distributions used in calculations.

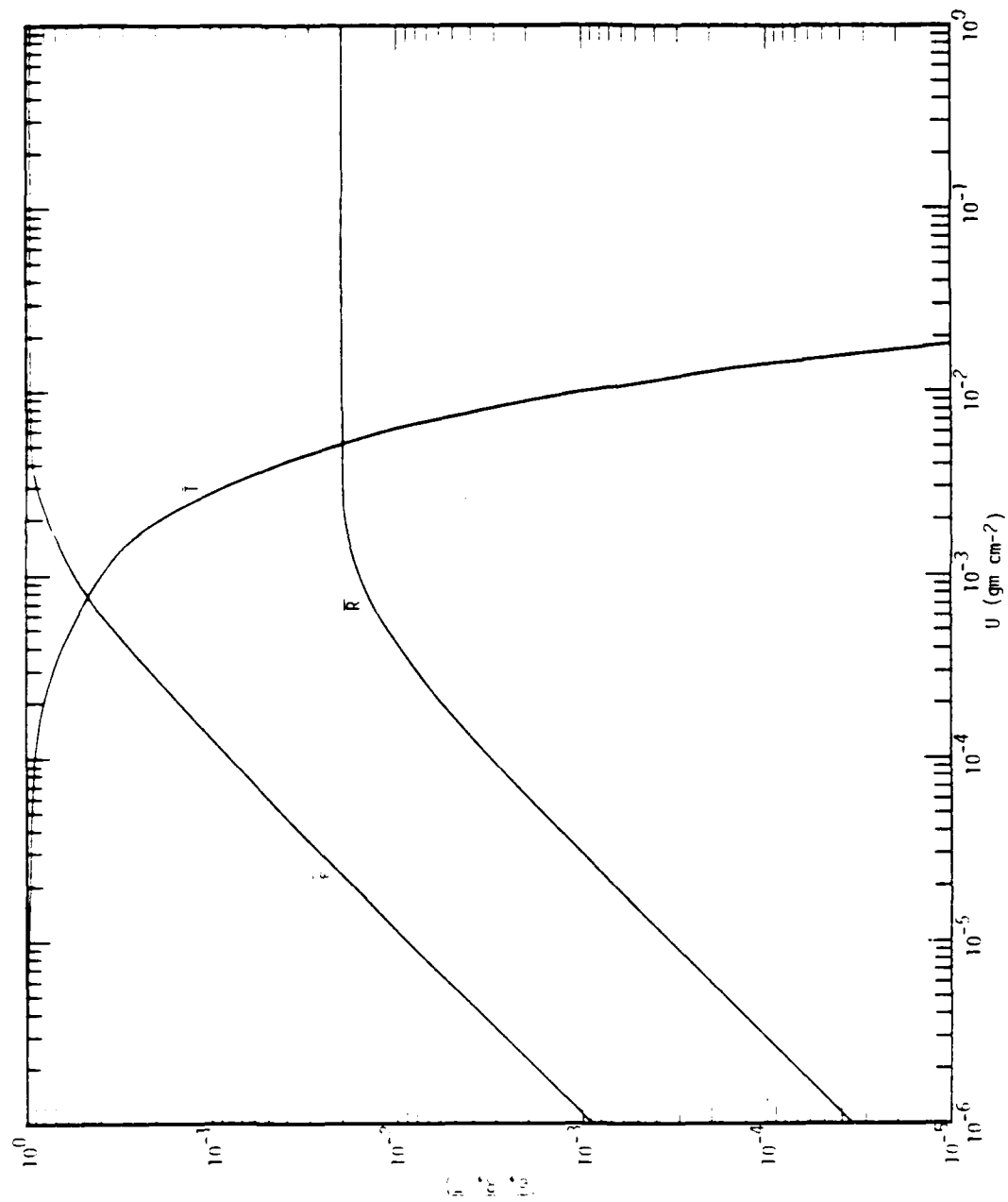


Figure 2-5. Broad-band IR properties of water clouds (distribution 1).

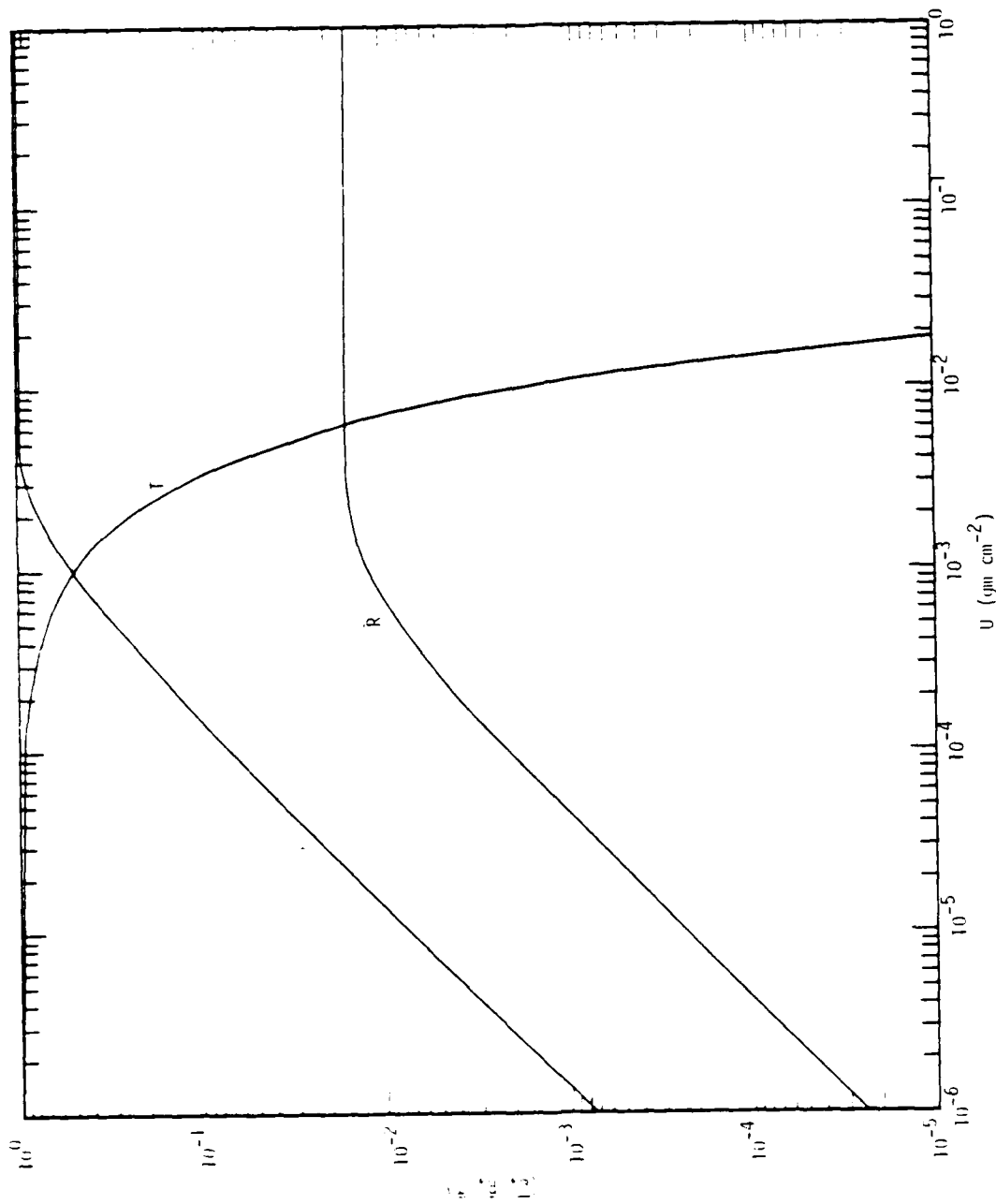


Figure 2-6. Broad-band IR properties of water clouds (distribution 2).



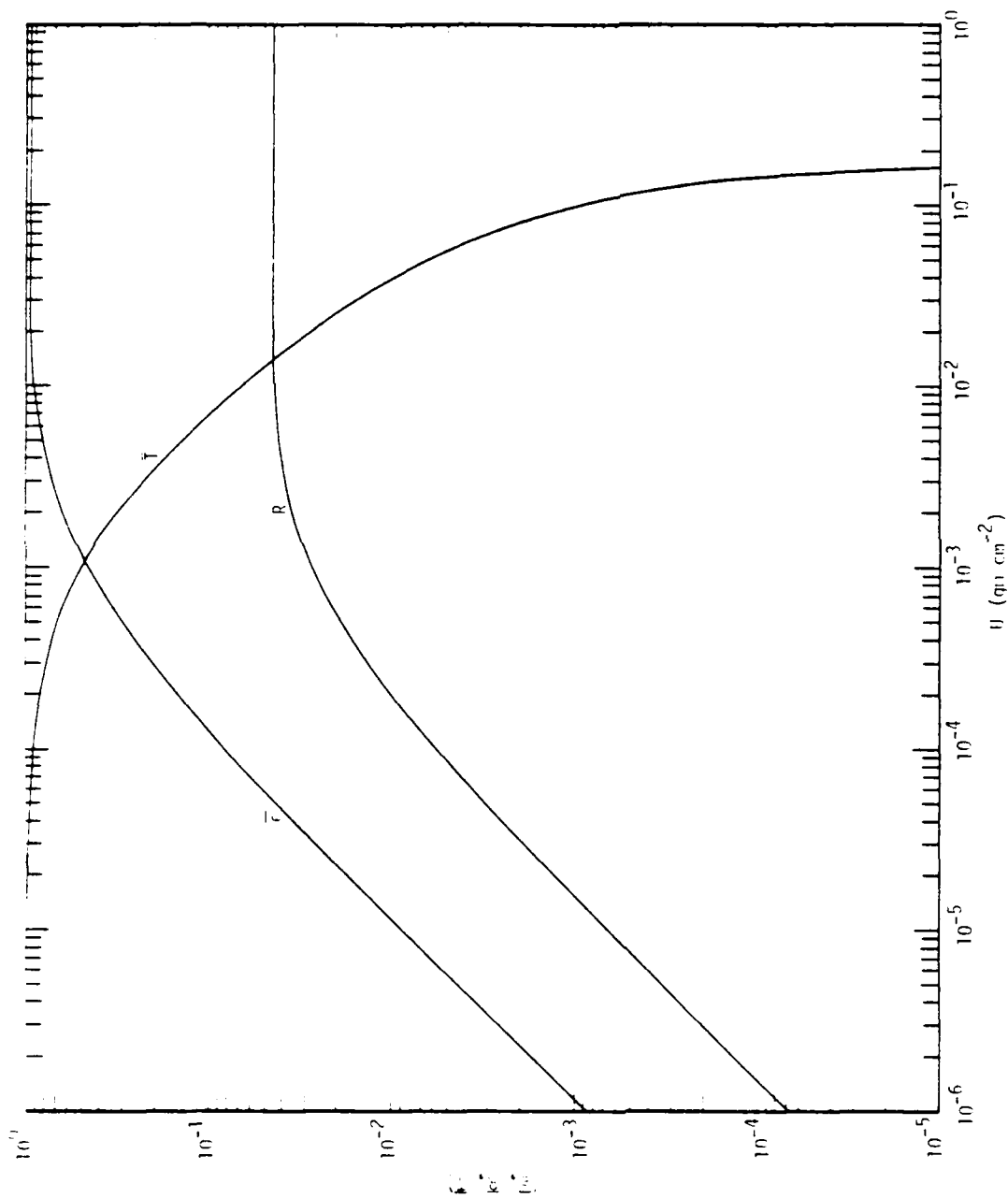


Figure 2-7. Broad-band IR properties of dust (basaltic glass) layers.

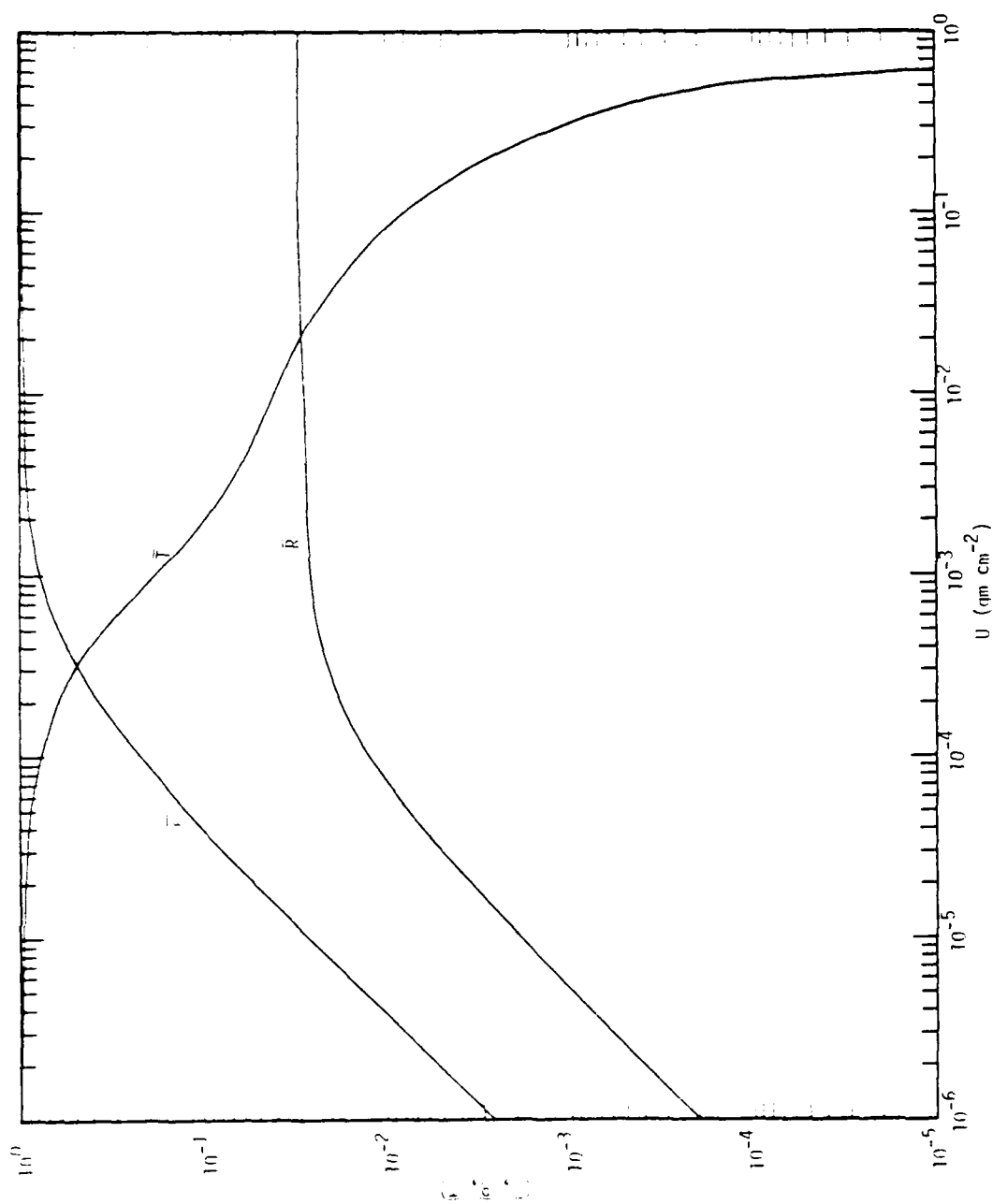


Figure 2-8. Broad-band IR properties of soot (carbon) layers.

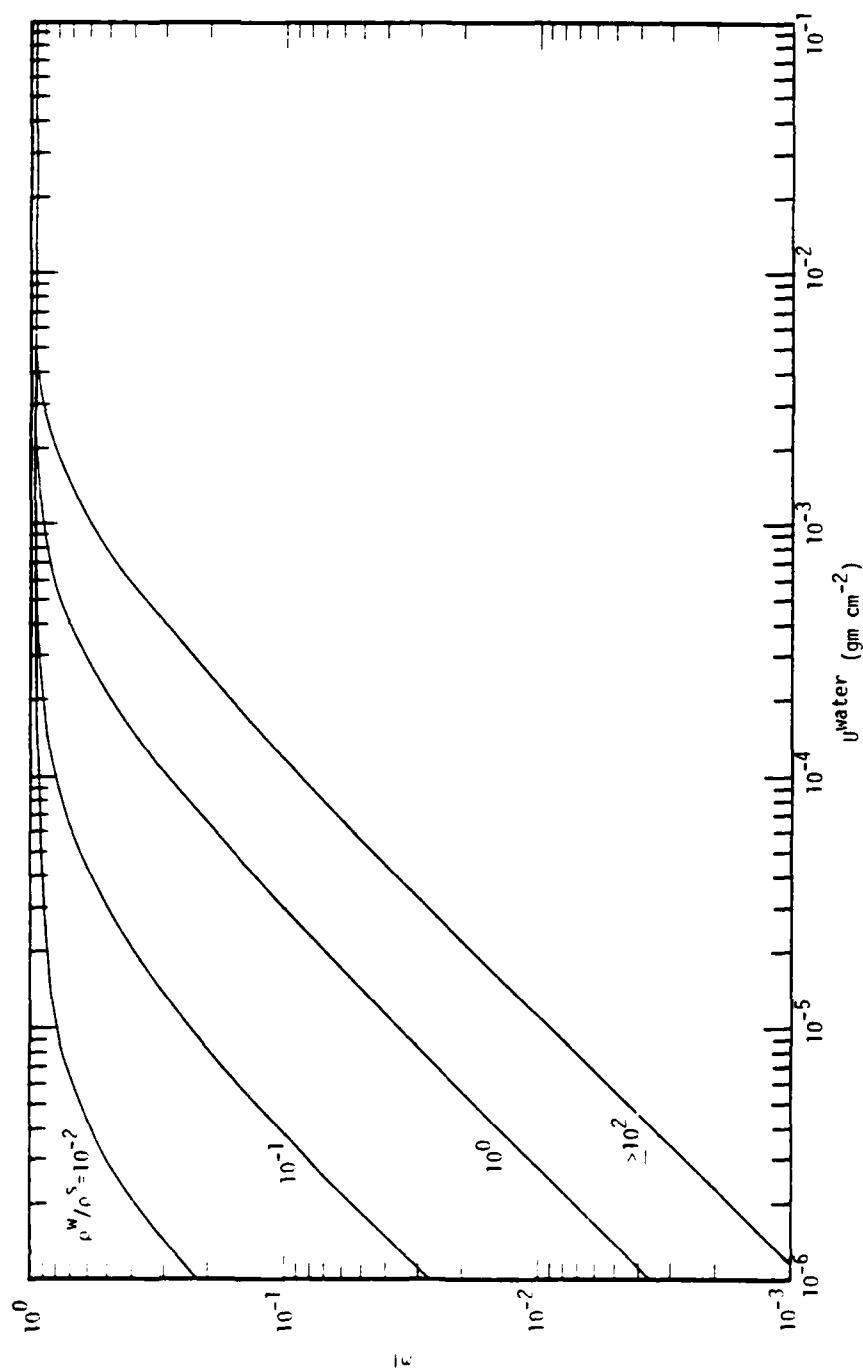


Figure 2-9. Broad-band IR emissivity of sooty water clouds for selected values of the water-to-soot density ratio.

## OPTICAL PROPERTIES OF PARTICULATE LAYERS IN THE VISIBLE

The formulas 2-23 to 2-36 have been applied to the calculation of the optical properties of particulate layers at a wavelength of  $0.55 \mu\text{m}$  in the visible. The calculations were done for a water cloud (size distribution 1) a dust (basaltic glass) layer, a soot (carbon)-particle layer, and a layer consisting of a mixture of water droplets (distribution 1) and soot particles. For the size-distribution parameters shown in Table 2-6, the values obtained from our Mie-code calculations for the parameters  $q_a$ ,  $q_s$ ,  $q_e$ ,  $\kappa$ , and  $\beta$ , required for input to the formulas, are shown in Table 2-7. Also shown in Table 2-7 are the values for the real and imaginary components of the refractive index ( $n = n_R - in_I$ ) used in the Mie calculations. For water, dust (basaltic glass), and soot, the index values were obtained from References 2-20, 2-21, and 2-1, respectively.

Table 2-7. Input parameters to optical formulas for  $\lambda = 0.55 \mu\text{m}$ .

Particle	$n_R$	$n_I$	$q_a(\text{cm}^2 \text{ gm}^{-1})$	$q_s(\text{cm}^2 \text{ gm}^{-1})$	$q_e(\text{cm}^2 \text{ gm}^{-1})$	$\kappa$	$\beta$
water (1)	1.335	$1.0 \times 10^{-9}$	$2.568 \times 10^1$	$1.715 \times 10^3$	$1.741 \times 10^3$	$1.475 \times 10^{-7}$	$4.603 \times 10^{-2}$
dust	1.57	$4.6 \times 10^{-4}$	$8.010 \times 10^1$	$9.228 \times 10^3$	$9.308 \times 10^3$	$8.605 \times 10^{-3}$	$1.090 \times 10^{-1}$
soot	1.55	0.1	$1.770 \times 10^4$	$2.652 \times 10^4$	$4.422 \times 10^4$	$4.003 \times 10^{-1}$	$6.464 \times 10^{-2}$

Figures 2-10, 2-11, and 2-12 show the resulting values of the emissivity, transmissivity, and reflectivity as functions of the layer thickness ( $\text{gm cm}^{-2}$ ) through the water, dust, and soot layers, respectively. For the layer consisting of a mixture of soot particles and water droplets, results have been obtained for parametric values of the  $\rho^W/\rho^S$  ratio and the optical depth. These are shown in Table C-5 of Appendix C. The emissivity results in this case, for selected values of the  $\rho^W/\rho^S$  ratio, are shown in Figure 2-13.

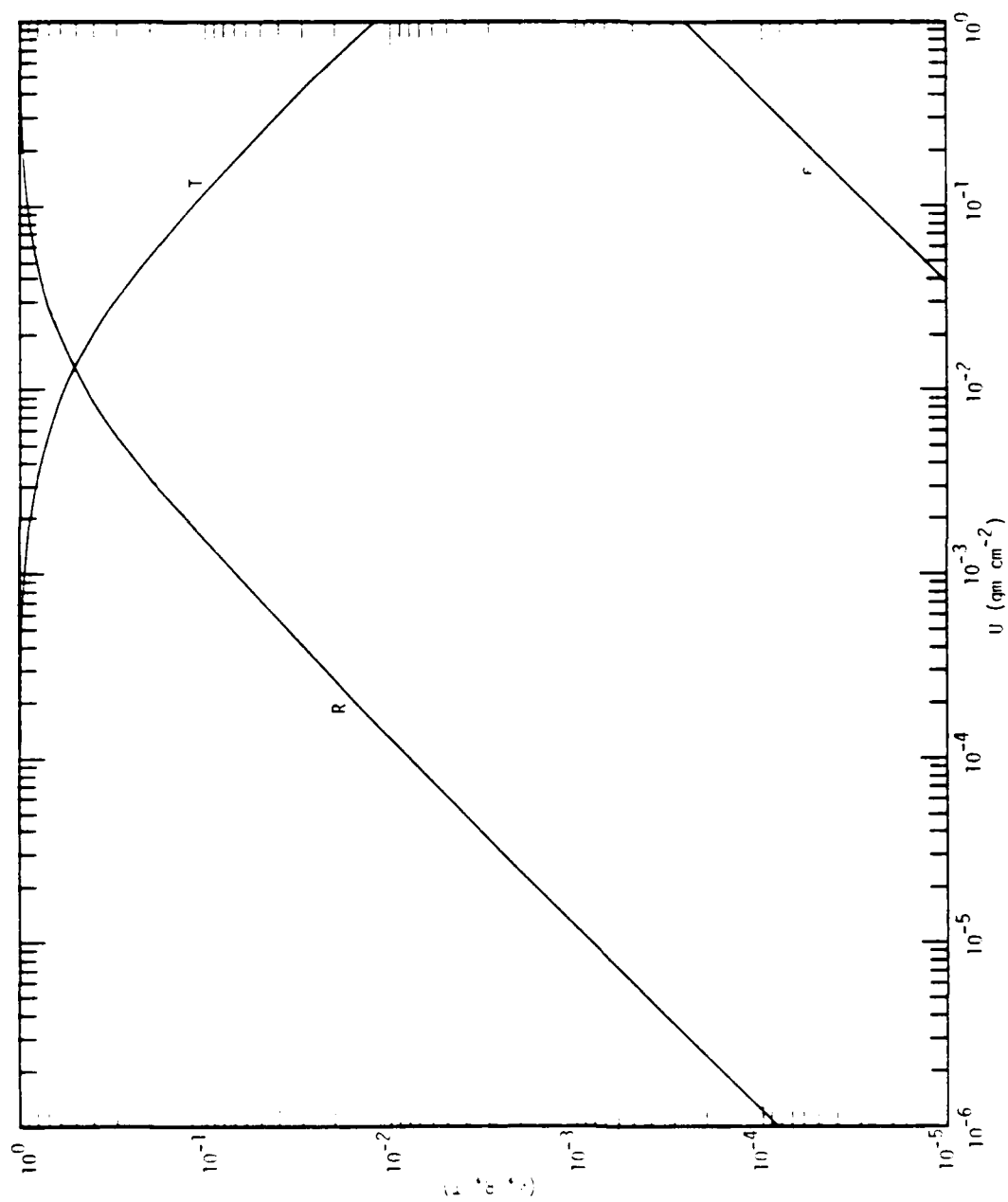


Figure 2-10. Optical properties in the visible ( $\lambda=0.55 \mu\text{m}$ ) of water clouds (distribution 1).

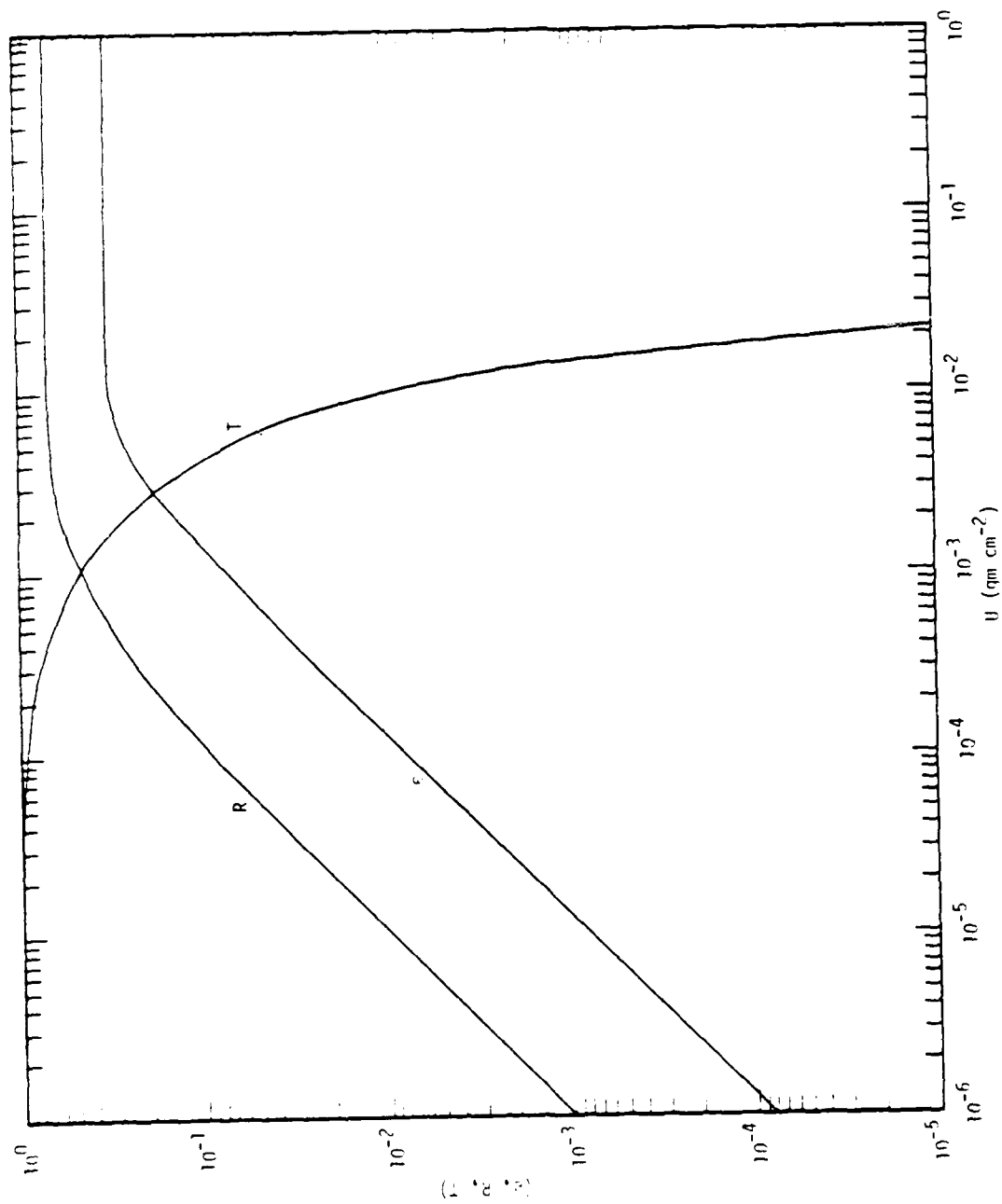


Figure 2-11. Optical properties in the visible ( $\lambda = 0.55 \mu\text{m}$ ) of dust (basaltic glass) layers.

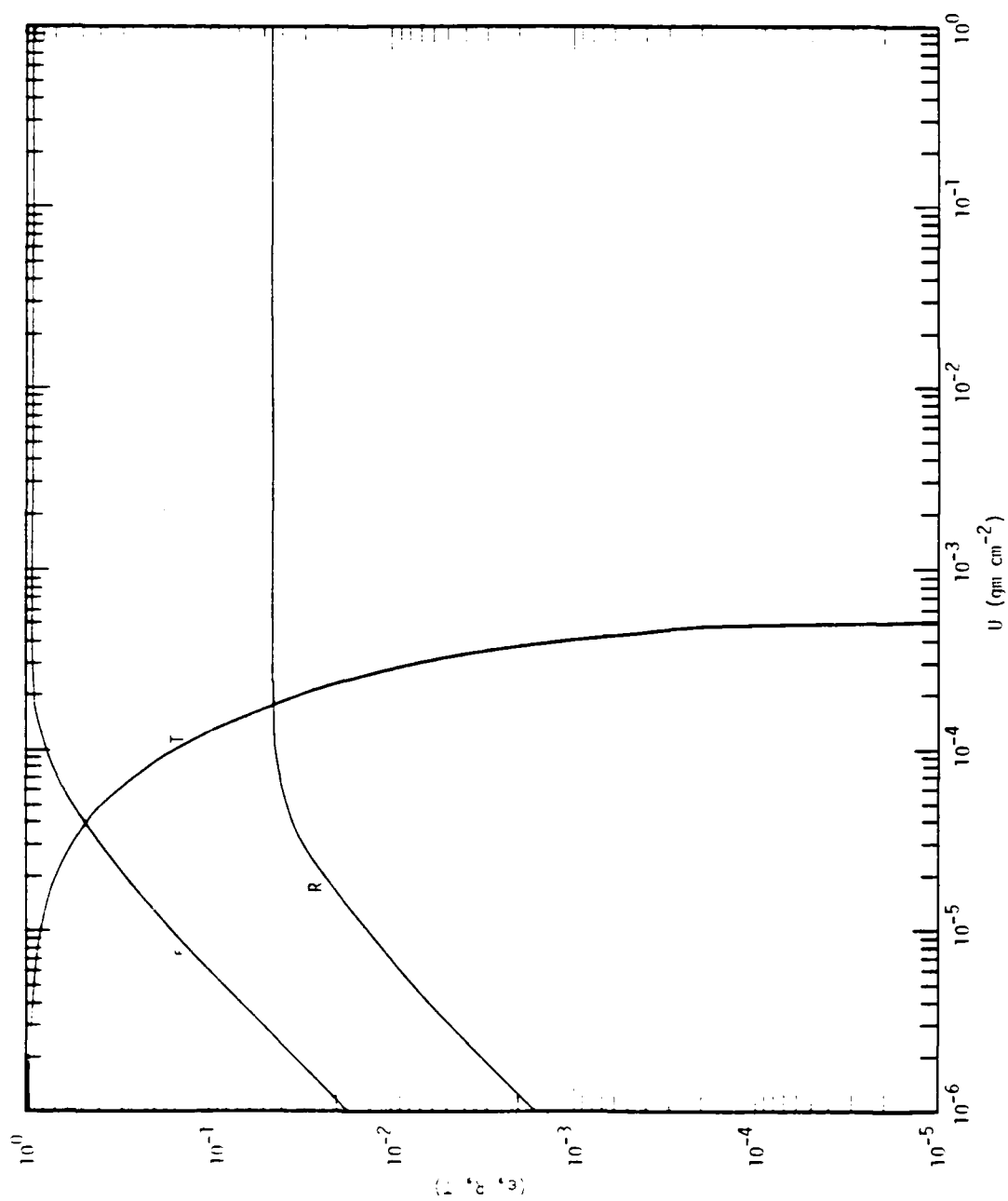


Figure 2-12. Optical properties in the visible ( $\lambda=0.55 \mu\text{m}$ ) of soot (carbon) layers.

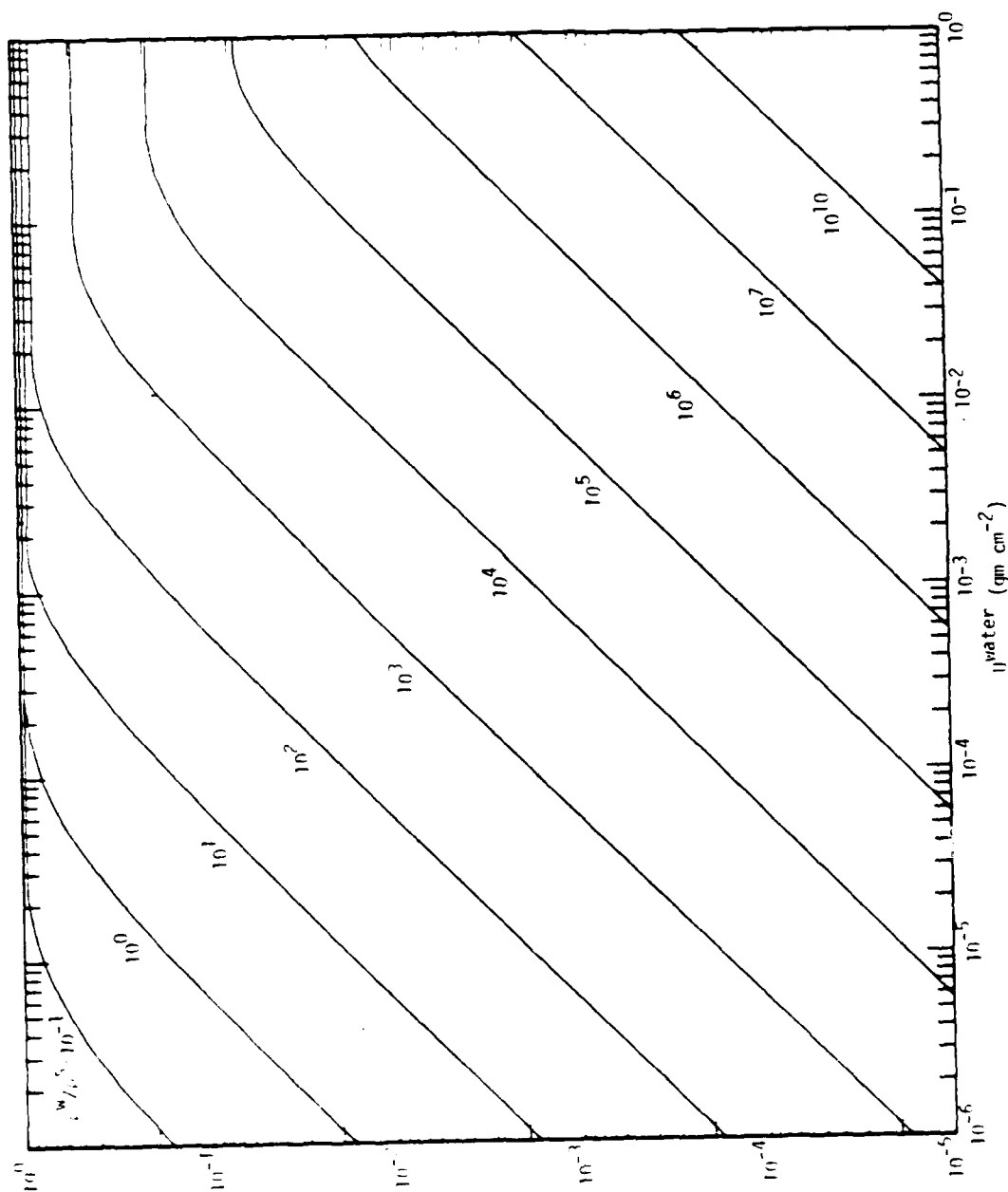


Figure 2-13. Emissivity in the visible ( $\lambda=0.55 \mu\text{m}$ ) of sooty water clouds for selected values of the water-to-soot density ratio.



### SECTION 3 MODEL CALCULATIONS

#### THE BASIC MODEL

Most of the models we shall discuss in this report will consist of two or three atmospheric layers over an earth which is assumed either to be black or to have some significant albedo (the last case is for study of the effect over snowpack). It is important to understand that within a given layer only the optical properties of the medium are taken as constant; the radiative fluxes and the temperature vary continuously throughout a given layer. Before discussing these models let us consider the case of a single layer which we shall take to be infinitely deep. We shall assume that a flux of solar energy of intensity  $\Sigma$  is incident on the surface of the layer which we take to be  $z=0$ . If such a flux is incident on a blackbody the body will reach an equilibrium temperature,  $T_{BB}$ , given by

$$T_{BB} = \left( \frac{\Sigma}{\sigma} \right)^{1/4} \quad (3-1)$$

where  $\sigma$  is the Stefan-Boltzmann constant. We shall assume that the medium in the layer is characterized by a visible opacity  $\epsilon_s$  but that the medium does not emit in the visible. We shall also assume that the medium possesses an opacity  $\epsilon_I$  in the infrared and that the infrared radiation consists of an upward flux,  $U$ , and a downward flux,  $D$ , since the medium does not emit in the visible the solar flux is downward and we shall call it  $S$ . The equations for the fluxes are

$$\frac{dS}{dz} = -\epsilon_s S \quad (3-2)$$

$$\frac{dU}{dz} = \epsilon_I U - \epsilon_I \sigma T^4$$

$$\frac{dD}{dz} = -\epsilon_I D + \epsilon_I \sigma T^4$$

$$2\epsilon_I \sigma T^4 = \epsilon_I (U+D) + \epsilon_S S$$

In order to produce transport equations of this form, it is necessary to assume local thermodynamic equilibrium, ignore scattering and provide an ansatz for the angular distribution of the radiation. If the radiation fields are taken to be uniform in angle over each hemisphere (up and down) but possibly of a different amplitude (Eddington's approximation), the above equations result provided that  $\epsilon$  is interpreted as twice the absorption opacity. The general solution to these equations (which we shall need later) is

$$\begin{aligned} S &= \Sigma e^{-\epsilon_S z} \\ U &= \frac{1}{2} \left\{ A \left( 1 - \frac{\epsilon_I}{\epsilon_S} \right) e^{-\epsilon_S z} + B(\epsilon_I z + 1) + C \right\} \\ D &= \frac{1}{2} \left\{ -A \left( 1 + \frac{\epsilon_I}{\epsilon_S} \right) e^{-\epsilon_S z} + B(\epsilon_I z - 1) + C \right\} \\ \tau \equiv \sigma T^4 &= \frac{1}{2} \left\{ A \left( \frac{\epsilon_S}{\epsilon_I} - \frac{\epsilon_I}{\epsilon_S} \right) e^{-\epsilon_S z} + B \epsilon_I z + C \right\} \end{aligned} \quad (3-3)$$

where we have defined  $\tau$  to be  $\sigma T^4$  in order to simplify the notation. The boundary conditions for the problem at hand are

$$\begin{aligned} S|_{z=0} &= \Sigma \\ D|_{z=0} &= 0 \\ U|_{z=0} &= S|_{z=0} \end{aligned} \quad (3-4)$$

For the temperature we get

$$\tau = \frac{\Sigma}{2} \left[ 1 + \frac{\epsilon_I}{\epsilon_S} + \left( \frac{\epsilon_S}{\epsilon_I} - \frac{\epsilon_I}{\epsilon_S} \right) e^{-\epsilon_S z} \right] \quad (3-5)$$

Many of the IR effects on the nuclear winter phenomenon can be understood in terms of this equation. If  $\epsilon_I = \epsilon_S$  we find that

$$\tau = \sigma T_{BB}^4 \quad (3-6)$$

independent of  $z$ . If  $\epsilon_S > \epsilon_I$  we find that at the top of the layer the temperature is hotter than  $T_{BB}$ :

$$\tau \Big|_{z=0} = \sigma T_{BB}^4 \frac{1}{2} \left( 1 + \frac{\epsilon_S}{\epsilon_I} \right) \quad (3-7)$$

The temperature decreases from this value as one proceeds into the layer asymptotically approaching a value less than  $T_{BB}$ :

$$\tau \Big|_{z=\infty} = \sigma T_{BB}^4 \frac{1}{2} \left( 1 + \frac{\epsilon_I}{\epsilon_S} \right) \quad (3-8)$$

If  $\epsilon_S < \epsilon_I$  the situation is reversed: Equations (3-7) and (3-8) are still valid but they now predict that the temperature at the top of the layer is less than  $T_{BB}$  while the temperature deep within the layer is greater than  $T_{BB}$ .

In the normal atmosphere the solar absorption is small but there is appreciable IR absorption due mostly to water vapor; thus  $\epsilon_I$  is larger than  $\epsilon_S$  and the stratosphere is colder than  $T_{BB}$  while the earth's surface

is warmer than  $T_{BB}$ . The essence of the nuclear winter phenomenon as it has been previously reported is that a layer of soot is injected into the atmosphere whereupon  $\epsilon_s$  becomes greater than  $\epsilon_I$ ; therefore the top of the layer, which is at several kilometers altitude, becomes hotter than  $T_{BB}$  while the surface temperature may cool to near  $T_{BB}$  or below (the reason it is usually not below  $T_{BB}$  is that the layer is not infinitely thick).

Before considering numerical examples we need a slightly more complicated model so that the effects of the finite thickness of the layers may be considered. We shall study the model shown in Figure 3-1. Layer 1 is composed primarily of dust and water vapor and we shall assume that it has a solar albedo,  $A_1$ , an IR opacity of  $\epsilon_{I1}$  with a total optical depth in the IR of  $\mu_{I1}$ , and no solar absorption; such a layer is probably there in realistic cases but its optional depth is probably not very great. Layer 2 is the soot layer - the main component of the nuclear winter phenomenon; we shall assume that it has a solar albedo of  $A_2$ , a solar opacity of  $\epsilon_{s2}$  with a total optical depth in the solar of  $\mu_{s2}$  and a ratio of  $\epsilon_{I2}/\epsilon_{s2}$  of  $\alpha$ . Layer 3 is included in the model to represent a possible rain-out layer which may or may not be present in realistic cases. We assume it has no solar absorption but has an IR opacity of  $\epsilon_{I3}$  with a total depth  $\mu_{I3}$  due mostly to water vapor. Under the third layer is the surface of the earth which is taken to be a black body.

Within any layer the temperature and the fluxes satisfy Equations (3-2) and so have the general solution (3-3). A complete solution is easily written down but the collection of formulae is somewhat tedious. Here we shall study the behavior of the temperature at two points:  $T_s$ , the temperature at the top of the soot layer and  $T_E$ , the temperature of the earth; the complete solution can be found in Appendix D. We have:

---

LAYER 1       $\epsilon_{I1}$ : DUE TO H<sub>2</sub>O, CO<sub>2</sub>, NO<sub>2</sub>  
              A<sub>1</sub> (Albedo): DUE TO DUST

---

LAYER 2       $\epsilon_{S2}$ : DUE TO SOOT  
               $\epsilon_{I2}$ : DUE TO SOOT, H<sub>2</sub>O, HYDROCARBONS, WATER CLOUDS  
              A<sub>2</sub>: DUE TO SOOT-CLOUD MIXTURE

---

LAYER 3 (RAINOUT LAYER)       $\epsilon_{I3}$ : DUE TO H<sub>2</sub>O

---

EARTH (BLACK BODY)

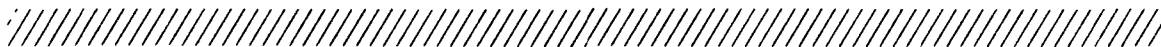


Figure 3-1. Schematic of the simple model nuclear winter which ignores convective instabilities.

$$\tau_s = \frac{1}{2} \Sigma (1-A_1)(1-A_2) \left[ 1 + \frac{1}{\alpha} + \mu_{I_1} \right] \quad (3-9)$$

$$\tau_E = \frac{1}{2} \Sigma (1-A_1)(1-A_2) \left[ 1 + \mu_{I_1} + \alpha(1 - e^{-\mu_{S_2}}) + (1 + \mu_{I_3}) e^{-\mu_{S_2}} \right] \quad (3-10)$$

Let us now look at some examples of using equations (3-9) and (3-10). We shall assume that  $\Sigma$  is equal to the solar constant divided by 4:  $\Sigma = 3.5 \times 10^5$  ergs/cm<sup>2</sup>sec. If we assume that layers 1 and 2 are missing, that  $\mu_{I_3} = 1.3$  and that the total albedo is .2 we obtain a temperature for  $T_E$  of 300K. This temperature represents approximately ambient conditions in our model and should be used as a standard of comparison for other temperatures we shall calculate later. Let us now consider a case which closely resembles the NRC baseline scenario: we shall choose  $\alpha$  to be .25, the NRC baseline value for pure soot<sup>1</sup>,  $\mu_{S_2}$  to be 2, the value attained in the NRC baseline scenario for the time of the minimum surface temperature;  $\mu_{I_1}$  we shall choose to be .2 based on the assumption that there will be a few times  $10^{-3}$ g/cm<sup>2</sup> of water vapor above the soot layer and shall choose the albedos to be:  $A_1 = .1$  based on  $\approx 10^{-4}$  g/cm<sup>2</sup> of dust and Fig. 2-11; and  $A_2 = .04$  based on Fig. 2-12. Equations (3-9) and (3-10) give  $T_s = 340$ K and  $T_E = 255$ K. We thus get a temperature for the earth which is 45K below the ambient value and a temperature for the top of the soot layer (which would have been at 237K under ambient conditions) 103K hotter than ambient; these results are in good agreement with the NRC study.

Of principal interest to the present study is the variation of these results with changes in the parameter  $\alpha$ . In Figure 3-2 we show a plot of  $T_s$  and  $T_E$  as functions of  $\alpha$  with all other parameters fixed at the values we have just used. The values of  $\alpha$  shown in the graph range from .1 to 5; according to the NRC the likely range of values for  $\alpha$  due to soot alone is .03 to 1<sup>2</sup>. We believe that there will always be enough water

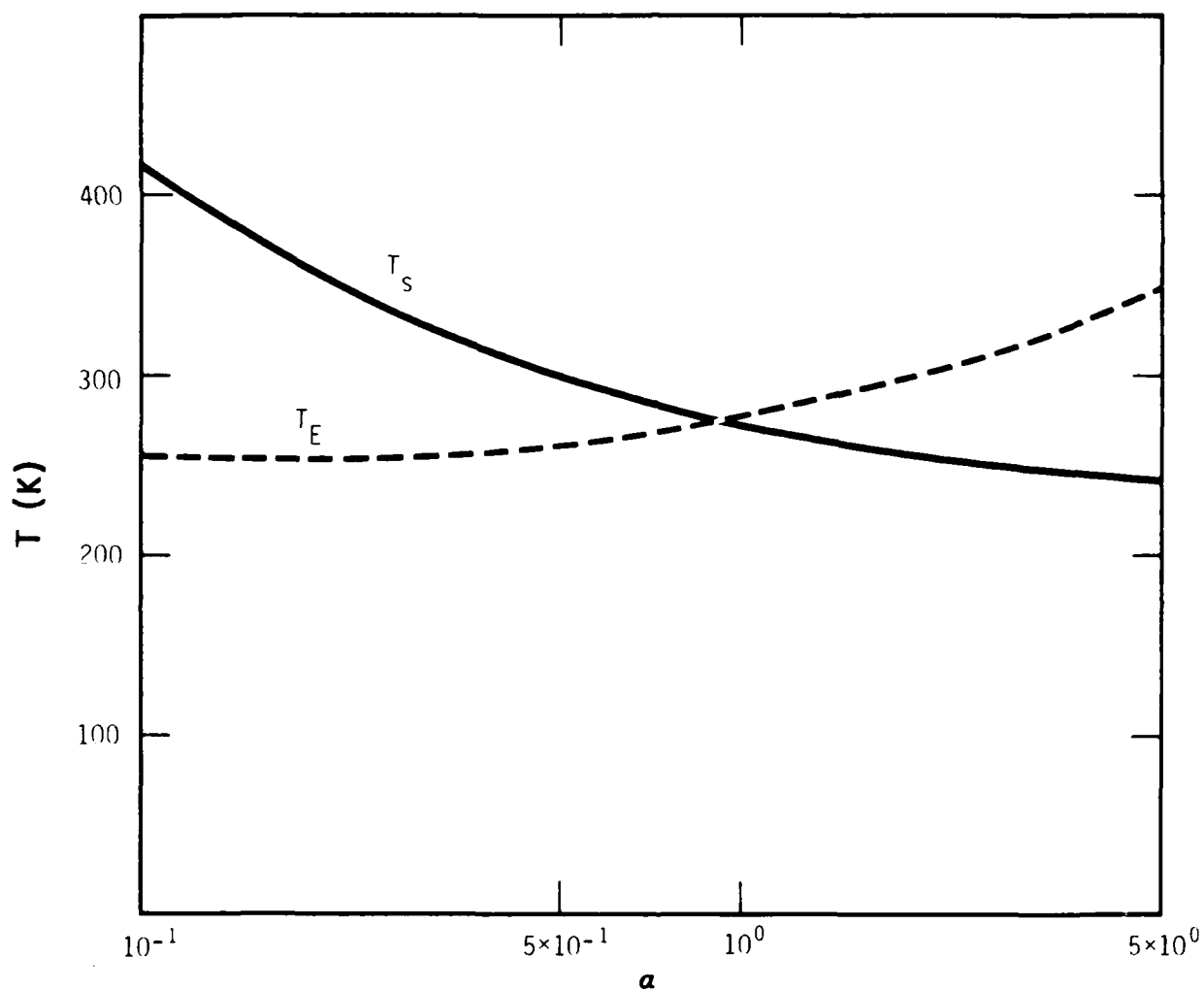


Figure 3-2. The temperature at the earth's surface,  $T_E$ , and the temperature at the top of the soot layer,  $T_S$ , plotted vs.  $\alpha$ . Convective instabilities are ignored in these calculations.

vapor present such that the value of  $\alpha$  for the mixture will not fall below .1; to raise the value of  $\alpha$  to something greater than one would require the presence of absorbers which are more effective in the IR than they are in the solar. The likely candidates for such absorbers are hydrocarbon vapors, water vapor and condensed water (clouds).

By looking at Fig. 3-2 we can see that to make an appreciable change in the temperature structure we must change  $\alpha$  by at least .1 or more; at the NRC value of .25 a change of .1 in  $\alpha$  would lead to a 3K change in  $T_E$  and a 17K change in  $T_S$ . For the NRC range of values for pure soot ( $.1 < \alpha < 1$ ) we see that the temperature of the earth ranges from 251K to 278K while the temperature at the top of the layer ranges from 413K to 272K. While convective instabilities, discussed below, will alter these ranges, particularly the range for the top of the layer, somewhat, the variation implied by the uncertainties in the properties of the soot alone is substantial and studies to determine these properties with less uncertainty are clearly warranted.

The information on hydrocarbon emissions given in section 2 along with the information on the IR properties of the hydrocarbons, especially Fig. 2-3 makes it clear that hydrocarbon emission cannot change  $\alpha$  by an amount nearly as large as .1. The most important hydrocarbon is probably the ethylene although the acetylene appears to be stronger in Figure 2-3. The reason for the enhanced importance of ethylene is that most of its emission lies in the window where water vapor is transparent while the overlap between water vapor and acetylene will partly cancel the importance of the acetylene. Even if we ignore any questions of overlap we see that the total of all the additional hydrocarbons is only about equal in IR emissivity to the ambient methane. To estimate the effects of these gases on the temperature structure we recall that the optical depth of the visible is taken to be 2. Since the soot and the additional hydrocarbons came from the same source (the fires) they must be approximately uniformly mixed. Thus we find that  $\alpha$  is given by



$$\alpha = \frac{\text{optical depth in the IR}}{2}$$

The IR optical depth of the soot is .5; the change in  $\alpha$  due to the hydrocarbons is

$$\Delta\alpha = \frac{\text{IR optical depth of the hydrocarbons}}{2}$$

The IR optical depth of the hydrocarbons assuming no overlap is about  $2 \times 10^{-2}$  which gives

$$\Delta\alpha_{\text{hydrocarbons}} = .01$$

The specific optical depths we have been using assume a particular distribution of the soot and hydrocarbons over the earth's surface.  $\alpha$  and  $\Delta\alpha$  will, however, be approximately independent of this assumption since if the hydrocarbons are concentrated due to patchiness the soot will be also. Even if there were to exist some mechanism whereby the hydrocarbons were ten times as concentrated as the soot the effect of the hydrocarbons would have only a marginal effect on the temperature structure. We conclude that the "greenhouse" effect of the hydrocarbons cannot significantly counteract the "anti-greenhouse" effect of the soot.

Much the same situation is encountered in the case of  $\text{CO}_2$  as was found in the case of the hydrocarbons. According to the discussion which can be found in Chapter 2 the amount of  $\text{CO}_2$  added to the atmosphere by the fires is small compared with the amount in the ambient atmosphere. Furthermore the ambient  $\text{CO}_2$  is mixed nearly uniformly over the portion of the atmosphere which is affected by the soot so the blasts and fires will not cause an appreciable redistribution of the  $\text{CO}_2$ . Thus the IR optical depth of the  $\text{CO}_2$  will be the ambient value of about .004 which is not enough to change  $\alpha$  by an appreciable amount.

In the case of  $\text{NO}_2$  it is the value of  $\mu_{I_1}$ , rather than  $\alpha$ , which is most likely to be affected. Much of the  $\text{NO}_2$  created by the blasts will be carried to altitudes where it will remain above the soot. Figure 2-1 shows that if the high altitude  $\text{NO}_2$  is distributed more or less uniformly its contribution to  $\mu_{I_1}$  will be less than the contribution we have assumed for water vapor by a factor of twenty; thus, even for relatively concentrated patches the  $\text{NO}_2$  will not have a major effect on the temperature.

The question of the effects of water vapor is much more complicated. One reason is that the water vapor has a much greater chance of being important so we cannot perform a quick calculation and dismiss it. Another reason is that the ambient water vapor is not uniformly distributed over the part of the atmosphere where the soot is found (it is concentrated at the lower altitudes) so the redistribution of the ambient water vapor in addition to the addition of new water vapor must be considered. A final complication is that the absorption coefficient of water vapor has a complicated behavior as a function of frequency across the IR band whereas our simple calculations treat it as constant. To correct this last problem we should keep more IR groups (the absorption coefficient of water vapor can be well approximated by four IR groups) which would considerably complicate our formalism. We shall instead observe that optical depths on the order of one are the ones important to us and water vapor has an effective absorption coefficient of about  $1 \text{ cm}^2/\text{g}$  in this range. More complicated calculations using more than one IR group have confirmed that this procedure is sufficient to our needs.

Estimating the amount of water vapor which will be mixed with the smoke is a difficult problem. We first consider the water released by the combustion process. According to the NRC most combustible materials generate about  $1 \text{ g-H}_2\text{O/g-burned}$ ; the emission factor for the soot is about  $.02\text{g/g}$ . However, the absorption coefficient for the soot in the visible

$(2 \times 10^4 \text{ cm}^2/\text{g})$  is  $2 \times 10^4$  larger than the one we are assuming for water vapor in the IR. Thus the increment in  $\alpha$  due to the water of combustion is only .0025.

While the water of combustion is not sufficient to significantly change the value of  $\alpha$  the atmospheric water vapor redistributed by the fire plumes is much greater. The NRC estimates that a total of 40,000 Tg of water would probably be drawn into the fire plumes with an upper-limit estimate of 500,000 Tg. Since the estimate for the total soot content is 180 Tg these numbers correspond to changes in  $\alpha$  of .011 and .14 respectively. The latter number is just at the borderline where significant changes in the phenomenon might be observed. Even if the smaller number for the total entrained water is correct, which is likely the case, the water vapor will undoubtedly be distributed very unevenly depending on the particular location and also depending on the time of year of the event. In spite of these reservations we believe that water vapor will not make a significant impact on the nuclear winter phenomenon by causing an appreciable change in  $\alpha$ . Even the extreme amounts of water vapor seem to fall just short of being enough.

We thus come finally to the question of the possible effect on  $\alpha$  of condensed water. For condensed water one problem we had for water-vapor is removed: the strong dependence of the IR absorption coefficient on frequency; the absorption coefficient of water clouds is quite constant as a function of frequency. It does depend on the drop size distribution. For the size distribution of Figure 2-5 we find an absorption coefficient of  $890 \text{ cm}^2/\text{g}$ ; for that of Figure 2-6 we find  $730 \text{ cm}^2/\text{g}$ ; we have seen values as high as  $2.2 \times 10^3 \text{ cm}^2/\text{g}$  for naturally occurring clouds quoted in the literature. We shall adopt a value of  $800 \text{ cm}^2/\text{g}$  for the moment. If we take the NRC's estimate for the most likely amount of entrained water, 40,000 Tg, we find a ratio of water mass to soot mass of 220. If all the water condensed out we would find a value of  $\alpha$  of 9.

We thus see that if any appreciable portion of the water condenses out it will have a dominant effect on  $\alpha$ . It will also have a significant effect on  $A_2$  the albedo of the cloud-soot layer. From Table C-5 we see that if the ratio of water to soot is 200 to 1 the albedo will be about .26 while if it is 100 to 1 the albedo will be about .18; if the ratio is 50 to 1 which would correspond to a value of  $\alpha$  of about 2.5 the albedo is about .12. (Note that the optical depth shown in the table is for scattering and absorption; we are interested in an absorption optical depth of 2 which requires about  $10^{-4}$  g/cm<sup>2</sup> of soot.) In Figure 3-3 we plot  $T_s$  and  $T_E$  as given by Equations (3-9) and (3-10) using the value of  $A_2$  given in Table C-5 (recall that convective instabilities were ignored in deriving these equations).

Water clouds, if they are present, have the potential to play a dominant role in the nuclear winter phenomenon. Furthermore clouds typically do form in fire plumes and once the cloud forms its presence keeps the top of the cloud cold which keeps the cloud there. We believe that the calculations just presented indicate that water clouds cannot be ignored and warrant further study; their temperatures given in Figure 3-3 cannot be considered realistic due to the fact we have ignored the effects of convective instabilities. Convective instabilities will be triggered once  $\alpha$  becomes greater than 1 by any appreciable amount (something less than 1.2 for typical conditions). Having convinced ourselves that  $\alpha$  might be raised to such values by the presence of clouds we shall now proceed to incorporate convection instabilities into our calculations.

### THE EFFECTS OF CONVECTIVE INSTABILITIES

Up to this point we have been ignoring the fact that if the derivative of the atmospheric temperature with respect to  $z$  (recall that we are taking the direction of positive  $z$  to be downward) exceeds some value the lower hotter air will rise spontaneously and convection will set in. We shall take the critical value for the derivative to be 7K/Km, the

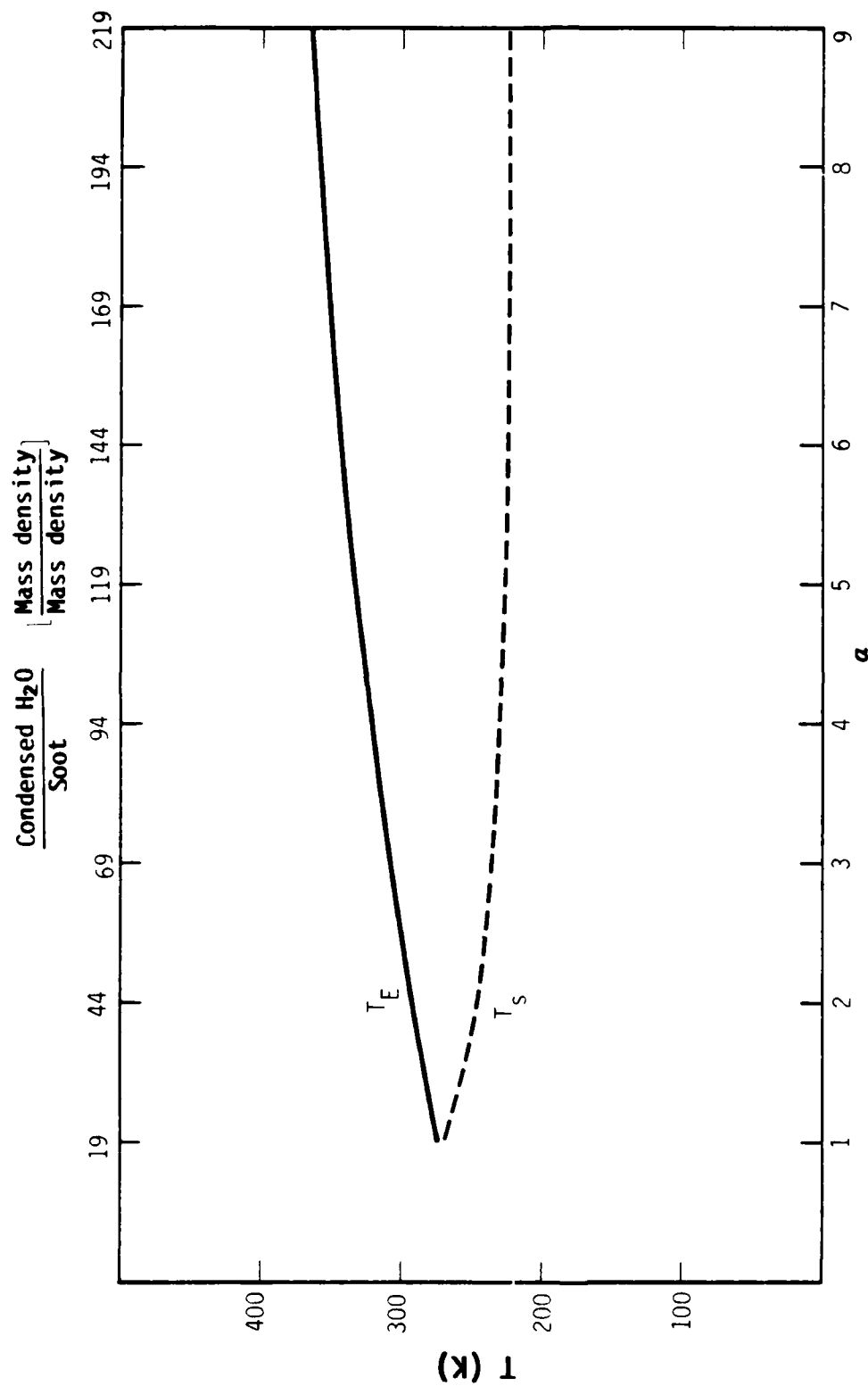


Figure 3-3. The temperature at the earth's surface,  $T_E$ , and the temperature at the top of the soot layer,  $T_S$ , plotted vs.  $\alpha$  and vs. the ratio of cloud mass to soot mass. Convective instabilities are ignored in this calculation.

dry adiabatic lapse rate, and shall not in this report attempt to correct for condensation.

From the formula which gives the temperature in the cloud-soot layer (Equation D-2) we calculate the derivative of the temperature in that layer to be:

$$\frac{dT}{dz} = \left[ \frac{(1-A_1)(1-A_2)\epsilon}{2\sigma} \right]^{1/4} \frac{.25 \epsilon_{s_2} \left( \alpha - \frac{1}{\alpha} \right) e^{-\epsilon_{s_2} z}}{\left[ \left( \frac{1}{\alpha} - \alpha \right) e^{-\epsilon_{s_2} z} + 1 + \mu_{I_1} \right]^{3/4}} \quad (3-11)$$

where  $z$  is zero at the top of the cloud-soot layer and increases as we proceed deeper into the layer. The maximum value of  $\frac{dT}{dz}$  is at  $z=0$  where the value is

$$\left. \frac{dT}{dz} \right|_{z=0} = \left[ \frac{(1-A_1)(1-A_2)\epsilon}{2\sigma} \right]^{1/4} \frac{.25 \epsilon_{s_2} \left( \alpha - \frac{1}{\alpha} \right)}{\left[ \frac{1}{\alpha} + 1 + \mu_{I_1} \right]^{3/4}} \quad (3-12)$$

If we assume that the total optical depth in the solar of 2 is spread over 4 Km of altitude  $\epsilon_{s_2}$  will be  $.5 \text{ Km}^{-1}$ . For typical values of the other parameters we find that the temperature profile will be unstable for values of  $\alpha$  greater than about 1.2. For a value of  $\alpha$  of 4 the region  $z < 3.2 \text{ Km}$  has a gradient larger than  $7 \text{ K/Km}$ .

The details of the way the unstable temperature profile is relieved by convection to become stable will depend on the way in which the instability develops and on the character of the atmosphere above the cloud-soot layer. Under the assumptions we have been making the temperature in layer 1 is nearly constant so that layer is quite stable.

If the cloud-soot layer mixes with the air above it the value of  $\alpha$  would remain unchanged but the individual opacities,  $\epsilon_{s_2}$  and  $\epsilon_{I_2}$  would

be reduced; that would lead to a smaller gradient in the temperature and a more stable profile as can be seen by examination of Equation (3-12). If the convection is confined to occur entirely within the cloud-soot layer the values of  $\alpha$  and the opacities will be unchanged. Since our goal here is to estimate the potential effects of the convection on the temperature profile, and the assumption that the convection takes place entirely within the layer will provide the maximum effect on that profile, we shall assume that the convection takes place within the layer.

We seek a solution of the form shown in Figure 3-4. At the top of the cloud-soot layer there is a convection zone in which the temperature gradient is 7K/Km. Below the convection region are stable layers of the type we have been studying. The solution to the problem will be determined such that the depth of the mixing layer is the smallest it can be and still allow us to satisfy the following requirements: the radiation transport equations are satisfied in all regions; energy conservation is produced by a physically realizable convective flux in the convection zone. This last requirement amounts to insisting that the convective flux necessary to conserve energy in the convection zone must vanish at the top and bottom of the zone.

In addition to the solutions already obtained we shall need the solution to Equations (3-2) except with the last of these replaced by the specification of the temperature gradient:

$$\begin{aligned}
 \frac{dS}{dz} &= -\epsilon_{s2} S \\
 \frac{dU}{dz} &= \epsilon_{I2} U - \epsilon_{I2} \sigma T^4 \\
 \frac{dD}{dz} &= -\epsilon_{I2} D + \epsilon_{I2} \sigma T^4 \\
 T &= T_0 + \mu z
 \end{aligned}
 \tag{3-13}$$

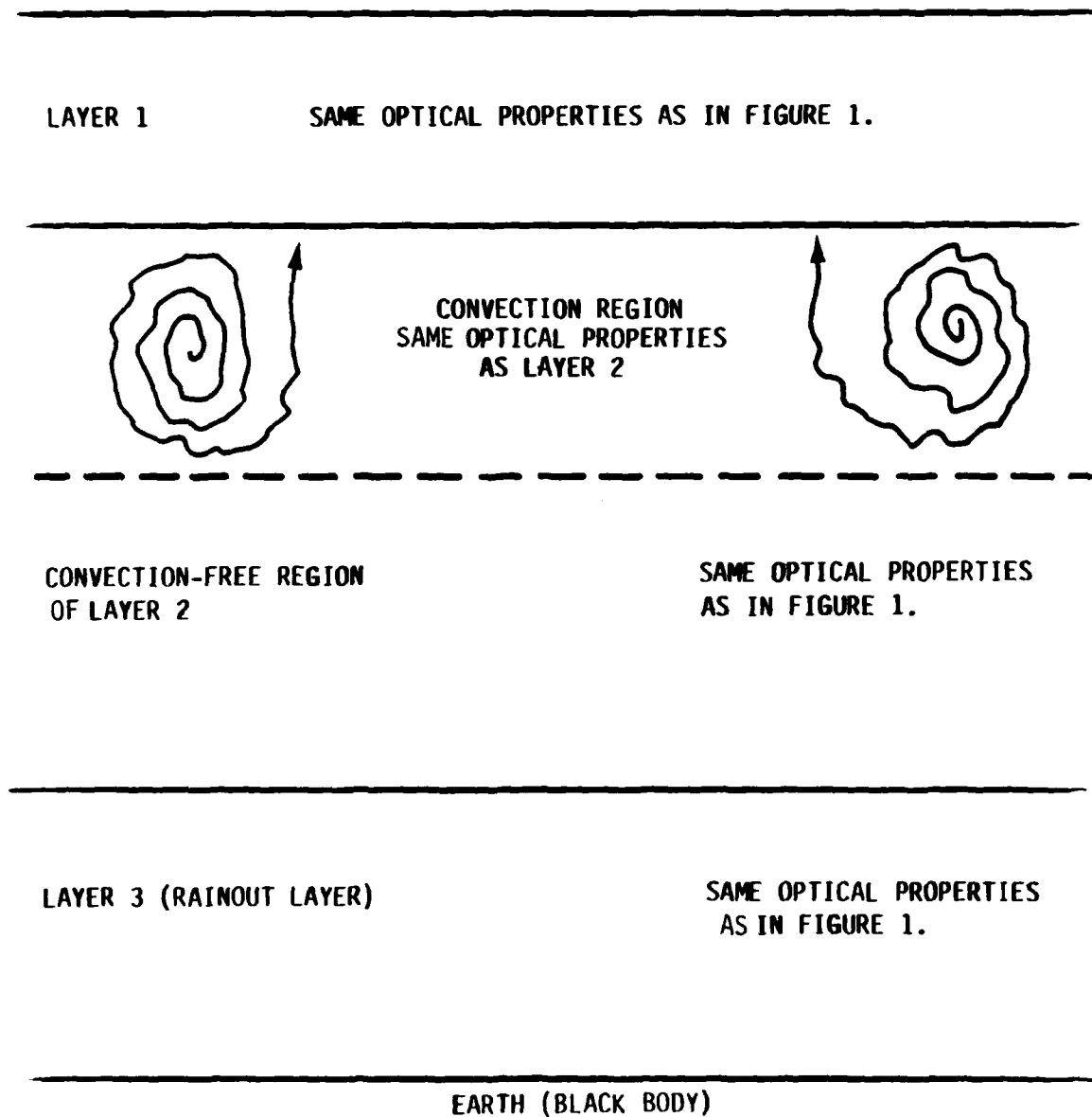


Figure 3-4. Schematic of the model nuclear winter with a convection region at the top of the cloud-soot layer.



where  $T_0$  is the temperature at  $z=0$  (the top of the cloud-soot layer) and we shall take  $\beta$  to be 7K/Km. We define a new independent variable to be

$$y = T_0 + \beta z \quad (3-14)$$

which is just the temperature. The equations become

$$\begin{aligned} \frac{dS}{dy} &= -\frac{\epsilon_{s_2}}{\beta} S \\ \frac{dU}{dy} &= \frac{\epsilon_{I_2}}{\beta} U - \frac{\epsilon_{I_2}}{\beta} \sigma y^4 \\ \frac{dD}{dy} &= -\frac{\epsilon_{I_2}}{\beta} D + \frac{\epsilon_{I_2}}{\beta} y^4 \end{aligned} \quad (3-15)$$

The general solution to these equations is

$$\begin{aligned} S &= (1-A_1)(1-A_2) \Sigma e^{\frac{\epsilon_{s_2} T_0}{\beta} - \frac{\epsilon_{s_2}}{\beta} y} = (1-A_1)(1-A_2) \Sigma e^{-\epsilon_{s_2} z} \\ U &= \sigma \left[ y^4 + 4 \frac{\beta}{\epsilon_{I_2}} y^3 + 12 \left( \frac{\beta}{\epsilon_{I_2}} \right)^2 y^2 + 24 \left( \frac{\beta}{\epsilon_{I_2}} \right)^3 y + 24 \left( \frac{\beta}{\epsilon_{I_2}} \right)^4 \right] + C_1 e^{\frac{\epsilon_{I_2}}{\beta} y} \\ D &= \sigma \left[ y^4 - 4 \frac{\beta}{\epsilon_{I_2}} y^3 + 12 \left( \frac{\beta}{\epsilon_{I_2}} \right)^2 y^2 - 24 \left( \frac{\beta}{\epsilon_{I_2}} \right)^3 y + 24 \left( \frac{\beta}{\epsilon_{I_2}} \right)^4 \right] + C_2 e^{-\frac{\epsilon_{I_2}}{\beta} y} \end{aligned} \quad (3-16)$$

Let  $F$  be the flux of convective energy in the convection zone.  $F$  must be zero at the top of the cloud-soot layer and at the bottom of the convection zone. The conservation of energy requires

$$\epsilon_{s_2} S + \epsilon_{I_2} (U+D) = 2\epsilon_{I_2} \tau + \frac{dF}{dz} \quad (3-17)$$

F is negative throughout the convection zone and is approaching zero at the bottom of it. Therefore  $\frac{dF}{dz}$  must be positive or zero at the bottom of the zone. The radiative fluxes are continuous at the bottom of the zone so if  $\frac{dF}{dz}$  is not zero  $\tau$  must be discontinuous there and must be colder at the bottom of the convection zone than at the top of the convection-free region beneath it; a situation which is unstable. To achieve a stable atmosphere we must therefore have  $\frac{dF}{dz}$  equal to zero at the bottom of the convection zone which is equivalent to having the temperature be continuous there. We now have five conditions which must be satisfied in the convection zone: the continuity of the fluxes U and D at the top of the zone; the vanishing of F at the top and bottom of the zone; and the vanishing of  $\frac{dF}{dz}$  at the bottom of the zone. The unknown parameters associated with the zone are the temperature at the top of the zone,  $T_0$ , the constants  $C_1$  and  $C_2$  in Equation (3-16), the constant of integration which appears when we integrate Equation (3-17) to solve for F, and the depth of the layer. The solution is therefore determined; we do not have the freedom to impose stability criteria on the layer under the convection zone and we must concern ourselves with whether or not our solution will have a stable temperature gradient in that region. We have shown above that the largest temperature gradient in the convection-free region will occur at the interface with the convection zone. Differentiating Equation (3-17) with respect to z we find:

$$\epsilon_{s_2} \frac{dS}{dz} + \epsilon_{I_2} \left( \frac{dU}{dz} + \frac{dD}{dz} \right) = 2\epsilon_{I_2} \frac{d\tau}{dz} + \frac{d^2 F}{dz^2} \quad (3-18)$$

which we can use Equation (3-13) to rewrite (3-18) as:

$$\epsilon_{s_2}^2 S + \epsilon_{I_2}^2 (U - D) = 2\epsilon_{I_2} \frac{d\tau}{dz} + \frac{d^2 F}{dz^2} \quad (3-19)$$

The left hand side of this equation is continuous across the interface.  $F$  is negative throughout the convection zone and both it and its first derivative vanish at the bottom of the convection zone; therefore the second derivative is either negative or zero at the interface. We thus conclude that the gradient of the temperature at the top of the convection-free region is less than or equal to that in the convection zone which is stable by construction so the entire cloud-soot layer is stable.

The radiative fluxes in the convection zone are given by Equation (3-16). We can use Equation (3-13) to rewrite Equation (3-17) as

$$\frac{dF}{dz} = \frac{d}{dz} (-S + U - D) \quad (3-20)$$

which gives

$$F = -S + U - D + C_3 \quad (3-21)$$

where  $C_3$  is an integration constant. To simplify the notation we shall assume that  $\epsilon_{I_1}$  is zero and shall include the albedo of layer 1 into that of layer 2 by defining  $A = (1-A_1)(1-A_2)$ . The boundary conditions at the top of the cloud-soot layer are then:

$$\sigma \left[ T_0^4 + 4 \frac{\beta}{\epsilon_{I_2}} T_0^3 + 12 \left( \frac{\beta}{\epsilon_{I_2}} \right)^2 T_0^2 + 24 \left( \frac{\beta}{\epsilon_{I_2}} \right)^3 T_0 + 24 \left( \frac{\beta}{\epsilon_{I_2}} \right)^4 \right] + C_1 = A\Sigma$$

$$\sigma \left[ T_0^4 - 4 \frac{\beta}{\epsilon_{I_2}} T_0^3 + 12 \left( \frac{\beta}{\epsilon_{I_2}} \right)^2 T_0^2 - 24 \left( \frac{\beta}{\epsilon_{I_2}} \right)^3 T_0 + 24 \left( \frac{\beta}{\epsilon_{I_2}} \right)^4 \right] + C_2 = 0$$

(3-22)

$$-A\Sigma + 8\sigma \left[ \frac{\beta}{\epsilon_{I_2}} T_0^3 + 6 \left( \frac{\beta}{\epsilon_{I_2}} \right)^3 T_0 \right] + C_1 - C_2 + C_3 = 0$$

These equations determine that  $C_3 = 0$ . The boundary conditions at the lower boundary are:

$$\begin{aligned}
 & -A\epsilon e^{-\epsilon s_2 d} + \sigma \left[ 8 \frac{\beta}{\epsilon I_2} (T_0 + \beta d)^3 + 24 \left( \frac{\beta}{\epsilon I_2} \right)^3 (T_0 + \beta d) \right] \\
 & + C_1 e^{\epsilon I_2 d} - C_2 e^{-\epsilon I_2 d} = 0
 \end{aligned}
 \tag{3-23}$$

$$\begin{aligned}
 & \epsilon_{s_2} A\epsilon e^{-\epsilon s_2 d} + \epsilon_{I_2} \sigma \left[ 24 \frac{\beta^2}{\epsilon I_2} (T_0 + \beta d)^2 + 48 \left( \frac{\beta}{\epsilon I_2} \right)^4 \right] \\
 & + \epsilon_{I_2} + C_1 e^{\epsilon I_2 d} + \epsilon_{I_2} C_2 e^{-\epsilon I_2 d} = 0
 \end{aligned}$$

In these equations  $d$  is the depth of the convection zone. By observing that  $T_0$  will be large compared with  $\frac{\beta}{\epsilon I_2}$  one can derive the following approximate solutions to these equations:

$$\begin{aligned}
 T_0 & \approx T_B - \frac{\beta}{\epsilon I_2} \\
 d & \approx - \frac{1}{\epsilon_{s_2}} \ln \frac{88}{T_B(\epsilon_{I_2} + \epsilon_{s_2})}
 \end{aligned}
 \tag{3-24}$$

where we have defined

$$T_B = \left[ \frac{A}{\sigma} \right]^{1/4}$$

We have solved the transcendental Equations (3-22) and (3-23) numerically and find that the approximate solution (3-24) is adequate for our needs, using Equations (3-24) Equations (3-22) provide the values of  $C_1$  and  $C_2$ .

The solution in the convective zone provides the boundary conditions which determine the solution in the layers below it; the full

solution is given in Appendix D. Here we shall focus our attention on the temperature at three points: the top of cloud-soot layer as given by Equation (3-24); the temperature at the bottom of the cloud-soot layer, which we call  $T_L$  and which is given by

$$\tau_L = \frac{1}{2} [2\sigma(T_0 + \beta d)^4 + A\epsilon \left( \frac{\epsilon_{I_2}}{\epsilon_{s_2}} - \frac{\epsilon_{s_2}}{\epsilon_{I_2}} \right) (e^{-\epsilon_{s_2} d} - e^{-\mu_{s_2}})] ; \quad (3-25)$$

and the temperature of the earth,  $T_E$ , given by

$$\tau_E = \frac{1}{2} [2\sigma(T_0 + \beta d)^4 + A\epsilon \left\{ \left( \frac{\epsilon_{I_2}}{\epsilon_{s_2}} - \frac{\epsilon_{s_2}}{\epsilon_{I_2}} \right) e^{-\epsilon_{s_2} d} + e^{-\mu_{s_2}} \left( 1 + \mu_{I_3} - \frac{\epsilon_{I_2}}{\epsilon_{s_2}} \right) \right\}] \quad (3-26)$$

These three temperatures are shown as functions of  $\alpha$  in Figure 3-5 with the assumption that the cloud-soot layer is distributed over 8 Km of altitude.

Comparing the results shown in Figures 3-3 and 3-5 we see that the effect of the convection has been to raise the temperature  $T_s$  and lower the temperature  $T_E$ . The reason we do not show results for values of  $\alpha$  greater than about 5 is that for higher values the depth of the convection zone,  $d$ , becomes larger than the 8 Km we have assumed for the total depth of the cloud-soot layer. Calculations for these cases would require an extension of our methodology. The temperature profile from the top of the cloud-soot layer to the earth's surface is a stable one. The interface between the top of the cloud-soot layer and the air above it is probably unstable. The temperatures at the layer top are around 250K; the temperature just above it is probably somewhat less since the top of the layer is at an altitude of  $\approx 9$ Km. If this instability is present it will cause the top of the layer to rise which in turn will cause the top of the layer to become colder and will increase the surface temperatures. Thus a

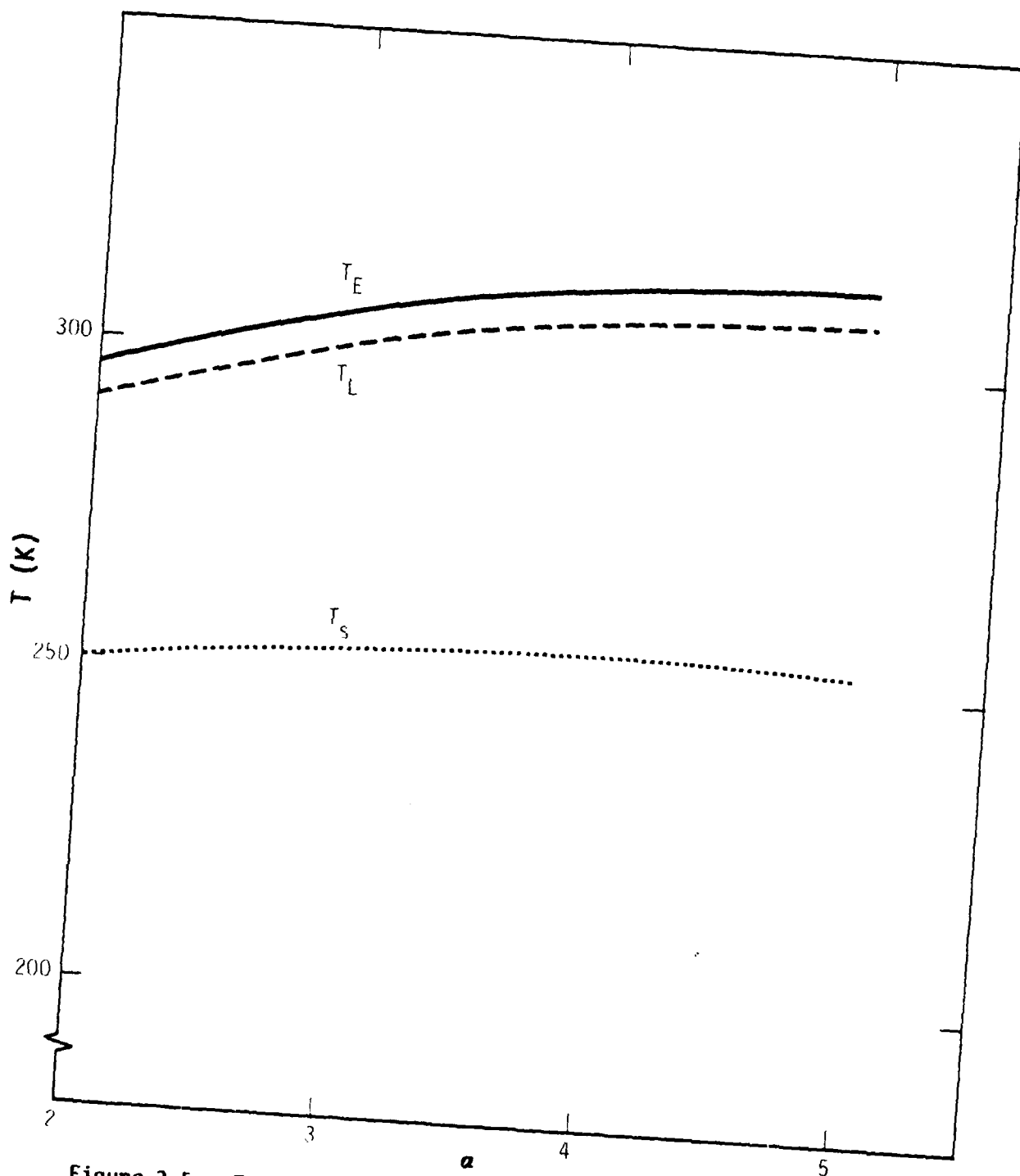


Figure 3-5. The temperature at the earth's surface,  $T_E$ , at the top of the cloud-soot layer,  $T_S$ , and at the bottom of the cloud-soot layer,  $T_L$ , plotted vs.  $\alpha$  assuming convection within the cloud stabilizes the temperature profile.

temperature profile between that predicted by ignoring convective instabilities and that we have calculated by allowing convection only within the cloud-soot layer may be expected.

Another somewhat unrealistic feature of the present calculations is seen in the results for  $T_L$ , the temperature at the bottom of the cloud-soot layer. This quantity is seen, in Figure 3-5, to range from 290K to 310K; it is unlikely that there will be sufficient water to maintain a condensation cloud to such high temperatures and we should assume that the cloud disappears at some temperature which depends on the amount of water present. When the cloud disappears the value of  $\alpha$  will change dramatically, probably falling below 1. Our present methodology can allow for such an effect but we shall postpone such calculations until a more realistic treatment of the interface at the top of cloud-soot layer has been developed.

We should perhaps remark on the comparison between the effects of the cloud-soot layers we have been studying and those of naturally occurring clouds. It may seem strange that either a soot cloud or a water cloud would cool the surface while a mixture of the two would warm the surface. The source of the effect is the difference in the albedos of water clouds and cloud-soot mixtures. Water clouds as heavy as those we have been studying would have albedos in the solar of .8 or more; the presence of the soot lowers this to about .2. Thus while the presence of naturally occurring water clouds leads to an increased IR opacity for the atmosphere, which tends to raise surface temperatures, the high albedo of the clouds tends to lower temperatures throughout the profile; the net effect is slightly lower surface temperatures. The presence of the soot mixed with the cloud allows for the presence of high IR opacity without a high solar albedo.

## NUCLEAR WINTER OVER SNOWPACK

The nuclear winter phenomenon is always warming for the surface if it occurs over snowpack. By this we mean that the snow will ultimately absorb more of the solar energy directed at it if there exists a soot layer, with or without an accompanying water cloud, than it would under clear sky conditions. The reason for this is as follows: the absorption of solar energy by the soot ultimately results in a downwardly propagating IR flux. The magnitude of the IR flux at the surface depends on the opacity structure of the atmosphere but, as we shall see below, it is at least one half the value of the absorbed solar flux. The albedo of the snow in the visible is .8 or more while the snow is very nearly black in the IR. Thus more of the solar energy will be absorbed by the snow if it is first absorbed by the soot than if it propagates unimpeded to the surface.

To study the effect over snowpack we must allow for an upward as well as a downward solar flux. We call these respectively  $S_U$  and  $S_D$ . They satisfy the equations

$$\begin{aligned}\frac{dS_D}{dz} &= -\epsilon_s S_D \\ \frac{dS_U}{dz} &= \epsilon_s S_U\end{aligned}\tag{3-27}$$

All of Equations (3-2) remain valid except the last which becomes:

$$\epsilon_s (S_U + S_D) + \epsilon_I (U + D) - 2\epsilon_I \tau = 0\tag{3-28}$$

the general solution to the system is

$$\begin{aligned}S_D &= A e^{-\epsilon_s z} \\ S_U &= B e^{\epsilon_s z}\end{aligned}\tag{3-29}$$



$$U = \frac{1}{2} (1-\alpha) A e^{-\epsilon s^Z} - \frac{1}{2} (1+\alpha) B e^{\epsilon s^Z} + C(z+1) + E$$

$$D = -\frac{1}{2} (1+\alpha) A e^{-\epsilon s^Z} + \frac{1}{2} (1-\alpha) B e^{\epsilon s^Z} + C(z-1) + E$$

$$\tau = \frac{1}{2} \left( \frac{1}{\alpha} - \alpha \right) (A e^{-\epsilon s^Z} + B e^{\epsilon s^Z}) + Cz + E$$

where A, B, C and E are constants. We shall consider the same model shown in Figure 1, with the same values for the parameters we used earlier, except that we shall assume that the earth has an albedo to solar radiation of .8. The solar fluxes can be solved for independently of the IR fluxes; the solution is given in Appendix D. Here we shall concentrate on the temperature at the surface. The temperature with all the layers present is given by:

$$\tau_E = \frac{1}{2} \{ (1+\mu_{I_3}) (S_{D_3} e^{-\mu s_2} - S_{U_3} e^{\mu s_2}) + \alpha [ (1-e^{-\mu s_2}) S_{D_3} + (1-e^{\mu s_2}) S_{U_3} ] + S_N (1+\mu_{I_1}) \} \quad (3-30)$$

where 
$$S_{D_3} = \Sigma \left\{ (1-A_1)(1-A_2) + \frac{(1-A_1)(1-A_2)^2 A_1 A_e e^{-2\mu s_2}}{1 - A_2 A_e - A_1 A_e (1-A_2) e^{-2\mu s_2}} \right\}$$

$$S_{U_3} = \Sigma \left\{ A_1 + A_2 - A_1 A_2 + \frac{(1-A_1)(1-A_2)^2 A_e e^{-2\mu s_2}}{1 - A_2 A_e - A_1 A_e (1-A_2) e^{-2\mu s_2}} \right\} \quad (3-31)$$

$$S_N = \Sigma \left\{ 1-A_1 - A_2 + A_1 A_2 - \frac{(1-A_1)^2 (1-A_2)^2 A_e e^{-2\mu s_2}}{1 - A_2 A_e - A_1 A_e (1-A_2) e^{-2\mu s_2}} \right\}$$

where  $A_e$  is the albedo of the earth.

To render these expressions somewhat more transparent we shall assume that layer 1 is missing (it does little anyway) and that  $A_2$  is zero (it is always small and is very small for a soot layer with no water cloud). We get

$$\tau_E = \frac{1}{2} \Sigma [1 - A_e e^{-2\mu s_2} + (1 - A_e)(1 + \mu_{I_3})e^{-\mu s_2} + \alpha (1 - e^{-\mu s_2})(1 + A_e e^{-\mu s_2})] \quad (3-32)$$

For clear sky condition we get

$$\tau_{EC} = (1 - A_e) \Sigma \quad (3-33)$$

The change is thus

$$\Delta \tau_E = \frac{1}{2} \Sigma [(1 - e^{-2\mu s_2}) \{ (2A_e - 1) + \alpha(1 + A_e e^{-\mu s_2}) \} + \mu_{I_3}(1 - A_e)e^{-2\mu s_2}] \quad (3-34)$$

As long as  $A_e > .5$   $\Delta \tau_E$  is always positive, even if  $\alpha$  and  $\mu_{I_3}$  are zero. Perhaps a better comparison is between the conditions with layers 2 and 3 present (the nuclear winter condition) with those for layer 3 alone (the normal troposphere). For that case it is not quite guaranteed that the soot cloud will lead to warming although it will be for most conditions expected to be encountered. If only layer 3 is present we get

$$\tau_{E_a} = \frac{1}{2} \Sigma (1 - A_e) [2 + \mu_{I_3}] \quad (3-35)$$

Comparing this formula with Equation (3-32) we see that

$$\Delta \tau = \frac{1}{2} \Sigma [(1 - e^{-2\mu s_2}) (2A_e - 1 - \mu_{I_3}(1 - A_e) + \alpha(1 + A_e e^{-\mu s_2}))] \quad (3-36)$$

This quantity is positive unless  $\alpha$  is very small and  $\mu_{I_3}$  is very large. The reason that  $\Delta\tau$  can be negative is that the soot layer reduces the effectiveness of the tropospheric layer. In spite of this  $\Delta\tau$  will be positive unless  $\mu_{I_3}$  is very large (greater than 3) and  $\alpha$  is near zero. If a water cloud is present along with the soot it will probably melt the snow; if we assume that the optical depth in the solar is 2, Equation (3-32) predicts melting of the snow if  $\alpha$  is greater than .77. Thus even if the effective solar flux is considerably below our assumed value, which will probably be the case since we are presumably dealing with winter conditions or quite high latitudes, the values of  $\alpha$  associated with soot-water cloud mixtures would in most cases be high enough to melt the snow.

The importance of the fact that the nuclear winter phenomenon is warming over snow pack is difficult to access. The fact that the regions of snowpack will be warmer than normal might alter normal circulation patterns. Whether that would occur and, if it did, what the consequences would be are questions beyond the scope of the present study.

## SECTION 4

### CONCLUSIONS

The principal conclusions of the present study pertain to the possible importance of various IR radiators on the nuclear winter phenomenon. We find that hydrocarbons,  $\text{CO}_2$  and  $\text{NO}_2$  will not have a major impact on the phenomenon. Water vapor will have at most a marginal effect on the temperature profile if convective instabilities are ignored; water vapor may be important to the development of the instability which will exist at the top of the soot layer if no condensation cloud is present. Condensed water has the potential to play a major, perhaps dominant role in the nuclear winter phenomenon.

If water clouds are present at late times they will probably alter the entire character of the temperature profile, changing it from one which is hot at the cloud top and cold at the earth's surface to one which is cold at the top and hot at the earth's surface. The amount of water needed to produce such clouds is well within the bounds of what might reasonably be expected to be entrained into the fire plumes. If a cloud exists at the top of the soot layer the temperature is cold there and the cloud tends to persist. If the top of the soot layer is cloud-free the temperature is hot there and clouds will form, if at all, only at lower altitudes where they have a much smaller effect on the temperature profile. This hysteresis effect greatly complicates the analysis as to whether or not a condensation cloud will be present. To analyze the problem one must calculate the development of the plumes, many of which will be cloud topped, some of which may not be, as they spread and merge to form the hemisphere-wide layer. The condensation clouds will probably

affect this merging process. If they survive to later times they may have a profound effect on the phenomenon. The models we have described in this report form a framework in which one may think about the problem and they provide a starting point from which to develop the much more detailed calculations which will be necessary. Performing sufficiently complete calculations in the necessary detail presents a challenge.

## SECTION 5

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## APPENDIX A

### BROAD-BAND EMISSIVITY FOR OPTICALLY-THIN BANDS

If a band model, or the spectral absorption coefficient for an infrared molecular band,  $\nu_i$ , is unavailable, but the integrated band intensity,  $S_i$ , is known, then one can still obtain the broad-band infrared emissivity for the band in the optically-thin case. This is easily demonstrated as follows.

If  $\epsilon_i(\tilde{\nu})$  is the spectral emissivity of a layer at wavenumber  $\tilde{\nu}$  within band  $\nu_i$ , and  $B(\tilde{\nu})$  is the Planck function, then the broad-band emissivity for the band is defined as

$$\overline{\epsilon}_i = \frac{\int_{\text{band}} \epsilon_i(\tilde{\nu}) B(\tilde{\nu}) d\tilde{\nu}}{\int_0^\infty B(\tilde{\nu}) d\tilde{\nu}} \quad . \quad (\text{A-1})$$

But  $\epsilon_i(\tilde{\nu})$  is related to the spectral transmissivity,  $T_i(\tilde{\nu})$ , by the relation

$$\epsilon_i(\tilde{\nu}) = 1 - T_i(\tilde{\nu}) \quad . \quad (\text{A-2})$$

However, in the optically-thin case,

$$T_i(\tilde{\nu}) \approx e^{-k\tilde{\nu}U} \approx 1 - k\tilde{\nu}U \quad (\text{A-3})$$

where  $k\tilde{\nu}$  is the linear absorption coefficient ( $\text{atm}^{-1} \text{ cm}^{-1}$ ) for band  $\nu_i$  and  $U$  is the path length ( $\text{atm cm}$ ) through the absorber. Thus, in this case,

$$\epsilon_i(\tilde{\nu}) \approx k_{\tilde{\nu}} U \quad (A-4)$$

Consequently, because the Planck function generally varies slowly over a molecular band, we can write

$$\int_{\text{band}} \epsilon_i(\tilde{\nu}) B(\tilde{\nu}) d\tilde{\nu} \approx B(\tilde{\nu}_i) U \int_{\text{band}} k_{\tilde{\nu}} d\tilde{\nu} \quad (A-5)$$

where  $\tilde{\nu}_i$  is the band-center wavenumber. Furthermore, by definition of the integrated band intensity,

$$S_i \equiv \int_{\text{band}} k_{\tilde{\nu}} d\tilde{\nu} \quad (A-6)$$

and we thus obtain, from Equations A-1, A-5, and A-6,

$$\bar{\epsilon}_i \approx \frac{B'(\nu_i) S_i U}{\int_0^{\infty} B'(\tilde{\nu}) d\tilde{\nu}} \quad (A-7)$$

where

$$B'(\tilde{\nu}) = \frac{\tilde{\nu}^3}{e^{1.435\tilde{\nu}/T} - 1} \quad (A-8)$$

But, integration of A-8 yields

$$\int_0^{\infty} B'(\tilde{\nu}) d\tilde{\nu} = 1.53 T^4 \quad (A-9)$$

and so

$$\bar{\epsilon}_i \approx 1.53 B'(\tilde{\nu}_i) S_i U / T^4 \quad (A-10)$$

## APPENDIX B

### BROAD-BAND EMISSIVITY FOR TWO SPECIES WITH OVERLAPPING BANDS

If we have a layer composed of two different species whose absorption bands partially overlap, then the broad-band emissivity of the layer is less than the sum of the broad-band emissivities for the individual species. This result is proved as follows.

Let  $T_1(\tilde{\nu})$  and  $T_2(\tilde{\nu})$  be the spectral transmissivities for species 1 and 2, respectively. Suppose that an absorption band for species 1 lies between wavenumbers 0 and  $\tilde{\nu}_2$  and, for species 2, an absorption band lies beyond wavenumber  $\tilde{\nu}_1$ , where  $\tilde{\nu}_1 < \tilde{\nu}_2$ . Then, for  $0 \leq \tilde{\nu} \leq \tilde{\nu}_1$ , only species 1 absorbs; for  $\tilde{\nu}_1 \leq \tilde{\nu} \leq \tilde{\nu}_2$ , both species absorb; for  $\tilde{\nu} \geq \tilde{\nu}_2$ , only species 2 absorbs.

For simplicity, define a normalized Planck function,  $B(\tilde{\nu})$ , such that

$$\int_0^{\infty} B(\tilde{\nu}) d\tilde{\nu} = 1 \quad . \quad (B-1)$$

Then the broad-band transmissivity of the layer, composed of the two species, is defined as

$$\bar{T} = \int_0^{\infty} T_1(\tilde{\nu}) T_2(\tilde{\nu}) B(\tilde{\nu}) d\tilde{\nu} \quad . \quad (B-2)$$

But, considering the absorption regions described above, Equation B-2 can be written as

$$\bar{T} = \int_0^{\tilde{\nu}_1} T_1(\tilde{\nu})B(\tilde{\nu})d\tilde{\nu} + \int_{\tilde{\nu}_1}^{\tilde{\nu}_2} T_1(\tilde{\nu})T_2(\tilde{\nu})B(\tilde{\nu})d\tilde{\nu} + \int_{\tilde{\nu}_2}^{\infty} T_2(\tilde{\nu})B(\tilde{\nu})d\tilde{\nu} \quad (B-3)$$

If  $\bar{T}_1$  is the broad-band transmissivity of the layer if only species 1 were present, and  $\bar{T}_2$  is the transmissivity if only species 2 were present, then

$$\begin{aligned} \bar{T}_1 &= \int_0^{\infty} T_1(\tilde{\nu})B(\tilde{\nu})d\tilde{\nu} \\ &= \int_0^{\tilde{\nu}_1} T_1(\tilde{\nu})B(\tilde{\nu})d\tilde{\nu} + \int_{\tilde{\nu}_1}^{\tilde{\nu}_2} T_1(\tilde{\nu})B(\tilde{\nu})d\tilde{\nu} + \int_{\tilde{\nu}_2}^{\infty} B(\tilde{\nu})d\tilde{\nu} \end{aligned} \quad (B-4)$$

and

$$\begin{aligned} \bar{T}_2 &= \int_0^{\infty} T_2(\tilde{\nu})B(\tilde{\nu})d\tilde{\nu} \\ &= \int_{\tilde{\nu}_1}^{\tilde{\nu}_2} T_2(\tilde{\nu})B(\tilde{\nu})d\tilde{\nu} + \int_{\tilde{\nu}_2}^{\infty} T_2(\tilde{\nu})B(\tilde{\nu})d\tilde{\nu} + \int_0^{\tilde{\nu}_1} B(\tilde{\nu})d\tilde{\nu} \end{aligned} \quad (B-5)$$

Equations B-3 to B-5 can now be combined to yield

$$\bar{T} = \bar{T}_1 + \bar{T}_2 + \int_{\tilde{\nu}_1}^{\tilde{\nu}_2} [T_1(\tilde{\nu})T_2(\tilde{\nu}) - T_1(\tilde{\nu}) - T_2(\tilde{\nu})] B(\tilde{\nu})d\tilde{\nu} - \int_0^{\tilde{\nu}_1} B(\tilde{\nu})d\tilde{\nu} - \int_{\tilde{\nu}_2}^{\infty} B(\tilde{\nu})d\tilde{\nu} \quad (B-6)$$

But, since

$$T_1 T_2 - T_1 - T_2 = (1-T_1)(1-T_2) - 1 \quad , \quad (B-7)$$

and, in view of the normalization B-1, Equation B-6 can be written as

$$\bar{T} = \bar{T}_1 + \bar{T}_2 - 1 + \int_{\tilde{\nu}_1}^{\tilde{\nu}_2} [1-T_1(\tilde{\nu})][1-T_2(\tilde{\nu})]B(\tilde{\nu})d\tilde{\nu} \quad . \quad (B-8)$$

Equation B-8 can be expressed, alternatively, in terms of the broad-band emissivities, by noting that both the spectral and broad-band emissivities,  $\epsilon$ , are related to the spectral and broad-band transmissivities,  $T$ , through the relation

$$\epsilon = 1 - T \quad . \quad (B-9)$$

We thus obtain the result

$$\bar{\epsilon} = \bar{\epsilon}_1 + \bar{\epsilon}_2 - \int_{\tilde{\nu}_1}^{\tilde{\nu}_2} \epsilon_1(\tilde{\nu})\epsilon_2(\tilde{\nu})B(\tilde{\nu})d\tilde{\nu} \quad (B-10)$$

where  $\bar{\epsilon}_1$  and  $\bar{\epsilon}_2$  are the broad-band emissivities of the layer with only species 1 and 2, respectively, present.

This proves that the broad-band emissivity for the mixture is less than the sum of the individual emissivities by the average cross product of the two emissivities in the region of band overlap. Although we have made no attempt to prove that this result is valid for an arbitrary number of different species, we see no reason to doubt that when band overlap occurs, the broad-band emissivity is always less than the sum of the individual emissivities.

## APPENDIX C

### TABULATIONS OF OPTICAL PROPERTIES

Presented here are tabulations of the complex index of refraction, especially for the infrared (IR) region, used in the Mie-code calculations reported in Section 2. Detailed tabular results are also presented of the emissivity, transmissivity, and reflectivity of sooty water clouds, both for broad-band IR thermal radiation and for visible ( $\lambda = 0.55 \mu\text{m}$ ) radiation.

Tables C-1 to C-3 give, respectively, the real and imaginary components of the complex index of refraction ( $n = n_R - in_I$ ) for water, dust (basaltic glass), and soot (carbon). Table C-4 gives the broad-band IR properties of sooty water clouds for parametric values of the water-to-soot density ratio,  $\rho^W/\rho^S$ , and the cloud thickness  $U(\text{gm cm}^{-2})$ . Table C-5 gives corresponding results for radiation of wavelength  $0.55 \mu\text{m}$ , and includes as well the optical depth,  $\tau$ , of the cloud. The log-normal distribution parameters used for Tables C-4 and C-5 are those for water (1) and soot shown in Table 2-6 of Section 2. In all cases the temperature was taken to be  $250^\circ\text{K}$ .

Table C-1. Complex index of refraction values for water (Reference 2-20).

$\lambda$ ( $\mu\text{m}$ )	$n_R$	$n_I$	$\lambda$ ( $\mu\text{m}$ )	$n_R$	$n_I$	$\lambda$ ( $\mu\text{m}$ )	$n_R$	$n_I$
0.200	1.396	$1.10^{-7}$	2.85	1.149	0.185	6.6	1.334	$3.56^{-2}$
0.225	1.373	$4.90^{-8}$	2.90	1.201	0.268	7.0	1.317	$3.20^{-2}$
0.450	1.337	$1.02^{-9}$	2.95	1.292	0.298	9.0	1.262	$3.99^{-2}$
0.475	1.336	$9.35^{-10}$	3.00	1.371	0.272	10.0	1.218	$5.08^{-2}$
0.500	1.335	$1.00^{-9}$	3.10	1.467	0.192	11.5	1.126	0.142
0.725	1.330	$9.15^{-8}$	3.15	1.483	0.135	12.0	1.111	0.199
0.750	1.330	$1.56^{-7}$	3.2	1.478	$9.24^{-2}$	12.5	1.123	0.259
0.775	1.330	$1.48^{-7}$	3.7	1.374	$3.60^{-3}$	13.5	1.177	0.343
0.800	1.329	$1.25^{-7}$	3.8	1.364	$3.40^{-3}$	15.0	1.270	0.402
0.925	1.328	$1.06^{-6}$	3.9	1.357	$3.80^{-3}$	17.5	1.401	0.429
0.950	1.327	$2.93^{-6}$	4.6	1.330	$1.47^{-2}$	28	1.549	0.338
0.975	1.327	$3.48^{-6}$	4.7	1.330	$1.57^{-2}$	30	1.551	0.328
1.00	1.327	$2.89^{-6}$	4.8	1.330	$1.50^{-2}$	32	1.546	0.324
1.20	1.324	$9.89^{-6}$	5.2	1.317	$1.01^{-2}$	38	1.522	0.361
1.40	1.321	$1.38^{-4}$	5.3	1.312	$9.80^{-3}$	40	1.519	0.385
1.60	1.317	$8.55^{-5}$	5.4	1.305	$1.03^{-2}$	42	1.522	0.409
1.80	1.312	$1.15^{-4}$	5.8	1.262	$3.30^{-2}$	50	1.587	0.514
2.00	1.306	$1.10^{-3}$	5.9	1.248	$6.22^{-2}$	60	1.703	0.587
2.20	1.296	$2.89^{-4}$	6.0	1.265	0.107	100	1.957	0.532
2.40	1.279	$9.56^{-4}$	6.1	1.319	0.131	150	2.069	0.495
2.75	1.157	$5.90^{-2}$	6.2	1.363	$8.80^{-2}$	200	2.130	0.504
2.80	1.142	0.115	6.3	1.357	$5.70^{-2}$			

Table C-2. Complex index of refraction values for dust (basaltic glass)  
(Reference 2-21).

$\lambda$ ( $\mu\text{m}$ )	$n_R$	$n_I \times 10^3$	$\lambda$ ( $\mu\text{m}$ )	$n_R$	$n_I \times 10^3$	$\lambda$ ( $\mu\text{m}$ )	$n_R$	$n_I \times 10^3$
3.0	1.52	0.47	11.0	2.2	570.	20.5	1.57	770.
3.1	1.52	0.44	11.5	2.11	340.	21.0	1.66	840.
3.15	1.52	0.42	12.0	2.01	230.	21.5	1.77	890.
3.2	1.52	0.41	12.5	1.93	180.	22.0	1.89	910.
3.5	1.52	0.35	13.0	1.87	160.	22.5	2.00	890.
4.0	1.50	0.37	13.5	1.81	140.	23.0	2.10	850.
4.5	1.50	0.53	14.0	1.77	140.	23.5	2.18	790.
5.0	1.46	1.5	14.5	1.72	140.	24.0	2.24	730.
5.25	1.46	2.7	15.0	1.68	140.	25.0	2.31	590.
6.0	1.4	20.	15.5	1.65	160.	26.0	2.33	480.
6.5	1.36	32.	16.0	1.61	180.	27.0	2.32	390.
7.0	1.3	52.	16.5	1.57	210.	28.0	2.31	330.
7.5	1.21	89.	17.0	1.53	240.	29.0	2.29	280.
8.0	1.11	170.	17.5	1.50	290.	30.0	2.27	240.
8.5	0.98	340.	18.0	1.47	350.	35.0	2.20	140.
9.0	0.96	700.	18.5	1.45	420.	40.0	2.15	97.
9.5	1.26	1100.	19.0	1.45	500.	45.0	2.12	75.
10.0	1.69	1100.	19.5	1.46	590.	50.0	2.11	61.
10.5	2.04	940.	20.0	1.50	690.			



Table C-3. Complex index of refraction values for soot (carbon)  
(Reference 2-19).

$\lambda$ ( $\mu\text{m}$ )	$n_k$	$n_I$	$\lambda$ ( $\mu\text{m}$ )	$n_R$	$n_I$	$\lambda$ ( $\mu\text{m}$ )	$n_R$	$n_I$
4.55	2.99	0.78	6.67	3.04	1.07	12.5	3.07	1.82
4.76	3.00	0.81	7.14	3.05	1.13	14.3	3.05	2.04
5.00	3.01	0.84	7.69	3.06	1.21	16.7	3.02	2.32
5.26	3.01	0.88	8.33	3.06	1.28	20.0	2.94	2.75
5.56	3.02	0.93	9.09	3.06	1.39	25.0	2.75	3.36
5.88	3.03	0.97	10.0	3.07	1.50	33.3	2.30	4.30
6.25	3.03	1.01	11.1	3.07	1.64	50.0	0.10	7.30

Table C-4. Broad-band IR properties of sooty water clouds.

$\rho_{H_2O}/\rho_{soot}$	$U_{H_2O}$ (gm cm <sup>-2</sup> )	$U_{soot}$ (gm cm <sup>-2</sup> )	Emissivity	Transmissivity	Reflectivity
1.000E-03	1.000E-06	1.000E-03	7.961E-01	1.791E-01	2.482E-02
1.000E-03	5.000E-06	5.000E-03	9.193E-01	5.416E-02	2.659E-02
1.000E-03	1.000E-05	1.000E-02	9.329E-01	3.967E-02	2.746E-02
1.000E-03	5.000E-05	5.000E-02	9.566E-01	1.397E-02	2.940E-02
1.000E-03	1.000E-04	1.000E-01	9.636E-01	6.464E-03	2.999E-02
1.000E-03	5.000E-04	5.000E-01	9.698E-01	9.135E-05	3.011E-02
1.000E-03	1.000E-03	1.000E+00	9.699E-01	6.477E-07	3.011E-02
1.000E-03	2.000E-03	2.000E+00	9.699E-01	3.272E-11	3.011E-02
1.000E-03	4.000E-03	4.000E+00	9.699E-01	9.349E-20	3.011E-02
1.000E-03	6.000E-03	6.000E+00	9.699E-01	2.131E-28	3.011E-02
1.000E-03	1.000E-02	1.000E+01	9.699E-01	0.000E+00	3.011E-02
1.000E-03	5.000E-02	5.000E+01	9.699E-01	0.000E+00	3.011E-02
1.000E-03	1.000E-01	1.000E+02	9.699E-01	0.000E+00	3.011E-02
1.000E-03	5.000E-01	5.000E+02	9.699E-01	0.000E+00	3.011E-02
1.000E-03	1.000E+00	1.000E+03	9.699E-01	0.000E+00	3.011E-02
1.000E-02	1.000E-06	1.000E-04	2.361E-01	7.609E-01	1.303E-02
1.000E-02	5.000E-06	5.000E-04	6.416E-01	3.350E-01	2.337E-02
1.000E-02	1.000E-05	1.000E-03	7.976E-01	1.775E-01	2.486E-02
1.000E-02	5.000E-05	5.000E-03	9.214E-01	5.193E-02	2.668E-02
1.000E-02	1.000E-04	1.000E-02	9.360E-01	3.647E-02	2.755E-02
1.000E-02	5.000E-04	5.000E-02	9.618E-01	9.123E-03	2.909E-02
1.000E-02	1.000E-03	1.000E-01	9.680E-01	2.714E-03	2.928E-02
1.000E-02	2.000E-03	2.000E-01	9.703E-01	3.477E-04	2.930E-02
1.000E-02	4.000E-03	4.000E-01	9.707E-01	7.786E-06	2.930E-02
1.000E-02	6.000E-03	6.000E-01	9.707E-01	1.888E-07	2.930E-02
1.000E-02	1.000E-02	1.000E+00	9.707E-01	1.128E-10	2.930E-02
1.000E-02	5.000E-02	5.000E+00	9.707E-01	0.000E+00	2.930E-02
1.000E-02	1.000E-01	1.000E+01	9.707E-01	0.000E+00	2.930E-02
1.000E-02	5.000E-01	5.000E+01	9.707E-01	0.000E+00	2.930E-02
1.000E-02	1.000E+00	1.000E+02	9.707E-01	0.000E+00	2.930E-02
1.000E-01	1.000E-06	1.000E-05	2.735E-02	9.707E-01	1.964E-03
1.000E-01	5.000E-06	5.000E-05	1.270E-01	8.649E-01	9.131E-03
1.000E-01	1.000E-05	1.000E-04	2.323E-01	7.545E-01	1.321E-02
1.000E-01	5.000E-05	5.000E-04	6.559E-01	3.205E-01	2.369E-02
1.000E-01	1.000E-04	1.000E-03	8.123E-01	1.624E-01	2.530E-02
1.000E-01	5.000E-04	5.000E-03	9.386E-01	3.412E-02	2.729E-02
1.000E-01	1.000E-03	1.000E-02	9.565E-01	1.573E-02	2.782E-02
1.000E-01	2.000E-03	2.000E-02	9.677E-01	4.281E-03	2.900E-02
1.000E-01	4.000E-03	4.000E-02	9.716E-01	4.023E-04	2.902E-02
1.000E-01	6.000E-03	6.000E-02	9.719E-01	4.219E-05	2.902E-02
1.000E-01	1.000E-02	1.000E-01	9.720E-01	5.261E-07	2.902E-02
1.000E-01	5.000E-02	5.000E-01	9.720E-01	2.396E-25	2.902E-02
1.000E-01	1.000E-01	1.000E+00	9.720E-01	0.000E+00	2.902E-02
1.000E-01	5.000E-01	5.000E+00	9.720E-01	0.000E+00	2.902E-02
1.000E-01	1.000E+00	1.000E+01	9.720E-01	0.000E+00	2.902E-02

Table C-4. Broad-band IR properties of sooty water clouds (continued).

$\rho_{H_2O}/\rho_{soot}$	$U_{H_2O}$ (gm cm <sup>-2</sup> )	$U_{soot}$ (gm cm <sup>-2</sup> )	Emissivity	Transmissivity	Reflectivity
5.000E-01	1.000E-06	2.000E-06	6.254E-03	9.933E-01	4.361E-04
5.000E-01	5.000E-06	1.000E-05	3.078E-02	9.671E-01	2.092E-03
5.000E-01	1.000E-05	2.000E-05	6.035E-02	9.357E-01	3.977E-03
5.000E-01	5.000E-05	1.000E-04	2.594E-01	7.267E-01	1.394E-02
5.000E-01	1.000E-04	2.000E-04	4.363E-01	5.441E-01	1.966E-02
5.000E-01	5.000E-04	1.000E-03	8.641E-01	1.095E-01	2.640E-02
5.000E-01	1.000E-03	2.000E-03	9.362E-01	3.661E-02	2.721E-02
5.000E-01	2.000E-03	4.000E-03	9.631E-01	9.350E-03	2.751E-02
5.000E-01	4.000E-03	8.000E-03	9.714E-01	1.060E-02	2.755E-02
5.000E-01	6.000E-03	1.200E-02	9.723E-01	1.345E-02	2.755E-02
5.000E-01	1.000E-02	2.000E-02	9.724E-01	2.361E-02	2.755E-02
5.000E-01	5.000E-02	1.000E-01	9.724E-01	1.773E-02	2.755E-02
5.000E-01	1.000E-01	2.000E-01	9.724E-01	0.000E+00	2.755E-02
5.000E-01	5.000E-01	1.000E+00	9.724E-01	0.000E+00	2.755E-02
5.000E-01	1.000E+00	2.000E+00	9.724E-01	0.000E+00	2.755E-02
1.000E+00	1.000E-06	1.000E-06	3.572E-03	9.962E-01	2.361E-04
1.000E+00	5.000E-06	5.000E-06	1.771E-02	9.811E-01	1.155E-03
1.000E+00	1.000E-05	1.000E-05	3.504E-02	9.627E-01	2.249E-03
1.000E+00	5.000E-05	5.000E-05	1.612E-01	8.296E-01	9.201E-03
1.000E+00	1.000E-04	1.000E-04	2.918E-01	6.935E-01	1.477E-02
1.000E+00	5.000E-04	5.000E-04	7.698E-01	2.058E-01	2.541E-02
1.000E+00	1.000E-03	1.000E-03	9.062E-01	6.703E-02	2.675E-02
1.000E+00	2.000E-03	2.000E-03	9.587E-01	1.413E-02	2.714E-02
1.000E+00	4.000E-03	4.000E-03	9.714E-01	1.417E-02	2.719E-02
1.000E+00	6.000E-03	6.000E-03	9.726E-01	1.870E-02	2.720E-02
1.000E+00	1.000E-02	1.000E-02	9.728E-01	3.540E-02	2.720E-02
1.000E+00	5.000E-02	5.000E-02	9.728E-01	5.149E-02	2.720E-02
1.000E+00	1.000E-01	1.000E-01	9.728E-01	0.000E+00	2.720E-02
1.000E+00	5.000E-01	5.000E-01	9.728E-01	0.000E+00	2.720E-02
1.000E+00	1.000E+00	1.000E+00	9.728E-01	0.000E+00	2.720E-02
5.000E+00	1.000E-06	2.000E-07	1.419E-03	9.995E-01	7.167E-05
5.000E+00	5.000E-06	1.000E-06	7.073E-03	9.926E-01	4.710E-04
5.000E+00	1.000E-05	2.000E-06	1.409E-02	9.852E-01	7.360E-04
5.000E+00	5.000E-05	1.000E-05	6.845E-02	9.281E-01	3.456E-03
5.000E+00	1.000E-04	2.000E-05	1.321E-01	8.615E-01	6.405E-03
5.000E+00	5.000E-04	1.000E-04	5.027E-01	4.783E-01	1.892E-02
5.000E+00	1.000E-03	2.000E-04	7.437E-01	2.331E-01	2.319E-02
5.000E+00	2.000E-03	4.000E-04	9.171E-01	5.842E-02	2.403E-02
5.000E+00	4.000E-03	8.000E-04	9.708E-01	4.565E-03	2.465E-02
5.000E+00	6.000E-03	1.200E-03	9.749E-01	4.631E-02	2.466E-02
5.000E+00	1.000E-02	2.000E-03	9.753E-01	7.510E-02	2.466E-02
5.000E+00	5.000E-02	1.000E-02	9.753E-01	2.760E-02	2.466E-02
5.000E+00	1.000E-01	2.000E-02	9.753E-01	0.000E+00	2.466E-02
5.000E+00	5.000E-01	1.000E-01	9.753E-01	0.000E+00	2.466E-02
5.000E+00	1.000E+00	2.000E-01	9.753E-01	0.000E+00	2.466E-02

Table C-4. Broad-band IR properties of sooty water clouds (continued).

$\rho_{H_2O}/\rho_{soot}$	$U_{H_2O}$ (gm cm <sup>-2</sup> )	$U_{soot}$ (gm cm <sup>-2</sup> )	Emissivity	Transmissivity	Reflectivity
1.000E+01	1.000E-06	1.000E-07	1.149E-03	9.988E-01	5.439E-05
1.000E+01	5.000E-06	5.000E-07	5.733E-03	9.940E-01	2.707E-04
1.000E+01	1.000E-05	1.000E-06	1.143E-02	9.980E-01	9.381E-04
1.000E+01	5.000E-05	5.000E-06	5.584E-02	9.416E-01	2.565E-03
1.000E+01	1.000E-04	1.000E-05	1.085E-01	8.846E-01	1.840E-03
1.000E+01	5.000E-04	5.000E-05	4.349E-01	5.492E-01	1.589E-02
1.000E+01	1.000E-03	1.000E-04	6.760E-01	3.033E-01	2.075E-02
1.000E+01	2.000E-03	2.000E-04	8.833E-01	9.393E-02	2.278E-02
1.000E+01	1.000E-03	4.000E-04	9.674E-01	9.574E-03	2.302E-02
1.000E+01	3.000E-03	6.000E-04	9.759E-01	1.054E-03	2.303E-02
1.000E+01	1.000E-02	1.000E-03	9.770E-01	1.548E-03	2.303E-02
1.000E+01	5.000E-02	5.000E-03	9.770E-01	4.186E-22	2.303E-02
1.000E+01	1.000E-01	1.000E-02	9.770E-01	0.000E+00	2.303E-02
1.000E+01	5.000E-01	5.000E-02	9.770E-01	0.000E+00	2.303E-02
1.000E+01	1.000E+00	1.000E-01	9.770E-01	0.000E+00	2.303E-02
3.000E+01	1.000E-06	2.000E-08	9.335E-04	9.990E-01	3.816E-05
3.000E+01	5.000E-06	1.000E-07	4.658E-03	9.952E-01	1.900E-04
3.000E+01	1.000E-05	2.000E-07	9.294E-03	9.903E-01	3.782E-04
3.000E+01	5.000E-05	1.000E-06	1.503E-02	9.526E-01	1.819E-03
3.000E+01	1.000E-04	2.000E-06	1.502E-02	9.095E-01	3.169E-03
3.000E+01	5.000E-04	1.000E-05	4.141E-01	5.117E-01	1.222E-02
3.000E+01	1.000E-03	2.000E-05	6.844E-01	3.845E-01	1.694E-02
3.000E+01	2.000E-03	4.000E-05	8.214E-01	1.019E-01	1.941E-02
3.000E+01	4.000E-03	8.000E-05	8.709E-01	2.693E-02	2.049E-02
3.000E+01	1.000E-02	1.000E-04	9.144E-01	5.143E-03	2.049E-02
3.000E+01	1.000E-02	2.000E-04	9.145E-01	2.905E-04	2.022E-02
3.000E+01	5.000E-02	1.000E-03	9.145E-01	2.713E-15	2.022E-02
3.000E+01	1.000E-01	2.000E-03	9.145E-01	1.093E-27	2.022E-02
3.000E+01	5.000E-01	1.000E-02	9.145E-01	1.093E-27	2.022E-02
3.000E+01	1.000E+00	2.000E-02	9.145E-01	0.000E-27	2.022E-02
1.000E+02	1.000E-06	1.000E-08	1.045E-03	9.991E-01	3.413E-05
1.000E+02	5.000E-06	5.000E-08	1.024E-03	9.953E-01	1.778E-04
1.000E+02	1.000E-05	1.000E-07	1.026E-03	9.944E-01	3.112E-04
1.000E+02	5.000E-05	5.000E-07	1.129E-02	9.504E-01	1.724E-03
1.000E+02	1.000E-04	1.000E-06	3.604E-02	9.107E-01	1.214E-03
1.000E+02	5.000E-04	5.000E-06	1.614E-01	5.264E-01	1.148E-02
1.000E+02	1.000E-03	1.000E-05	3.369E-01	3.318E-01	1.133E-02
1.000E+02	2.000E-03	2.000E-05	3.172E-01	1.613E-01	1.095E-02
1.000E+02	1.000E-02	1.000E-04	3.197E-01	3.108E-02	1.041E-02
1.000E+02	5.000E-02	5.000E-04	3.132E-01	2.116E-03	1.041E-02
1.000E+02	1.000E-01	1.000E-03	3.149E-01	1.047E-04	1.041E-02
1.000E+02	5.000E-01	5.000E-03	3.149E-01	1.047E-17	1.041E-02
1.000E+02	1.000E+00	1.000E-02	3.149E-01	1.047E-17	1.041E-02
1.000E+02	5.000E+00	5.000E-02	3.149E-01	0.000E+00	1.041E-02
1.000E+02	1.000E+00	1.000E-01	3.149E-01	0.000E+00	1.041E-02

Table C-4. Broad-band IR properties of sooty water clouds (continued).

$\rho_{H_2O}/\rho_{soot}$	$U_{H_2O}$ (gm cm <sup>-2</sup> )	$U_{soot}$ (gm cm <sup>-2</sup> )	Emissivity	Transmissivity	Reflectivity
2.000E+02	1.000E-06	5.000E-09	9.930E-04	9.991E-01	3.511E-05
2.000E+02	5.000E-06	2.500E-08	4.457E-03	9.954E-01	1.749E-04
2.000E+02	1.000E-05	5.000E-08	8.892E-03	9.908E-01	3.481E-04
2.000E+02	5.000E-05	2.500E-07	4.364E-02	9.547E-01	1.676E-03
2.000E+02	1.000E-04	5.000E-07	8.529E-02	9.115E-01	3.200E-03
2.000E+02	5.000E-04	2.500E-06	3.569E-01	6.317E-01	1.176E-02
2.000E+02	1.000E-03	5.000E-06	5.809E-01	4.032E-01	1.589E-02
2.000E+02	2.000E-03	1.000E-05	8.117E-01	1.587E-01	1.858E-02
2.000E+02	4.000E-03	2.000E-05	9.462E-01	3.447E-02	1.928E-02
2.000E+02	6.000E-03	3.000E-05	9.724E-01	8.275E-03	1.934E-02
2.000E+02	1.000E-02	5.000E-05	9.800E-01	6.592E-04	1.935E-02
2.000E+02	5.000E-02	2.500E-04	9.807E-01	5.857E-12	1.935E-02
2.000E+02	1.000E-01	5.000E-04	9.807E-01	4.863E-20	1.935E-02
2.000E+02	5.000E-01	2.500E-03	9.807E-01	0.000E+00	1.935E-02
2.000E+02	1.000E+00	5.000E-03	9.807E-01	0.000E+00	1.935E-02
5.000E+02	1.000E-06	2.000E-09	8.849E-04	9.991E-01	3.451E-05
5.000E+02	5.000E-06	1.000E-08	4.416E-03	9.954E-01	1.719E-04
5.000E+02	1.000E-05	2.000E-08	8.812E-03	9.908E-01	3.421E-04
5.000E+02	5.000E-05	1.000E-07	4.325E-02	9.551E-01	1.647E-03
5.000E+02	1.000E-04	2.000E-07	8.455E-02	9.113E-01	3.145E-03
5.000E+02	5.000E-04	1.000E-06	3.542E-01	6.346E-01	1.119E-02
5.000E+02	1.000E-03	2.000E-06	5.773E-01	4.011E-01	1.546E-02
5.000E+02	2.000E-03	4.000E-06	8.023E-01	1.733E-01	1.935E-02
5.000E+02	4.000E-03	8.000E-06	9.446E-01	3.530E-02	1.908E-02
5.000E+02	6.000E-03	1.200E-05	9.713E-01	9.048E-03	1.914E-02
5.000E+02	1.000E-02	2.000E-05	9.801E-01	2.855E-04	1.915E-02
5.000E+02	5.000E-02	1.000E-04	9.809E-01	4.087E-11	1.910E-02
5.000E+02	1.000E-01	2.000E-04	9.809E-01	3.007E-19	1.915E-02
5.000E+02	5.000E-01	1.000E-03	9.809E-01	0.000E+00	1.915E-02
5.000E+02	1.000E+00	2.000E-03	9.809E-01	0.000E+00	1.915E-02
1.000E+03	1.000E-06	1.000E-09	8.822E-04	9.991E-01	3.430E-05
1.000E+03	5.000E-06	5.000E-09	4.403E-03	9.954E-01	1.709E-04
1.000E+03	1.000E-05	1.000E-08	8.785E-03	9.908E-01	3.401E-04
1.000E+03	5.000E-05	5.000E-08	4.312E-02	9.552E-01	1.608E-03
1.000E+03	1.000E-04	1.000E-07	8.430E-02	9.126E-01	3.107E-03
1.000E+03	5.000E-04	5.000E-07	3.533E-01	6.356E-01	1.113E-02
1.000E+03	1.000E-03	1.000E-06	5.750E-01	4.084E-01	1.559E-02
1.000E+03	2.000E-03	2.000E-06	8.071E-01	1.744E-01	1.920E-02
1.000E+03	4.000E-03	4.000E-06	9.441E-01	3.589E-02	1.901E-02
1.000E+03	6.000E-03	6.000E-06	9.716E-01	9.324E-03	1.907E-02
1.000E+03	1.000E-02	1.000E-05	9.801E-01	2.835E-04	1.909E-02
1.000E+03	5.000E-02	5.000E-05	9.809E-01	6.101E-11	1.908E-02
1.000E+03	1.000E-01	1.000E-04	9.809E-01	3.001E-19	1.908E-02
1.000E+03	5.000E-01	5.000E-04	9.809E-01	0.000E+00	1.908E-02
1.000E+03	1.000E+00	1.000E-03	9.809E-01	0.000E+00	1.908E-02

Table C-4. Broad-band IR properties of sooty water clouds (continued).

$\rho_{H_2O}/\rho_{soot}$	$U_{H_2O}$ ( $gm\ cm^{-2}$ )	$U_{soot}$ ( $gm\ cm^{-2}$ )	Emissivity	Transmissivity	Reflectivity
5.000E+03	1.000E-06	2.000E-10	8.800E-04	9.991E-01	3.414E-05
5.000E+03	5.000E-06	1.000E-09	4.392E-03	9.954E-01	1.700E-04
5.000E+03	1.000E-05	2.000E-09	8.764E-03	9.909E-01	3.385E-04
5.000E+03	5.000E-05	1.000E-08	4.302E-02	9.553E-01	1.630E-03
5.000E+03	1.000E-04	2.000E-08	8.410E-02	9.128E-01	3.112E-03
5.000E+03	5.000E-04	1.000E-07	3.526E-01	6.364E-01	1.108E-02
5.000E+03	1.000E-03	2.000E-07	5.751E-01	1.094E-01	1.551E-02
5.000E+03	2.000E-03	4.000E-07	8.062E-01	1.755E-01	1.821E-02
5.000E+03	4.000E-03	8.000E-07	9.436E-01	3.745E-02	1.395E-02
5.000E+03	5.000E-03	1.200E-06	9.714E-01	9.553E-03	1.901E-02
5.000E+03	1.000E-02	2.000E-06	9.801E-01	8.745E-04	1.903E-02
5.000E+03	5.000E-02	1.000E-05	9.810E-01	1.422E-10	1.903E-02
5.000E+03	1.000E-01	2.000E-05	9.810E-01	5.944E-17	1.903E-02
5.000E+03	5.000E-01	1.000E-04	9.810E-01	0.000E+00	1.903E-02
5.000E+03	1.000E+00	2.000E-04	9.810E-01	0.000E+00	1.903E-02
1.000E+04	1.000E-06	1.000E-10	8.798E-04	9.991E-01	3.412E-05
1.000E+04	5.000E-06	5.000E-10	4.391E-03	9.954E-01	1.699E-04
1.000E+04	1.000E-05	1.000E-09	8.761E-03	9.909E-01	3.383E-04
1.000E+04	5.000E-05	5.000E-09	4.301E-02	9.554E-01	1.629E-03
1.000E+04	1.000E-04	1.000E-08	8.407E-02	9.128E-01	3.111E-03
1.000E+04	5.000E-04	5.000E-08	3.525E-01	6.365E-01	1.107E-02
1.000E+04	1.000E-03	1.000E-07	5.749E-01	4.096E-01	1.551E-02
1.000E+04	2.000E-03	2.000E-07	8.061E-01	1.757E-01	1.820E-02
1.000E+04	4.000E-03	4.000E-07	9.435E-01	3.751E-02	1.394E-02
1.000E+04	6.000E-03	6.000E-07	9.714E-01	9.582E-03	1.901E-02
1.000E+04	1.000E-02	1.000E-06	9.801E-01	8.798E-04	1.902E-02
1.000E+04	5.000E-02	5.000E-06	9.810E-01	1.525E-10	1.902E-02
1.000E+04	1.000E-01	1.000E-05	9.810E-01	6.930E-17	1.902E-02
1.000E+04	5.000E-01	5.000E-05	9.810E-01	0.000E+00	1.902E-02
1.000E+04	1.000E+00	1.000E-04	9.810E-01	0.000E+00	1.902E-02
1.000E+05	1.000E-06	1.000E-11	8.795E-04	9.991E-01	3.410E-05
1.000E+05	5.000E-06	5.000E-11	4.389E-03	9.954E-01	1.699E-04
1.000E+05	1.000E-05	1.000E-10	8.759E-03	9.909E-01	3.381E-04
1.000E+05	5.000E-05	5.000E-10	4.300E-02	9.554E-01	1.629E-03
1.000E+05	1.000E-04	1.000E-09	8.405E-02	9.128E-01	3.109E-03
1.000E+05	5.000E-04	5.000E-09	3.524E-01	6.365E-01	1.108E-02
1.000E+05	1.000E-03	1.000E-08	5.748E-01	4.097E-01	1.550E-02
1.000E+05	2.000E-03	2.000E-08	8.060E-01	1.758E-01	1.819E-02
1.000E+05	4.000E-03	4.000E-08	9.435E-01	3.757E-02	1.393E-02
1.000E+05	6.000E-03	6.000E-08	9.714E-01	9.598E-03	1.900E-02
1.000E+05	1.000E-02	1.000E-07	9.801E-01	8.845E-04	1.901E-02
1.000E+05	5.000E-02	5.000E-07	9.810E-01	1.525E-10	1.901E-02
1.000E+05	1.000E-01	1.000E-06	9.810E-01	7.932E-17	1.901E-02
1.000E+05	5.000E-01	5.000E-06	9.810E-01	0.000E+00	1.901E-02
1.000E+05	1.000E+00	1.000E-05	9.810E-01	0.000E+00	1.901E-02

Table C-4. Broad-band IR properties of sooty water clouds (Concluded).

$\rho_{\text{H}_2\text{O}}/\rho_{\text{soot}}$	$U_{\text{H}_2\text{O}}$ (gm cm <sup>-2</sup> )	$U_{\text{soot}}$ (gm cm <sup>-2</sup> )	Emissivity	Transmissivity	Reflectivity
1.000E+10	1.000E-06	1.000E-16	8.795E-04	9.991E-01	3.410E-05
1.000E+10	5.000E-06	5.000E-16	4.389E-03	9.954E-01	1.698E-04
1.000E+10	1.000E-05	1.000E-15	8.758E-03	9.909E-01	3.381E-04
1.000E+10	5.000E-05	5.000E-15	4.299E-02	9.554E-01	1.628E-03
1.000E+10	1.000E-04	1.000E-14	8.405E-02	9.128E-01	3.109E-03
1.000E+10	5.000E-04	5.000E-14	3.524E-01	6.365E-01	1.106E-02
1.000E+10	1.000E-03	1.000E-13	5.748E-01	4.097E-01	1.550E-02
1.000E+10	2.000E-03	2.000E-13	8.060E-01	1.758E-01	1.819E-02
1.000E+10	4.000E-03	4.000E-13	9.435E-01	3.758E-02	1.893E-02
1.000E+10	6.000E-03	6.000E-13	9.714E-01	9.611E-03	1.900E-02
1.000E+10	1.000E-02	1.000E-12	9.801E-01	8.851E-04	1.901E-02
1.000E+10	5.000E-02	5.000E-12	9.810E-01	1.637E-10	1.901E-02
1.000E+10	1.000E-01	1.000E-11	9.810E-01	8.052E-17	1.901E-02
1.000E+10	5.000E-01	5.000E-11	9.810E-01	0.000E+00	1.901E-02
1.000E+10	1.000E+00	1.000E-10	9.810E-01	0.000E+00	1.901E-02

Table C-5. Optical properties in the visible ( $\lambda=0.55 \mu\text{m}$ ) of sooty water clouds.

$\rho_{\text{H}_2\text{O}}/\rho_{\text{soot}}$	$\tau^*$ (Optical depth)	$U_{\text{soot}}$ ( $\text{gm cm}^{-2}$ )	$U_{\text{H}_2\text{O}}$ ( $\text{gm cm}^{-2}$ )	R (Reflectivity)	T (Transmissivity)	$\epsilon$ (Emissivity)
1.000E-03	4.422E+01	1.000E-03	1.000E-06	4.424E-02	3.986E-09	9.558E-01
1.000E-03	2.211E+02	5.000E-03	5.000E-06	4.421E-02	0.000E+00	9.558E-01
1.000E-03	4.422E+02	1.000E-02	1.000E-05	4.424E-02	0.000E+00	9.558E-01
1.000E-03	2.211E+03	5.000E-02	5.000E-05	4.424E-02	0.000E+00	9.558E-01
1.000E-03	4.422E+03	1.000E-01	1.000E-04	4.424E-02	0.000E+00	9.558E-01
1.000E-03	2.211E+04	5.000E-01	5.000E-04	4.424E-02	0.000E+00	9.558E-01
1.000E-03	4.422E+04	1.000E+00	1.000E-03	4.424E-02	0.000E+00	9.558E-01
1.000E-03	8.844E+04	2.000E+00	2.000E-03	4.424E-02	0.000E+00	9.558E-01
1.000E-03	1.769E+05	4.000E+00	4.000E-03	4.424E-02	0.000E+00	9.558E-01
1.000E-03	2.653E+05	6.000E+00	6.000E-03	4.424E-02	0.000E+00	9.558E-01
1.000E-03	4.422E+05	1.000E+01	1.000E-02	4.424E-02	0.000E+00	9.558E-01
1.000E-03	2.211E+06	5.000E+01	5.000E-02	4.424E-02	0.000E+00	9.558E-01
1.000E-03	4.422E+06	1.000E+02	1.000E-01	4.424E-02	0.000E+00	9.558E-01
1.000E-03	2.211E+07	5.000E+02	5.000E-01	4.421E-02	0.000E+00	9.558E-01
1.000E-03	4.422E+07	1.000E+03	1.000E+00	4.424E-02	0.000E+00	9.558E-01
1.000E-02	4.424E+00	1.000E-04	1.000E-06	4.333E-02	1.443E-01	8.124E-01
1.000E-02	2.212E+01	5.000E-04	5.000E-06	4.425E-02	6.305E-05	9.557E-01
1.000E-02	4.424E+01	1.000E-03	1.000E-05	4.425E-02	3.984E-09	9.557E-01
1.000E-02	2.212E+02	5.000E-03	5.000E-05	4.425E-02	0.000E+00	9.557E-01
1.000E-02	4.424E+02	1.000E-02	1.000E-04	4.425E-02	0.000E+00	9.557E-01
1.000E-02	2.212E+03	5.000E-02	5.000E-04	4.425E-02	0.000E+00	9.557E-01
1.000E-02	4.424E+03	1.000E-01	1.000E-03	4.425E-02	0.000E+00	9.557E-01
1.000E-02	8.847E+03	2.000E-01	2.000E-03	4.425E-02	0.000E+00	9.557E-01
1.000E-02	1.769E+04	4.000E-01	4.000E-03	4.425E-02	0.000E+00	9.557E-01
1.000E-02	2.654E+04	6.000E-01	6.000E-03	4.425E-02	0.000E+00	9.557E-01
1.000E-02	4.424E+04	1.000E+00	1.000E-02	4.425E-02	0.000E+00	9.557E-01
1.000E-02	2.212E+05	5.000E+00	5.000E-02	4.425E-02	0.000E+00	9.557E-01
1.000E-02	4.424E+05	1.000E+01	1.000E-01	4.425E-02	0.000E+00	9.557E-01
1.000E-02	2.212E+06	5.000E+01	5.000E-01	4.425E-02	0.000E+00	9.557E-01
1.000E-02	4.424E+06	1.000E+02	1.000E+00	4.425E-02	0.000E+00	9.557E-01
1.000E-01	4.439E-01	1.000E-05	1.000E-06	1.427E-02	8.236E-01	1.621E-01
1.000E-01	2.220E+00	5.000E-05	5.000E-06	3.802E-02	3.795E-01	5.825E-01
1.000E-01	4.439E+00	1.000E-04	1.000E-05	4.350E-02	1.442E-01	8.123E-01
1.000E-01	2.220E+01	5.000E-04	5.000E-05	4.442E-02	6.284E-05	9.555E-01
1.000E-01	4.439E+01	1.000E-03	1.000E-04	4.442E-02	3.957E-09	9.556E-01
1.000E-01	2.220E+02	5.000E-03	5.000E-04	4.442E-02	0.000E+00	9.556E-01
1.000E-01	4.439E+02	1.000E-02	1.000E-03	4.442E-02	0.000E+00	9.556E-01
1.000E-01	8.879E+02	2.000E-02	2.000E-03	4.442E-02	0.000E+00	9.556E-01
1.000E-01	1.776E+03	4.000E-02	4.000E-03	4.442E-02	0.000E+00	9.556E-01
1.000E-01	2.664E+03	6.000E-02	6.000E-03	4.442E-02	0.000E+00	9.556E-01
1.000E-01	4.439E+03	1.000E-01	1.000E-02	4.442E-02	0.000E+00	9.556E-01
1.000E-01	2.220E+04	5.000E-01	5.000E-02	4.442E-02	0.000E+00	9.556E-01
1.000E-01	4.439E+04	1.000E+00	1.000E-01	4.442E-02	0.000E+00	9.556E-01
1.000E-01	2.220E+05	5.000E+00	5.000E-01	4.442E-02	0.000E+00	9.556E-01
1.000E-01	4.439E+05	1.000E+01	1.000E+00	4.442E-02	0.000E+00	9.556E-01



Table C-5. Optical properties in the visible ( $\lambda=0.55 \mu\text{m}$ ) of sooty water clouds (continued).

$\rho_{\text{H}_2\text{O}}/\rho_{\text{soot}}$	$\tau^*$ (Optical Depth)	$U_{\text{soot}}$ ( $\text{gm cm}^{-2}$ )	$U_{\text{H}_2\text{O}}$ ( $\text{gm cm}^{-2}$ )	R (Reflectivity)	T (Transmissivity)	$\epsilon$ (Emissivity)
5.000E-01	9.018E-02	2.000E-06	1.000E-06	3.376E-03	9.618E-01	3.478E-02
5.000E-01	4.509E-01	1.000E-05	5.000E-06	1.454E-02	8.233E-01	1.621E-01
5.000E-01	9.018E-01	2.000E-05	1.000E-05	2.439E-02	6.780E-01	2.976E-01
5.000E-01	4.509E+00	1.000E-04	5.000E-05	4.425E-02	1.438E-01	8.120E-01
5.000E-01	9.018E+00	2.000E-04	1.000E-04	4.517E-02	2.071E-02	9.341E-01
5.000E-01	4.509E+01	1.000E-03	5.000E-04	4.518E-02	3.842E-09	9.548E-01
5.000E-01	9.018E+01	2.000E-03	1.000E-03	4.518E-02	1.479E-17	9.548E-01
5.000E-01	1.804E+02	4.000E-03	2.000E-03	4.518E-02	2.192E-34	9.548E-01
5.000E-01	3.607E+02	8.000E-03	4.000E-03	4.518E-02	0.000E+00	9.548E-01
5.000E-01	5.411E+02	1.200E-02	6.000E-03	4.518E-02	0.000E+00	9.548E-01
5.000E-01	9.018E+02	2.000E-02	1.000E-02	4.518E-02	0.000E+00	9.548E-01
5.000E-01	4.509E+03	1.000E-01	5.000E-02	4.518E-02	0.000E+00	9.548E-01
5.000E-01	9.018E+03	2.000E-01	1.000E-01	4.518E-02	0.000E+00	9.548E-01
5.000E-01	4.509E+04	1.000E+00	5.000E-01	4.518E-02	0.000E+00	9.548E-01
5.000E-01	9.018E+04	2.000E+00	1.000E+00	4.518E-02	0.000E+00	9.548E-01
1.000E+00	4.596E-02	1.000E-06	1.000E-06	1.760E-03	9.807E-01	1.754E-02
1.000E+00	2.298E-01	5.000E-06	5.000E-06	8.154E-03	9.072E-01	8.469E-02
1.000E+00	4.596E-01	1.000E-05	1.000E-05	1.486E-02	8.230E-01	1.621E-01
1.000E+00	2.298E+00	5.000E-05	5.000E-05	3.952E-02	3.782E-01	5.823E-01
1.000E+00	4.596E+00	1.000E-04	1.000E-04	4.518E-02	1.432E-01	8.116E-01
1.000E+00	2.298E+01	5.000E-04	5.000E-04	4.613E-02	6.079E-05	9.539E-01
1.000E+00	4.596E+01	1.000E-03	1.000E-03	4.613E-02	3.703E-09	9.539E-01
1.000E+00	9.192E+01	2.000E-03	2.000E-03	4.613E-02	1.374E-17	9.539E-01
1.000E+00	1.838E+02	4.000E-03	4.000E-03	4.613E-02	1.892E-34	9.539E-01
1.000E+00	2.758E+02	6.000E-03	6.000E-03	4.613E-02	0.000E+00	9.539E-01
1.000E+00	4.596E+02	1.000E-02	1.000E-02	4.613E-02	0.000E+00	9.539E-01
1.000E+00	2.298E+03	5.000E-02	5.000E-02	4.613E-02	0.000E+00	9.539E-01
1.000E+00	4.596E+03	1.000E-01	1.000E-01	4.613E-02	0.000E+00	9.539E-01
1.000E+00	2.298E+04	5.000E-01	5.000E-01	4.613E-02	0.000E+00	9.539E-01
1.000E+00	4.596E+04	1.000E+00	1.000E+00	4.613E-02	0.000E+00	9.539E-01
5.000E+00	1.058E-02	2.000E-07	1.000E-06	4.217E-04	9.960E-01	3.534E-03
5.000E+00	5.292E-02	1.000E-06	5.000E-06	2.075E-03	9.804E-01	1.754E-02
5.000E+00	1.058E-01	2.000E-06	1.000E-05	4.070E-03	9.611E-01	3.478E-02
5.000E+00	5.292E-01	1.000E-05	5.000E-05	1.748E-02	8.204E-01	1.621E-01
5.000E+00	1.058E+00	2.000E-05	1.000E-04	2.925E-02	6.733E-01	2.975E-01
5.000E+00	5.293E+00	1.000E-04	5.000E-04	5.252E-02	1.390E-01	8.085E-01
5.000E+00	1.059E+01	2.000E-04	1.000E-03	5.354E-02	1.938E-02	9.271E-01
5.000E+00	2.117E+01	4.000E-04	2.000E-03	5.356E-02	3.766E-04	9.461E-01
5.000E+00	4.234E+01	8.000E-04	4.000E-03	5.356E-02	1.423E-07	9.464E-01
5.000E+00	6.351E+01	1.200E-03	6.000E-03	5.356E-02	5.374E-11	9.464E-01
5.000E+00	1.058E+02	2.000E-03	1.000E-02	5.356E-02	7.667E-18	9.464E-01
5.000E+00	5.293E+02	1.000E-02	5.000E-02	5.356E-02	0.000E+00	9.464E-01
5.000E+00	1.059E+03	2.000E-02	1.000E-01	5.356E-02	0.000E+00	9.464E-01
5.000E+00	5.293E+03	1.000E-01	5.000E-01	5.356E-02	0.000E+00	9.464E-01
5.000E+00	1.059E+04	2.000E-01	1.000E+00	5.356E-02	0.000E+00	9.464E-01

Table C-5. Optical properties in the visible ( $\lambda=0.55 \mu\text{m}$ ) of sooty water clouds (continued).

$\rho_{\text{H}_2\text{O}}/\rho_{\text{soot}}$	$\tau^*$ (Optical Depth)	$U_{\text{soot}}$ ( $\text{gm cm}^{-2}$ )	$U_{\text{H}_2\text{O}}$ ( $\text{gm cm}^{-2}$ )	R (Reflectivity)	T (Transmissivity)	$\epsilon$ (Emissivity)
1.000E+01	6.163E-03	1.000E-07	1.000E-06	2.514E-04	9.980E-01	1.768E-03
1.000E+01	3.081E-02	5.000E-07	5.000E-06	1.247E-03	9.899E-01	8.811E-03
1.000E+01	6.163E-02	1.000E-06	1.000E-05	2.468E-03	9.800E-01	1.754E-02
1.000E+01	3.081E-01	5.000E-06	5.000E-05	1.140E-02	9.039E-01	8.468E-02
1.000E+01	6.163E-01	1.000E-05	1.000E-04	2.072E-02	8.172E-01	1.621E-01
1.000E+01	3.082E+00	5.000E-05	5.000E-04	5.415E-02	3.655E-01	5.803E-01
1.000E+01	6.163E+00	1.000E-04	1.000E-03	6.140E-02	1.340E-01	8.046E-01
1.000E+01	1.233E+01	2.000E-04	2.000E-03	6.251E-02	1.802E-02	9.195E-01
1.000E+01	2.465E+01	4.000E-04	4.000E-03	6.253E-02	3.261E-04	9.371E-01
1.000E+01	3.698E+01	6.000E-04	6.000E-03	6.253E-02	5.900E-06	9.375E-01
1.000E+01	6.163E+01	1.000E-03	1.000E-02	6.253E-02	1.931E-09	9.375E-01
1.000E+01	3.081E+02	5.000E-03	5.000E-02	6.253E-02	0.000E+00	9.375E-01
1.000E+01	6.163E+02	1.000E-02	1.000E-01	6.253E-02	0.000E+00	9.375E-01
1.000E+01	3.082E+03	5.000E-02	5.000E-01	6.253E-02	0.000E+00	9.375E-01
1.000E+01	6.163E+03	1.000E-01	1.000E+00	6.253E-02	0.000E+00	9.375E-01
5.000E+01	2.625E-03	2.000E-08	1.000E-06	1.145E-04	9.995E-01	3.539E-04
5.000E+01	1.313E-02	1.000E-07	5.000E-06	5.714E-04	9.977E-01	1.769E-03
5.000E+01	2.625E-02	2.000E-07	1.000E-05	1.140E-03	9.953E-01	3.534E-03
5.000E+01	1.313E-01	1.000E-06	5.000E-05	5.595E-03	9.769E-01	1.754E-02
5.000E+01	2.625E-01	2.000E-06	1.000E-04	1.093E-02	9.543E-01	3.478E-02
5.000E+01	1.313E+00	1.000E-05	5.000E-04	4.577E-02	7.923E-01	1.620E-01
5.000E+01	2.625E+00	2.000E-05	1.000E-03	7.455E-02	6.290E-01	2.964E-01
5.000E+01	5.251E+00	4.000E-05	2.000E-03	1.042E-01	3.979E-01	4.979E-01
5.000E+01	1.050E+01	8.000E-05	4.000E-03	1.209E-01	1.600E-01	7.191E-01
5.000E+01	1.575E+01	1.200E-04	6.000E-03	1.236E-01	6.448E-02	8.119E-01
5.000E+01	2.625E+01	2.000E-04	1.000E-02	1.241E-01	1.047E-02	8.654E-01
5.000E+01	1.313E+02	1.000E-03	5.000E-02	1.241E-01	1.342E-10	8.759E-01
5.000E+01	2.625E+02	2.000E-03	1.000E-01	1.241E-01	1.828E-20	8.759E-01
5.000E+01	1.313E+03	1.000E-02	5.000E-01	1.241E-01	0.000E+00	8.759E-01
5.000E+01	2.625E+03	2.000E-02	1.000E+00	1.241E-01	0.000E+00	8.759E-01
1.000E+02	2.183E-03	1.000E-08	1.000E-06	9.733E-05	9.997E-01	1.770E-04
1.000E+02	1.092E-02	5.000E-08	5.000E-06	4.861E-04	9.986E-01	8.847E-04
1.000E+02	2.183E-02	1.000E-07	1.000E-05	9.709E-04	9.973E-01	1.768E-03
1.000E+02	1.092E-01	5.000E-07	5.000E-05	4.802E-03	9.864E-01	8.811E-03
1.000E+02	2.183E-01	1.000E-06	1.000E-04	9.473E-03	9.730E-01	1.754E-02
1.000E+02	1.092E+00	5.000E-06	5.000E-04	4.260E-02	8.728E-01	8.468E-02
1.000E+02	2.183E+00	1.000E-05	1.000E-03	7.511E-02	7.631E-01	1.618E-01
1.000E+02	4.366E+00	2.000E-05	2.000E-03	1.191E-01	5.856E-01	2.953E-01
1.000E+02	8.733E+00	4.000E-05	4.000E-03	1.605E-01	3.479E-01	4.916E-01
1.000E+02	1.310E+01	6.000E-05	6.000E-03	1.752E-01	2.077E-01	6.171E-01
1.000E+02	2.183E+01	1.000E-04	1.000E-02	1.823E-01	7.435E-02	7.433E-01
1.000E+02	1.092E+02	5.000E-04	5.000E-02	1.834E-01	2.602E-06	8.166E-01
1.000E+02	2.183E+02	1.000E-03	1.000E-01	1.834E-01	7.006E-12	8.166E-01
1.000E+02	1.092E+03	5.000E-03	5.000E-01	1.834E-01	0.000E+00	8.166E-01
1.000E+02	2.183E+03	1.000E-02	1.000E+00	1.834E-01	0.000E+00	8.166E-01

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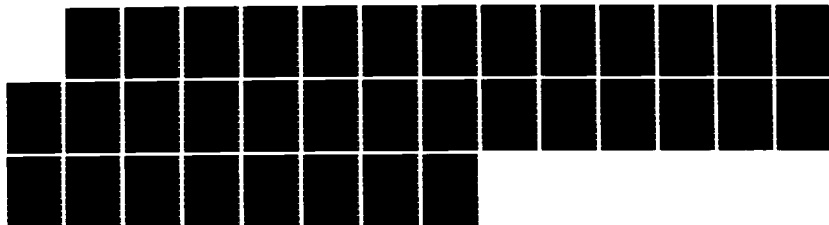
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Table C-5. Optical properties in the visible ( $\lambda=0.55 \mu\text{m}$ ) of sooty water clouds (continued).

$\rho_{\text{H}_2\text{O}}/\rho_{\text{soot}}$	$\tau^*$ (Optical Depth)	$U_{\text{soot}}$ ( $\text{gm cm}^{-2}$ )	$U_{\text{H}_2\text{O}}$ ( $\text{gm cm}^{-2}$ )	R (Reflectivity)	T (Transmissivity)	$\epsilon$ (Emissivity)
2.000E+02	1.962E-03	5.000E-09	1.000E-06	8.874E-05	9.998E-01	8.851E-05
2.000E+02	9.810E-03	2.500E-08	5.000E-06	4.434E-04	9.991E-01	4.424E-04
2.000E+02	1.962E-02	5.000E-08	1.000E-05	8.860E-04	9.982E-01	8.846E-04
2.000E+02	9.810E-02	2.500E-07	5.000E-05	4.399E-03	9.912E-01	4.415E-03
2.000E+02	1.962E-01	5.000E-07	1.000E-04	8.720E-03	9.825E-01	8.811E-03
2.000E+02	9.811E-01	2.500E-06	5.000E-04	4.069E-02	9.160E-01	4.327E-02
2.000E+02	1.962E+00	5.000E-06	1.000E-03	7.489E-02	8.405E-01	8.459E-02
2.000E+02	3.924E+00	1.000E-05	2.000E-03	1.281E-01	7.105E-01	1.614E-01
2.000E+02	7.848E+00	2.000E-05	4.000E-03	1.938E-01	5.132E-01	2.930E-01
2.000E+02	1.177E+01	3.000E-05	6.000E-03	2.284E-01	3.739E-01	3.977E-01
2.000E+02	1.962E+01	5.000E-05	1.000E-02	2.568E-01	2.007E-01	5.425E-01
2.000E+02	9.811E+01	2.500E-04	5.000E-02	2.684E-01	4.323E-04	7.312E-01
2.000E+02	1.962E+02	5.000E-04	1.000E-01	2.684E-01	2.014E-07	7.316E-01
2.000E+02	9.810E+02	2.500E-03	5.000E-01	2.684E-01	4.468E-34	7.316E-01
2.000E+02	1.962E+03	5.000E-03	1.000E+00	2.684E-01	0.000E+00	7.316E-01
5.000E+02	1.829E-03	2.000E-09	1.000E-06	8.357E-05	9.999E-01	3.541E-05
5.000E+02	9.147E-03	1.000E-08	5.000E-06	4.177E-04	9.994E-01	1.769E-04
5.000E+02	1.829E-02	2.000E-08	1.000E-05	8.349E-04	9.988E-01	3.539E-04
5.000E+02	9.147E-02	1.000E-07	5.000E-05	4.155E-03	9.941E-01	1.768E-03
5.000E+02	1.829E-01	2.000E-07	1.000E-04	8.261E-03	9.882E-01	3.534E-03
5.000E+02	9.147E-01	1.000E-06	5.000E-04	3.943E-02	9.430E-01	1.754E-02
5.000E+02	1.829E+00	2.000E-06	1.000E-03	7.454E-02	8.907E-01	3.476E-02
5.000E+02	3.659E+00	4.000E-06	2.000E-03	1.340E-01	7.978E-01	6.822E-02
5.000E+02	7.318E+00	8.000E-06	4.000E-03	2.209E-01	6.481E-01	1.311E-01
5.000E+02	1.098E+01	1.200E-05	6.000E-03	2.799E-01	5.328E-01	1.894E-01
5.000E+02	1.829E+01	2.000E-05	1.000E-02	3.457E-01	3.679E-01	2.864E-01
5.000E+02	9.147E+01	1.000E-04	5.000E-02	4.103E-01	1.205E-02	5.776E-01
5.000E+02	1.829E+02	2.000E-04	1.000E-01	4.104E-01	1.746E-04	5.894E-01
5.000E+02	9.147E+02	1.000E-03	5.000E-01	4.104E-01	3.396E-19	5.896E-01
5.000E+02	1.829E+03	2.000E-03	1.000E+00	4.104E-01	0.000E+00	5.896E-01
1.000E+03	1.785E-03	1.000E-09	1.000E-06	8.194E-05	9.999E-01	1.772E-05
1.000E+03	8.926E-03	5.000E-09	5.000E-06	4.091E-04	9.995E-01	8.847E-05
1.000E+03	1.785E-02	1.000E-08	1.000E-05	8.179E-04	9.990E-01	1.770E-04
1.000E+03	8.926E-02	5.000E-08	5.000E-05	4.073E-03	9.950E-01	8.847E-04
1.000E+03	1.785E-01	1.000E-07	1.000E-04	8.106E-03	9.901E-01	1.768E-03
1.000E+03	8.926E-01	5.000E-07	5.000E-04	3.898E-02	9.522E-01	8.811E-03
1.000E+03	1.785E+00	1.000E-06	1.000E-03	7.438E-02	9.081E-01	1.754E-02
1.000E+03	3.570E+00	2.000E-06	2.000E-03	1.361E-01	8.292E-01	3.475E-02
1.000E+03	7.141E+00	4.000E-06	4.000E-03	2.314E-01	7.005E-01	6.810E-02
1.000E+03	1.071E+01	6.000E-06	6.000E-03	3.003E-01	5.998E-01	9.993E-02
1.000E+03	1.785E+01	1.000E-05	1.000E-02	3.898E-01	4.515E-01	1.587E-01
1.000E+03	8.926E+01	5.000E-05	5.000E-02	5.227E-01	4.270E-02	4.346E-01
1.000E+03	1.785E+02	1.000E-04	1.000E-01	5.240E-01	2.509E-03	4.735E-01
1.000E+03	8.926E+02	5.000E-04	5.000E-01	5.240E-01	3.588E-13	4.760E-01
1.000E+03	1.785E+03	1.000E-03	1.000E+00	5.240E-01	1.775E-25	4.760E-01

Table C-5. Optical properties in the visible ( $\lambda=0.55 \mu\text{m}$ ) of sooty water clouds (continued).

$a_{\text{H}_2\text{O}}/a_{\text{soot}}$	$\tau^*$ (Optical Depth)	$U_{\text{soot}}$ ( $\text{cm}^{-2}$ )	$U_{\text{H}_2\text{O}}$ ( $\text{cm}^{-2}$ )	R (Reflectivity)	T (Transmissivity)	$\epsilon$ (Emissivity)
5.000E+03	1.750E-03	2.000E-10	1.000E-06	8.051E-05	9.999E-01	3.511E-06
5.000E+03	8.749E-03	1.000E-09	5.000E-06	4.023E-04	9.996E-01	1.769E-05
5.000E+03	1.750E-02	2.000E-09	1.000E-05	8.042E-04	9.992E-01	3.543E-05
5.000E+03	8.749E-02	1.000E-08	5.000E-05	4.008E-03	9.958E-01	1.771E-04
5.000E+03	1.750E-01	2.000E-08	1.000E-04	7.982E-03	9.917E-01	3.539E-04
5.000E+03	8.749E-01	1.000E-07	5.000E-04	3.862E-02	9.596E-01	1.769E-03
5.000E+03	1.750E+00	2.000E-07	1.000E-03	7.424E-02	9.222E-01	3.534E-03
5.000E+03	3.500E+00	4.000E-07	2.000E-03	1.377E-01	8.552E-01	7.054E-03
5.000E+03	6.999E+00	8.000E-07	4.000E-03	2.404E-01	7.455E-01	1.405E-02
5.000E+03	1.050E+01	1.200E-06	6.000E-03	3.196E-01	6.594E-01	2.098E-02
5.000E+03	1.750E+01	2.000E-06	1.000E-02	4.328E-01	5.325E-01	3.462E-02
5.000E+03	8.749E+01	1.000E-05	5.000E-02	7.129E-01	1.405E-01	1.467E-01
5.000E+03	1.750E+02	2.000E-05	1.000E-01	7.415E-01	4.012E-02	2.184E-01
5.000E+03	8.749E+02	1.000E-04	5.000E-01	7.441E-01	2.564E-02	2.558E-01
5.000E+03	1.750E+03	2.000E-04	1.000E+00	7.441E-01	1.473E-01	2.559E-01
1.000E+04	1.745E-03	1.000E-10	1.000E-06	8.032E-05	9.999E-01	1.821E-06
1.000E+04	8.727E-03	5.000E-10	5.000E-06	4.014E-04	9.996E-01	8.817E-06
1.000E+04	1.745E-02	1.000E-09	1.000E-05	8.026E-04	9.992E-01	1.763E-05
1.000E+04	8.727E-02	5.000E-09	5.000E-05	3.999E-03	9.959E-01	8.858E-05
1.000E+04	1.745E-01	1.000E-08	1.000E-04	7.966E-03	9.919E-01	1.770E-04
1.000E+04	8.727E-01	5.000E-08	5.000E-04	3.858E-02	9.605E-01	8.848E-04
1.000E+04	1.745E+00	1.000E-07	1.000E-03	7.422E-02	9.240E-01	1.769E-03
1.000E+04	3.491E+00	2.000E-07	2.000E-03	1.379E-01	8.585E-01	3.534E-03
1.000E+04	6.982E+00	4.000E-07	4.000E-03	2.416E-01	7.514E-01	7.053E-03
1.000E+04	1.047E+01	6.000E-07	6.000E-03	3.221E-01	6.673E-01	1.056E-02
1.000E+04	1.745E+01	1.000E-06	1.000E-02	4.388E-01	5.437E-01	1.751E-02
1.000E+04	8.727E+01	5.000E-06	5.000E-02	7.530E-01	1.668E-01	3.021E-02
1.000E+04	1.745E+02	1.000E-05	1.000E-01	8.014E-01	6.425E-02	1.344E-01
1.000E+04	8.727E+02	5.000E-05	5.000E-01	8.109E-01	7.122E-02	1.890E-01
1.000E+04	1.745E+03	1.000E-04	1.000E+00	8.109E-01	1.481E-02	1.891E-01
1.000E+05	1.741E-03	1.000E-11	1.000E-06	8.017E-05	9.999E-01	1.520E-07
1.000E+05	8.707E-03	5.000E-11	5.000E-06	4.007E-04	9.996E-01	8.352E-07
1.000E+05	1.741E-02	1.000E-10	1.000E-05	8.011E-04	9.992E-01	1.803E-06
1.000E+05	8.707E-02	5.000E-10	5.000E-05	3.992E-03	9.960E-01	9.361E-06
1.000E+05	1.741E-01	1.000E-09	1.000E-04	7.952E-03	9.920E-01	1.773E-05
1.000E+05	8.707E-01	5.000E-09	5.000E-04	3.853E-02	9.614E-01	8.866E-05
1.000E+05	1.741E+00	1.000E-08	1.000E-03	7.420E-02	9.256E-01	1.773E-04
1.000E+05	3.483E+00	2.000E-08	2.000E-03	1.381E-01	8.615E-01	3.544E-04
1.000E+05	6.966E+00	4.000E-08	4.000E-03	2.426E-01	7.566E-01	7.088E-04
1.000E+05	1.045E+01	6.000E-08	6.000E-03	3.245E-01	6.745E-01	1.063E-03
1.000E+05	1.741E+01	1.000E-07	1.000E-02	4.443E-01	5.539E-01	1.771E-03
1.000E+05	8.707E+01	5.000E-07	5.000E-02	7.952E-01	1.961E-01	3.772E-03
1.000E+05	1.741E+02	1.000E-06	1.000E-01	8.783E-01	1.045E-01	1.717E-02
1.000E+05	8.707E+02	5.000E-06	5.000E-01	9.251E-01	8.686E-02	5.620E-02
1.000E+05	1.741E+03	1.000E-05	1.000E+00	9.357E-01	6.009E-02	6.373E-02

Table C-5. Optical properties in the visible ( $\lambda=0.55 \mu\text{m}$ ) of sooty water clouds (continued).

$\rho_{\text{H}_2\text{O}}/\rho_{\text{soot}}$	$\tau^*$ (Optical Depth)	$U_{\text{H}_2\text{O}}$ ( $\text{gm cm}^{-2}$ )	$U_{\text{soot}}$ ( $\text{gm cm}^{-2}$ )	R (Reflectivity)	T (Transmissivity)	$\epsilon$ (Emissivity)
1.000E+06	1.741E-03	1.000E-12	1.000E-06	8.024E-05	9.999E-01	0.000E+00
1.000E+06	8.705E-03	5.000E-12	5.000E-06	4.011E-04	9.996E-01	5.971E-08
1.000E+06	1.741E-02	1.000E-11	1.000E-05	8.004E-04	9.992E-01	1.790E-07
1.000E+06	8.705E-02	5.000E-11	5.000E-05	3.991E-03	9.960E-01	8.924E-07
1.000E+06	1.741E-01	1.000E-10	1.000E-04	7.951E-03	9.921E-01	1.778E-06
1.000E+06	8.705E-01	5.000E-10	5.000E-04	3.853E-02	9.615E-01	3.966E-06
1.000E+06	1.741E+00	1.000E-09	1.000E-03	7.420E-02	9.258E-01	1.800E-05
1.000E+06	3.482E+00	2.000E-09	2.000E-03	1.381E-01	8.619E-01	3.590E-05
1.000E+06	6.964E+00	4.000E-09	4.000E-03	2.427E-01	7.572E-01	7.181E-05
1.000E+06	1.045E+01	6.000E-09	6.000E-03	3.247E-01	6.752E-01	1.077E-04
1.000E+06	1.741E+01	1.000E-08	1.000E-02	4.448E-01	5.550E-01	1.796E-04
1.000E+06	8.705E+01	5.000E-08	5.000E-02	7.998E-01	1.993E-01	8.969E-04
1.000E+06	1.741E+02	1.000E-07	1.000E-01	8.880E-01	1.103E-01	1.790E-03
1.000E+06	8.705E+02	5.000E-07	5.000E-01	9.700E-01	2.153E-02	8.440E-03
1.000E+06	1.741E+03	1.000E-06	1.000E+00	9.776E-01	7.850E-03	1.450E-02
1.000E+07	1.741E-03	1.000E-13	1.000E-06	7.961E-05	9.999E-01	8.989E-08
1.000E+07	8.705E-03	5.000E-13	5.000E-06	4.021E-04	9.996E-01	0.000E+00
1.000E+07	1.741E-02	1.000E-12	1.000E-05	7.998E-04	9.992E-01	0.000E+00
1.000E+07	8.705E-02	5.000E-12	5.000E-05	3.990E-03	9.960E-01	9.854E-08
1.000E+07	1.741E-01	1.000E-11	1.000E-04	7.949E-03	9.921E-01	2.646E-07
1.000E+07	8.705E-01	5.000E-11	5.000E-04	3.853E-02	9.615E-01	1.111E-06
1.000E+07	1.741E+00	1.000E-10	1.000E-03	7.420E-02	9.258E-01	2.059E-06
1.000E+07	3.482E+00	2.000E-10	2.000E-03	1.382E-01	8.619E-01	4.142E-06
1.000E+07	6.964E+00	4.000E-10	4.000E-03	2.428E-01	7.572E-01	8.096E-06
1.000E+07	1.045E+01	6.000E-10	6.000E-03	3.247E-01	6.753E-01	1.217E-05
1.000E+07	1.741E+01	1.000E-09	1.000E-02	4.449E-01	5.551E-01	2.025E-05
1.000E+07	8.705E+01	5.000E-09	5.000E-02	8.002E-01	1.997E-01	1.013E-04
1.000E+07	1.741E+02	1.000E-08	1.000E-01	8.989E-01	1.109E-01	2.026E-04
1.000E+07	8.705E+02	5.000E-08	5.000E-01	9.750E-01	2.400E-02	1.006E-03
1.000E+07	1.741E+03	1.000E-07	1.000E+00	9.864E-01	1.166E-02	1.972E-03
1.000E+08	1.741E-03	1.000E-14	1.000E-06	9.151E-05	9.999E-01	9.607E-08
1.000E+08	8.705E-03	5.000E-14	5.000E-06	3.984E-04	9.996E-01	9.604E-08
1.000E+08	1.741E-02	1.000E-13	1.000E-05	7.965E-04	9.992E-01	0.000E+00
1.000E+08	8.705E-02	5.000E-13	5.000E-05	3.988E-03	9.960E-01	0.000E+00
1.000E+08	1.741E-01	1.000E-12	1.000E-04	7.953E-03	9.920E-01	0.000E+00
1.000E+08	8.705E-01	5.000E-12	5.000E-04	3.853E-02	9.615E-01	1.348E-07
1.000E+08	1.741E+00	1.000E-11	1.000E-03	7.420E-02	9.258E-01	5.338E-07
1.000E+08	3.482E+00	2.000E-11	2.000E-03	1.381E-01	8.619E-01	9.113E-07
1.000E+08	6.964E+00	4.000E-11	4.000E-03	2.428E-01	7.572E-01	1.748E-06
1.000E+08	1.045E+01	6.000E-11	6.000E-03	3.247E-01	6.753E-01	2.599E-06
1.000E+08	1.741E+01	1.000E-10	1.000E-02	4.449E-01	5.551E-01	4.385E-06
1.000E+08	8.705E+01	5.000E-10	5.000E-02	8.003E-01	1.997E-01	2.170E-05
1.000E+08	1.741E+02	1.000E-09	1.000E-01	8.990E-01	1.109E-01	4.338E-05
1.000E+08	8.705E+02	5.000E-09	5.000E-01	9.755E-01	2.427E-02	2.166E-04
1.000E+08	1.741E+03	1.000E-08	1.000E+00	9.874E-01	1.218E-02	4.312E-04

Table C-5. Optical properties in the visible ( $\lambda=0.55 \mu\text{m}$ ) of sooty water clouds (Concluded).

$\rho_{\text{H}_2\text{O}}/\rho_{\text{soot}}$	$\tau^*$ (Optical Depth)	$U_{\text{soot}}$ ( $\text{gm cm}^{-2}$ )	$U_{\text{H}_2\text{O}}$ ( $\text{gm cm}^{-2}$ )	R (Reflectivity)	T (Transmissivity)	$\epsilon$ (Emissivity)
1.000E+09	1.741E-03	1.000E-15	1.000E-06	7.970E-05	9.999E-01	6.038E-08
1.000E+09	8.705E-03	5.000E-15	5.000E-06	3.984E-04	9.996E-01	6.036E-08
1.000E+09	1.741E-02	1.000E-14	1.000E-05	7.964E-04	9.992E-01	6.034E-08
1.000E+09	8.705E-02	5.000E-14	5.000E-05	3.992E-03	9.960E-01	6.015E-08
1.000E+09	1.741E-01	1.000E-13	1.000E-04	7.953E-03	9.920E-01	0.000E+00
1.000E+09	8.705E-01	5.000E-13	5.000E-04	3.853E-02	9.615E-01	1.742E-07
1.000E+09	1.741E+00	1.000E-12	1.000E-03	7.420E-02	9.258E-01	2.796E-07
1.000E+09	3.482E+00	2.000E-12	2.000E-03	1.381E-01	8.618E-01	5.727E-07
1.000E+09	6.964E+00	4.000E-12	4.000E-03	2.428E-01	7.572E-01	1.098E-06
1.000E+09	1.045E+01	6.000E-12	6.000E-03	3.247E-01	6.753E-01	1.633E-06
1.000E+09	1.741E+01	1.000E-11	1.000E-02	4.449E-01	5.551E-01	2.755E-06
1.000E+09	8.705E+01	5.000E-11	5.000E-02	8.003E-01	1.997E-01	1.373E-05
1.000E+09	1.741E+02	1.000E-10	1.000E-01	8.891E-01	1.109E-01	2.745E-05
1.000E+09	8.705E+02	5.000E-10	5.000E-01	9.756E-01	2.430E-02	1.371E-04
1.000E+09	1.741E+03	1.000E-09	1.000E+00	9.875E-01	1.223E-02	2.735E-04
1.000E+10	1.741E-03	1.000E-16	1.000E-06	8.212E-05	9.999E-01	0.000E+00
1.000E+10	8.705E-03	5.000E-16	5.000E-06	3.987E-04	9.996E-01	0.000E+00
1.000E+10	1.741E-02	1.000E-15	1.000E-05	7.972E-04	9.992E-01	6.217E-08
1.000E+10	8.705E-02	5.000E-15	5.000E-05	3.997E-03	9.960E-01	6.197E-08
1.000E+10	1.741E-01	1.000E-14	1.000E-04	7.950E-03	9.921E-01	1.235E-07
1.000E+10	8.705E-01	5.000E-14	5.000E-04	3.853E-02	9.615E-01	1.795E-07
1.000E+10	1.741E+00	1.000E-13	1.000E-03	7.420E-02	9.258E-01	2.305E-07
1.000E+10	3.482E+00	2.000E-13	2.000E-03	1.382E-01	8.619E-01	5.365E-07
1.000E+10	6.964E+00	4.000E-13	4.000E-03	2.428E-01	7.572E-01	1.095E-06
1.000E+10	1.045E+01	6.000E-13	6.000E-03	3.247E-01	6.753E-01	1.599E-06
1.000E+10	1.741E+01	1.000E-12	1.000E-02	4.449E-01	5.551E-01	2.596E-06
1.000E+10	8.705E+01	5.000E-12	5.000E-02	8.003E-01	1.997E-01	1.294E-05
1.000E+10	1.741E+02	1.000E-11	1.000E-01	8.891E-01	1.109E-01	2.586E-05
1.000E+10	8.705E+02	5.000E-11	5.000E-01	9.756E-01	2.430E-02	1.292E-04
1.000E+10	1.741E+03	1.000E-10	1.000E+00	9.875E-01	1.224E-02	2.576E-04

\* Note that the optical depth is defined by Equation 2-36 and includes effects due to both scattering and absorption.



## APPENDIX D SOLUTIONS TO THE NUCLEAR WINTER MODELS

### THE PROBLEM OF FIGURE 3-1

The solution to the problem of Figure 3-1 is as follows:

In layer 1:

$$\begin{aligned} S &= (1-A_1) \Sigma \\ U &= \frac{1}{2} (1-A_1) (1-A_2) \Sigma (2 + \epsilon_{I_1} z_1) \\ D &= \frac{1}{2} (1-A_1) (1-A_2) \Sigma \epsilon_{I_1} z_1 \\ \tau &= \frac{1}{2} (1-A_1) (1-A_2) \Sigma (1 + \epsilon_{I_1} z_1) \end{aligned} \tag{D-1}$$

where  $z_1$  measures the distance from the top of layer 1.

In layer 2:

$$\begin{aligned} S &= (1-A_1) (1-A_2) \Sigma e^{-\epsilon_{S_2} z_2} \\ U &= \frac{1}{2} (1-A_1) (1-A_2) \Sigma [1 + \alpha + \mu_{I_1} + (1-\alpha) e^{-\epsilon_{S_2} z_2}] \\ D &= \frac{1}{2} (1-A_1) (1-A_2) \Sigma [1 + \alpha + \mu_{I_1} - (1+\alpha) e^{-\epsilon_{S_2} z_2}] \\ \tau &= \frac{1}{2} (1-A_1) (1-A_2) \Sigma [1 + \alpha + \mu_{I_1} + (\frac{1}{2} - \alpha) e^{-\epsilon_{S_2} z_2}] \end{aligned} \tag{D-2}$$

where  $z_2$  is the distance from the top of layer 2.

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In layer 3:

$$S = (1-A_1) (1-A_2) \Sigma e^{-\mu s_2}$$

$$U = \frac{1}{2} (1-A_1) (1-A_2) \Sigma [1 + \alpha + \mu_{I_1} + (1-\alpha) e^{-\mu s_2} + e^{-\mu s_2} \epsilon_{I_3} z_3] \quad (D-3)$$

$$D = \frac{1}{2} (1-A_1) (1-A_2) \Sigma [1 + \alpha + \mu_{I_1} - (1+\alpha) e^{-\mu s_2} + e^{-\mu s_2} \epsilon_{I_3} z_3]$$

$$\tau = \frac{1}{2} (1-A_1) (1-A_2) \Sigma [1 + \mu_{I_1} + \alpha(1-e^{-\mu s_2}) + e^{-\mu s_2} \epsilon_{I_3} z_3]$$

where  $z_3$  is the distance from the top of layer 3.

For the earth:

$$\tau = \frac{1}{2} (1-A_1) (1-A_2) \Sigma [1 + \mu_{I_1} + (1 + \mu_{I_3}) e^{-\mu s_2} + \alpha(1-e^{-\mu s_2})] \quad (D-4)$$

#### THE PROBLEM OF FIGURE 3-4

An approximate solution to the problem of Figure 3-4 in the case  $\mu_{I_1}=0$  and defining  $A \equiv (1-A_1) (1-A_2)$  is as follows:

In the convection zone:

$$S = A \Sigma e^{-\epsilon s_2} z_2$$

$$U = \sigma \left[ (T_0 + \beta z_2)^4 + 4 \frac{\beta}{\epsilon_{I_2}} (T_0 + \beta z_2)^3 + 12 \left( \frac{\beta}{\epsilon_{I_2}} \right)^2 (T_0 + \beta z_2)^2 + 24 \left( \frac{\beta}{\epsilon_{I_2}} \right)^3 (T_0 + \beta z_2) + 24 \left( \frac{\beta}{\epsilon_{I_2}} \right)^4 \right] - \frac{\epsilon s_2}{\epsilon_{I_2}} \Sigma A e^{-\epsilon s_2} d \quad (D-5)$$

$$e^{-\epsilon_{I_2} d} e^{\epsilon_{I_2} z_2}$$

$$\begin{aligned}
D = & \sigma \left[ (T_0 + \beta z_2)^4 - 4 \frac{\beta}{\epsilon_{I_2}} (T_0 + \beta z_2)^3 + 12 \left( \frac{\beta}{\epsilon_{I_2}} \right)^2 (T_0 + \beta z_2)^2 \right. \\
& - 24 \left( \frac{\beta}{\epsilon_{I_2}} \right)^3 (T_0 + \beta z_2) + 24 \left( \frac{\beta}{\epsilon_{I_2}} \right)^4 \left. \right] - [T_0^4 - \\
& 4 \left( \frac{\beta}{\epsilon_{I_2}} \right) T_0^3 + 12 \left( \frac{\beta}{\epsilon_{I_2}} \right)^2 T_0^2 - 24 \left( \frac{\beta}{\epsilon_{I_2}} \right)^3 T_0 + 24 \left( \frac{\beta}{\epsilon_{I_2}} \right)^4] e^{-\epsilon_{S_2} z_2}
\end{aligned}$$

$$T = T_0 + \beta z_2$$

where  $z_2$  is the distance from the top of the convection zone.

In the convection-free region of layer 2

$$S = A \Sigma e^{-\epsilon_{S_2} z_2}$$

$$U = \frac{1}{2} [A \Sigma e^{-\epsilon_{S_2} d} \{ (1-\alpha) e^{-\epsilon_{S_2} z_2'} + \alpha - \frac{1}{\alpha} \} + 2\sigma(T_0 + \beta d)^4] \quad (D-6)$$

$$D = \frac{1}{2} [A \Sigma e^{-\epsilon_{S_2} d} \{ -(1+\alpha) e^{-\epsilon_{S_2} z_2'} + \alpha - \frac{1}{\alpha} \} + 2\sigma(T_0 + \beta d)^4]$$

$$\tau = \frac{1}{2} [A \Sigma e^{-\epsilon_{S_2} d} (\alpha - \frac{1}{\alpha}) (1 - e^{-\epsilon_{S_2} z_2'}) + 2\sigma(T_0 + \beta d)^4]$$

where  $z_2'$  is the distance from the top of the convection-free region of layer 2.

In layer 3:

$$S = A \Sigma e^{-\mu s_2}$$

$$U = \frac{1}{2} [2\sigma(T_0 + \beta d)^4 + A\Sigma\{(\alpha + \frac{1}{\alpha}) e^{-\epsilon s_2^d} - \alpha e^{-\mu s_2} + e^{-\mu s_2}(1 + \epsilon_{I_3} z_3)\}]$$

$$D = \frac{1}{2} [2\sigma(T_0 + \beta d)^4 + A\Sigma\{(\alpha + \frac{1}{\alpha}) e^{-\epsilon s_2^d} - \alpha e^{-\mu s_2} + e^{-\mu s_2}(-1 + \epsilon_{I_3} z_3)\}] \quad (D-7)$$

$$\tau = \frac{1}{2} [2\sigma(T_0 + \beta d)^4 + A\Sigma\{(\alpha - \frac{1}{\alpha}) e^{-\epsilon s_2^d} - \alpha e^{-\mu s_2} + e^{-\mu s_2} \epsilon_{I_3} z_3\}]$$

where  $z_3$  is the distance from the top of layer 3.

For the earth:

$$\tau = \frac{1}{2} [2\sigma(T_0 + \beta d)^4 + A\Sigma\{(\alpha - \frac{1}{\alpha}) e^{-\epsilon s_2^d} - \alpha e^{-\mu s_2} + e^{-\mu s_2} (1 + \mu_{I_3})\}] \quad (D-8)$$

In the above equations:

$$T_0 = T_B - \frac{\beta}{\epsilon_{I_2}}$$

$$D = -\frac{1}{\epsilon_{s_2}} \ln \frac{8\beta}{T_B (\epsilon_{I_2} + \epsilon_{s_2})}$$

where  $T_B \equiv \left[ \frac{A}{\sigma} \Sigma \right]^{1/4}$

## THE CASE OF HIGH SURFACE ALBEDO

For the solar fluxes in the case where the earth has an albedo,  $A_e$ , in the solar we have:

Above layer 1:

$$S_D = \Sigma$$

$$S_U = \Sigma \left[ A_1 + A_2 - A_1 A_2 + \frac{(1-A_1)^2 (1-A_2)^2 A_e e^{-2\mu s_2}}{1 - A_2 A_e - A_1 A_e (1-A_2) e^{-2\mu s_2}} \right] \quad (D-9)$$

In layer 1:

$$S_D = (1-A_1) \Sigma$$

$$S_U = \Sigma \left[ A_2 (1-A_1) + \frac{(1-A_1)^2 (1-A_2)^2 A_e e^{-2\mu s_2}}{1 - A_2 A_e - A_1 A_e (1-A_2) e^{-2\mu s_2}} \right] \quad (D-10)$$

In layer 2:

$$S_D = \Sigma \left[ (1-A_1) (1-A_2) + \frac{A_1 (1-A_1)^2 (1-A_2)^2 A_e e^{-2\mu s_2}}{1 - A_2 A_e - A_1 A_e (1-A_2) e^{-2\mu s_2}} \right] e^{-\epsilon s_2} z_2 \quad (D-11)$$

$$S_U = \Sigma \left[ \frac{(1-A_1) (1-A_2)^2 A_e e^{-2\mu s_2}}{1 - A_2 A_e - A_1 A_e (1-A_2) e^{-2\mu s_2}} \right] e^{\epsilon s_2} z_2$$

where  $z_2$  is the distance from the top of layer 2.

In layer 3:

$$S_D = \frac{\Sigma (1-A_1) (1-A_2) e^{-\mu s_2}}{1 - A_2 A_e - A_1 A_e (1-A_2) e^{-2\mu s_2}}$$

(D-12)

$$S_U = \frac{\Sigma (1-A_1) (1-A_2) A_e e^{-\mu s_2}}{1 - A_2 A_e - A_1 A_e (1-A_2) e^{-2\mu s_2}}$$

## APPENDIX E

### CONVECTIVE EQUILIBRIUM WITH MULTIPLE IR GROUPS

In this appendix we shall demonstrate that a region as might be formed by the NRC baseline, soot and water-vapor layer (Reference E-1) can be represented by a set of IR groups with constant opacities such that the resulting temperature profile is significantly different from that for a single IR group. In particular, if the range of IR opacities needed to represent the water-vapor emissivity includes opacities both less than and greater than the solar opacity, the temperature profile will always have a peak at about one solar optical depth. The temperature gradient, in the absence of convection, on the top of the layer will normally exceed the critical lapse rate.

Without using a dynamical model for the profile changes which result from convection, it is difficult to be confident that a complete understanding has been gained. However, it is possible to include a convective flux component with transfer equations in order to find a new equilibrium condition which has a convective layer which holds the temperature gradient at the critical lapse rate through a modest mixing of the unstable region with the optically inert atmosphere above it. This results in a modified temperature profile including an altered asymptotic temperature at the base of the soot layer.

#### OPTICAL PROPERTIES OF THE LAYER

The NRC baseline, 30°-70° N case shows that after 25 days a minimum surface temperature is reached and at this time the optical depth

for solar extinction is 2.5 due to the presence of soot which is taken to be uniformly distributed from 0 to 9 km above the surface. The optical depth is the product of the physical depth,  $z$ , and the solar opacity,  $\chi_s$ , so we can take  $\chi_s \approx 0.25 \text{ km}^{-1}$ . The broad-band infrared emissivity,  $\bar{\epsilon}$ , is mainly from water vapor and its behavior with path length,  $U$ , is given by Figure E-1.

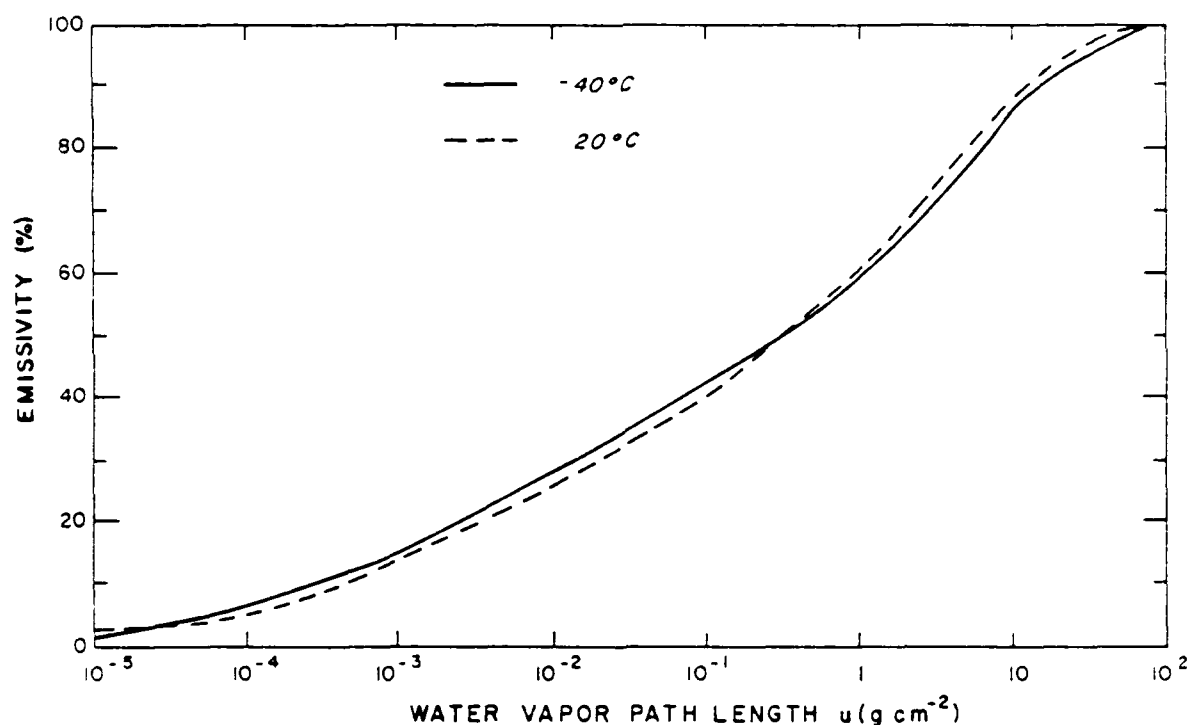


Figure E-1. Broad-band IR emissivity for water vapor (from Reference 2-10).

In the absence of scattering and for a parallel beam, the emissivity is related to the path length by

$$\bar{\epsilon} = 1 - e^{-\bar{k}U} \quad (\text{E-1})$$



where  $\bar{k}$  is a mean mass absorption coefficient with units of  $\text{cm}^2 \text{g}^{-1}$ . Here  $\bar{k}U$  is the optical depth.

The NRC baseline case provides for a water-vapor pathlength of  $1.45 \text{ gm cm}^{-2}$  giving an emissivity of 0.63 from Figure E-1. Thus, the optical depth for water vapor will be very nearly one for a mean opacity over a 9 km depth of  $\bar{\chi}_{\text{H}_2\text{O}} \approx 0.1 \text{ km}^{-1}$ .

Use of this mean value will give the correct emissivity at  $U = 1.45 \text{ gm/cm}^2$  but it would provide a very poor representation for the  $\bar{\epsilon}(U)$  curve of Figure E-1. In fact,  $\bar{\epsilon}(U)$  results from an averaging over a complex absorption structure. It is possible to represent this curve as resulting from a set of IR groups with significantly different optical properties. For example, a reasonable fit to  $\bar{\epsilon}(U)$  is given by

$$\begin{aligned} \bar{\epsilon} \approx & .2(1 - e^{-1300U}) + .2(1 - e^{-50U}) \\ & + .3(1 - e^{-U}) + .3(1 - e^{-.12U}) \end{aligned} \quad (\text{E-2})$$

over the range of  $U$  from  $10^{-4}$  to  $10^2$ . This form for  $\bar{\epsilon}$  would result if there were a set of four distinct IR frequency bands which contributed with uniform opacities within each band. The opacities  $\chi = k\rho$  of the four groups in this fit correspond to, for this mean density if  $\rho \sim 10^{-6} \text{ gm/cm}^3$ , values of  $130 \text{ km}^{-1}$ ,  $5 \text{ km}^{-1}$ ,  $0.1 \text{ km}^{-1}$ , and  $0.012 \text{ km}^{-1}$ . Recall that the solar opacity was  $\chi_s \approx 0.1 \text{ km}^{-1}$  so that there are IR groups with significant activities which are both more and less active than the solar absorption.

## TRANSFER EQUATIONS

The equation for the steady state radiative transfer for a planar atmosphere can be written as (Reference E-2)

$$\mu \frac{\partial I}{\partial z} = \eta - \chi I \quad (E-3)$$

where the specific intensity  $I(z, \hat{n}, \nu)$  is a function of position  $z$ , direction and frequency and has units of  $\text{ergs cm}^{-2} \text{ sec}^{-1} \text{ Hz}^{-1} \text{ sr}^{-1}$ . Here  $\mu$  is the cosine of the angle relative to vertical while  $\eta$  is the emission coefficient and  $\chi$  is the opacity with units of  $\text{cm}^{-1}$ . Generally  $\chi$  is the sum of absorption and scattering contributions but, for the present discussion, scattering will be ignored. Given  $\eta$  and  $\chi$ , both possibly functions of frequency, direction, and position, it is possible to solve for  $I$ . However, in general,  $\eta$  and  $\chi$  are functions of  $I$ , providing a nonlinear transfer equation. In a uniform medium at steady state there can be no net energy accumulation or loss so the emission coefficient and opacity are related by

$$\eta(\nu) = \chi(\nu) I(\hat{n}, \nu) \quad (E-4)$$

which is Kirchoff's law. For an enclosure in strict thermodynamic equilibrium the radiation field is given by the Planck function at temperature  $T$  so

$$\eta(\nu) = \chi(\nu) B_{\nu}(T) \quad (E-5)$$

If a medium has only small gradient lengths relative to photon mean free paths the approximation of local thermodynamic equilibrium (LTE) is often useful and this implies

$$\eta(z, \nu) = \chi(z, \nu) B_{\nu}(T) \quad (E-6)$$

so that the emissivity can be expressed in terms of the opacity and the known Planck function. Here  $B_{\nu}(T)$  has the property that the flux from a blackbody is

$$\sigma T^4 = \pi \int_0^{\infty} B_{\nu}(T) d\nu \quad (E-7)$$

which defines the Stefan-Boltzmann constant,  $\sigma$ .

Consider now an idealized atmospheric layer which has the properties that there are a finite number of infrared frequency ranges of importance and each of these has constant opacity. We assume that all thermal radiation takes place in these groups and that the solar spectrum does not significantly overlap the IR. Thus there is no emission into the solar spectrum. The layer then serves to absorb the solar radiation and convert the energy to thermal.

### THREE GROUPS

In order to get an analytic handle on the problem, we will now develop a set of transfer equations appropriate for a three-group two-stream approximation where the three groups consist of two IR groups and one solar group. The transfer equation under LTE is

$$\mu \frac{\partial I}{\partial z} = \chi(\nu)(B_{\nu}(T) - I) \quad (E-8)$$

Integrating over the frequency domains gives

$$\mu \frac{\partial I_1}{\partial z} = \chi_1(\alpha_1 \frac{\sigma T^4}{\pi} - I_1) \quad (E-9a)$$

$$\mu \frac{\partial I_2}{\partial z} = \chi_2(\alpha_2 \frac{\sigma T^4}{\pi} - I_2) \quad (E-9b)$$

and

$$\mu \frac{\partial I_s}{\partial z} = -\chi_s I_s \quad (E-9c)$$

Here the  $\chi_i$  are the opacities of IR groups and  $\alpha_i$  is the fraction of the thermal emission which takes place into the  $i^{\text{th}}$  group. Both  $\chi_i$  and  $\alpha_i$  will be taken as known. (The opacities  $\chi_i$  may be considered to be the product of the density and mass absorption coefficient.)

## TWO STREAMS

The full solution to the transfer equations includes the angular dependence of the specific intensity. The details of this dependence are not expected to have a significant impact on the result and it is convenient to make an approximation which allows closure of the set of moment equations generated by Equation E-3. Eddington's approximation provides that the upward and downward components of  $I$  are each independent of  $\mu$  but different from each other.

The flux associated with  $I$  is

$$\text{Flux} = \int \mu I(\mu) d\mu d\phi \quad (\text{E-10})$$

and defining  $I^+ \equiv I(\mu > 0)$  and  $I^- \equiv I(\mu < 0)$  the upward flux is

$$U = \int_0^1 \mu I^+ d\mu \int d\phi = \pi I^+ \quad (\text{E-11})$$

and the downward flux is

$$D = - \int_{-1}^0 \mu I^- d\mu \int d\phi = \pi I^- \quad (\text{E-12})$$

Thus, from Equation E-7 upon integration over angle

$$\frac{\partial}{\partial z} (U_i) = 2 \chi_i \alpha_i \sigma T^4 - 2 \chi_i U_i \quad (\text{E-13a})$$

$$\frac{\partial}{\partial z} (-D_i) = 2 \chi_i \alpha_i \sigma T^4 - 2 \chi_i D_i \quad (\text{E-13b})$$

for  $i = 1, 2$ . Since the solar flux is only down,  $\pi I_s = S$  and

$$\frac{\partial(S)}{\partial z} = 2 \chi_s S \quad . \quad (E-14)$$

Finally taking  $\tau \equiv -2z$  as a convenient unit of depth and expressing the IR fluxes in terms of plus,  $P = U+D$ , and minus,  $M=U-D$  components, we arrive at

$$\frac{\partial}{\partial \tau} (P_i) = \chi_i M_i \quad (E-15a)$$

$$\frac{\partial}{\partial \tau} (M_i) = \chi_i P_i - 2 \chi_i \alpha_i \sigma T^4 \quad (E-15b)$$

$$\frac{\partial}{\partial \tau} (S) = - \chi_s S \quad (E-15c)$$

which give the three-group, two-stream transfer equations. The steady state condition implies

$$\frac{\partial}{\partial \tau} (\sum M_i - S) = 0 \quad . \quad (E-16)$$

These results are correct for any number of IR groups. However, the essential features appear with two groups and this case can be solved analytically, providing a solution as follows:

$$S = S_0 \exp(-\chi_s \tau) \quad (E-17a)$$

$$M_1 = A \exp(\sqrt{\gamma} \tau) + B \exp(-\sqrt{\gamma} \tau) + X \exp(\sqrt{\gamma} \tau) \quad (E-17b)$$

$$M_2 = S - M_1 \quad (E-17c)$$

$$P_1 = P_{10} + \chi_1 \left[ \frac{A}{\sqrt{\gamma}} (\exp(\sqrt{\gamma} \tau) - 1) - \frac{B}{\sqrt{\gamma}} (\exp(-\sqrt{\gamma} \tau) - 1) \right. \\ \left. + \frac{X}{\chi_s} (\exp(-\chi_s \tau) - 1) \right] \quad (E-17d)$$

$$P_2 = P_{20} + \chi_1 \left[ -\frac{A}{\sqrt{\gamma}} (\exp(\sqrt{\gamma} \tau) - 1) + \frac{B}{\sqrt{\gamma}} (\exp(\sqrt{\gamma} \tau) - 1) - \frac{S_0 - X}{\chi_s} (\exp(-\chi_s \tau) - 1) \right] \quad (E-17e)$$

where  $S_0$  is the incident solar flux at the upper surface,  $\tau=0$ ,

$$\gamma = \frac{(\alpha_1 \chi_2 + \alpha_2 \chi_1) \chi_1 \chi_2}{(\alpha_1 \chi_1 + \alpha_2 \chi_2)} \quad (E-18)$$

and

$$X = S_0 \frac{\alpha_1 \chi_1}{\alpha_1 \chi_1 + \alpha_2 \chi_2} \frac{\chi_2^2 - \chi_s^2}{\gamma - \chi_2^2} \quad (E-19)$$

Finite fluxes in an infinitely deep layer requires  $A=0$  so that

$$B = \frac{\frac{1}{\alpha_2} \left[ (S_0 - X) \left( 1 + \frac{\chi_s}{\chi_2} \right) + 2 D_{20} \right] - \frac{1}{\alpha_1} \left[ X \left( 1 + \frac{\chi_s}{\chi_1} \right) + 2 D_{10} \right]}{\sqrt{\gamma} \left( \frac{1}{\alpha_1 \chi_1} + \frac{1}{\alpha_2 \chi_2} \right) + \frac{1}{\alpha_1} + \frac{1}{\alpha_2}} \quad (E-20)$$

where  $D_{10}$  provides for possible non-zero downward fluxes at  $\tau=0$ . The boundary conditions at  $\tau=0$  are

$$M_{10} = B + X = P_{10} - 2 D_{10} \quad (E-21a)$$

and

$$M_{20} = S_0 - M_{10} = P_{20} - 2 D_{20} \quad (E-21b)$$

These conditions provide the full solution for an infinitely deep region consisting of two IR groups and a solar group.

To illustrate the behavior exhibited by these conditions for a single layer, consider an example of equal strength IR groups ( $\alpha_1 = \alpha_2 =$

0.5) with arbitrary normalization of  $\chi_1 = 1$  and  $\chi_2 = 10^{-2}$ . The temperature profiles which result are shown for several values of  $\chi_s$  in Figure E-2. If  $\chi_s < \chi_2$  the temperature increases with depth to an asymptotic value. If  $\chi_2 < \chi_s < \chi_1$  the temperature reaches a maximum at a depth comparable to  $\chi_s^{-1}$ , or at a solar optical depth near 1. If  $\chi_s > \chi_1$  the temperature monotonically decreases while if  $\chi_s \gg \chi_1$  one sees structure at both of the depth scales of  $\chi_s^{-1}$  and  $(\sqrt{\chi_1 \chi_2})^{-1/2}$  but the temperature still decreases monotonically.

As illustrated by the previous discussion of soot layer optical properties, the activities of the equivalent IR groups span that for the solar radiation. In order to demonstrate the basic features expected in a realistic temperature profile, let us approximate the water-vapor emissivity using just two IR groups. We will take

$$\bar{\epsilon}(z) \approx .4 (1 - e^{-12.5z}) + .3(1 - e^{-0.0625z}) \quad (\text{E-22})$$

where  $z$  is in kilometers. Thus we are using  $\alpha_1 = .4$ ,  $\chi_1 = 12.5 \text{ km}^{-1}$ ,  $\alpha_2 = .3$ , and  $\chi_2 = 1/16 \text{ km}^{-1}$ , while taking  $\chi_s = 1/4 \text{ km}^{-1}$ . The above fit to  $\bar{\epsilon}(U)$  is not very good unless  $U \sim 1$  but the essential feature is preserved--namely, there are IR groups both more and less active than the solar. The exact values for  $\alpha_1$  and  $\chi_1$  are not well determined by such a fit but it turns out that the essential features of solution remain largely independent of the selection of parameter values.

The temperature profile which results from the two IR groups plus one solar group approximation for two streams is shown in Figure E-3. Since  $\chi_2 < \chi_s < \chi_1$ , there is a maximum temperature which occurs and it is at a depth of  $\tau = 2z = 2.2 \text{ km}$ , which corresponds to a solar optical depth of  $\sim 1/2$ . The temperature gradient at the top of the layer greatly exceeds the critical lapse rate of about 7 degrees per kilometer so that the profile will be unstable against convection. The resulting convection

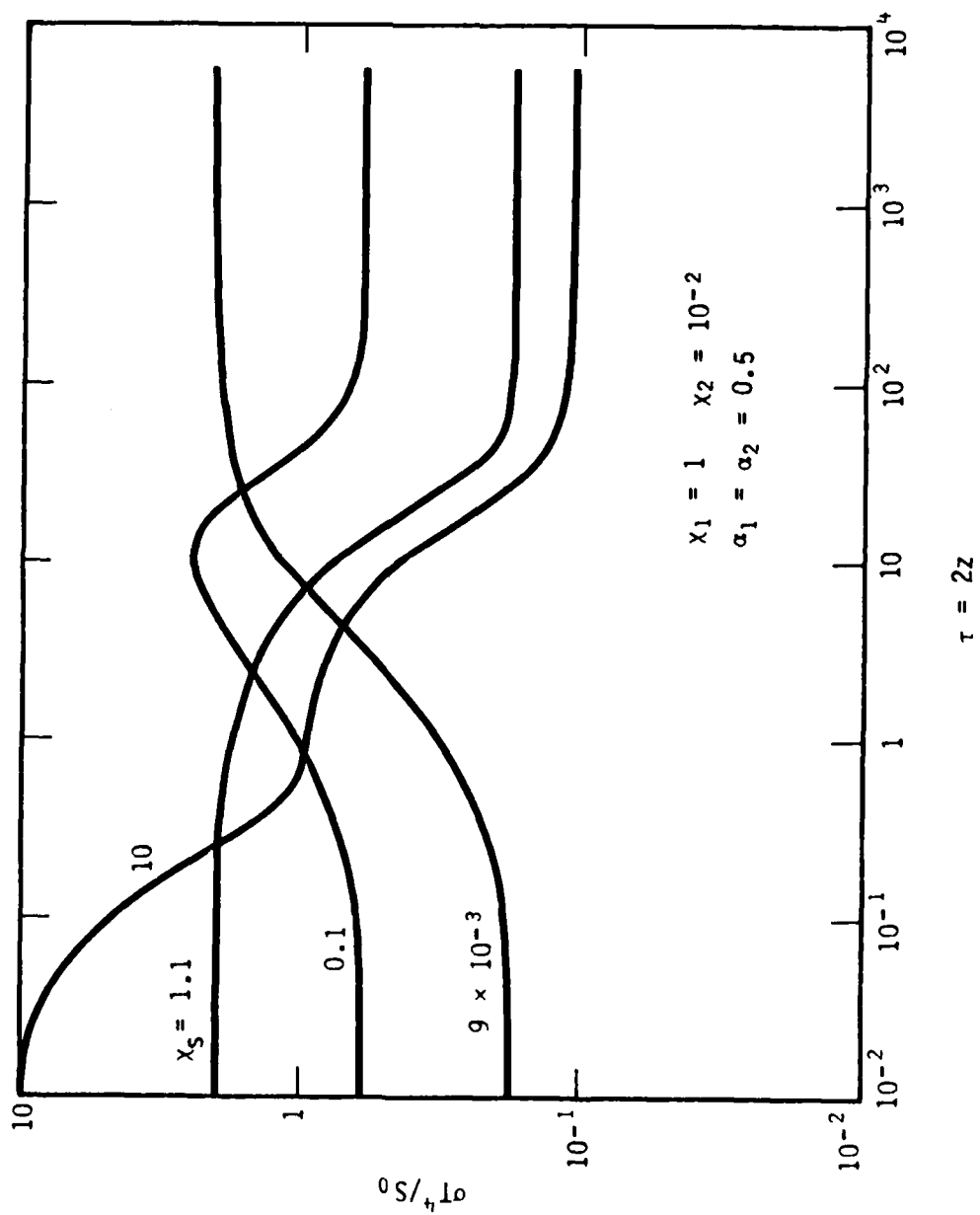


Figure E-2. Temperature profiles for two IR groups plus solar absorption.



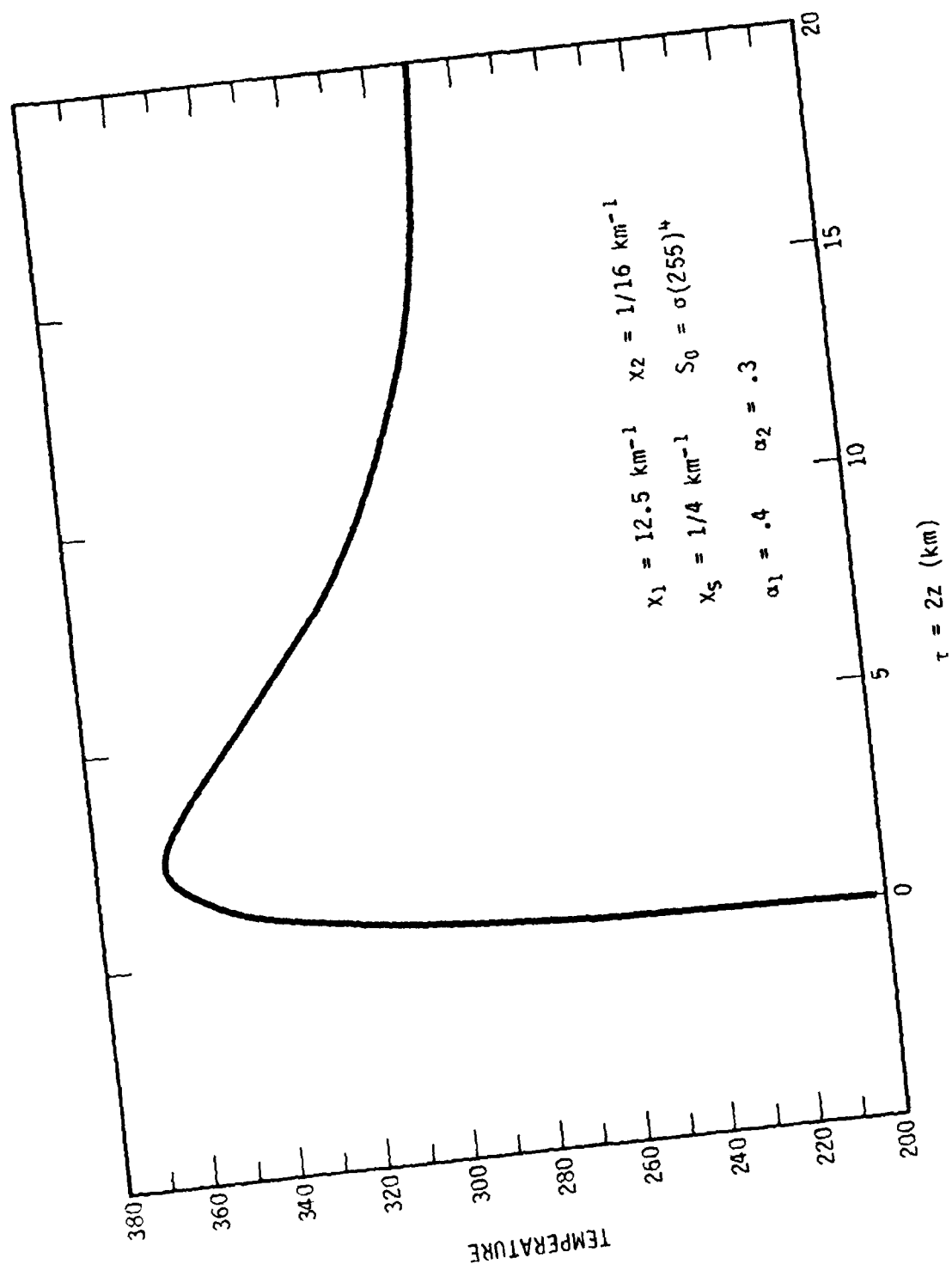


Figure E-3. Temperature profile for two IR group approximation in a soot layer.

will alter the profile so that the gradient will not exceed the critical lapse rate anywhere. It is not clear that there will exist a steady state profile maintained by convection. Without entering into a dynamical calculation we now want to consider the character of a possible steady state profile which is maintained by convection, allowing for the possibility that a portion of the layer may mix with air above to reduce the opacities and effectively expand the layer.

### CONVECTIVE LIMIT

In a region in which convection enforces a maximum gradient equal to some critical lapse rate,  $\beta$ , our previous solution for 2 IR groups is inappropriate. In such a region the gradient will be constant at  $\beta$  and there will exist an additional flux from the convection.

The transfer equations for the IR and solar groups are the same as in the absence of convection. Namely,

$$\frac{\partial}{\partial \tau} (P_i) = \chi_i M_i \quad (E-23a)$$

$$\frac{\partial}{\partial \tau} (M_i) = \chi_i P_i - 2 \chi_i \alpha_i \sigma T^4 \quad (E-23b)$$

$$S = S_0 e^{-\chi_s \tau} \quad (E-23c)$$

but the steady state condition becomes

$$\frac{\partial}{\partial \tau} (\sum M_i - S + F) = 0 \quad (E-24)$$

where  $F$  is the convective flux. Furthermore, the temperature now is restricted to the form

$$T = T_0 + \beta \tau \quad (E-25)$$

where  $\beta$  is the critical gradient and  $T_0$  is an unknown temperature at the top of the layer.

Eliminating  $M_i$  using Equations E-23a and b, while making use of Equation E-25, yields

$$-\frac{1}{x_i} \frac{\partial^2 p_i}{\partial \tau^2} + x_i p_i = 2x_i \alpha_i T_0^4 \left(1 + \left(\frac{\beta}{T_0}\right)\tau\right) \quad (E-26)$$

which has a general solution of the form

$$p_i = A_i e^{-x_i \tau} + B_i e^{x_i \tau} + \sum_{j=0}^4 a_{ij} \tau^j \quad (E-27)$$

The coefficients  $a_{ij}$  can be expressed in terms of  $T_0$  as

$$\begin{aligned} a_{i4} &= 2 \alpha_i \sigma T_0^4 (\beta/T_0)^4 \\ a_{i3} &= 2 \alpha_i \sigma T_0^4 (4(\beta/T_0)^3) \\ a_{i2} &= 2 \alpha_i \sigma T_0^4 (6(\beta/T_0)^2) + 12 a_{i4}/x_i^2 \\ a_{i1} &= 2 \alpha_i \sigma T_0^4 (4(\beta/T_0)) + 6 a_{i3}/x_i^2 \\ a_{i0} &= 2 \alpha_i \sigma T_0^4 + 2 a_{i2}/x_i^2 \end{aligned} \quad (E-28)$$

Using Equation (E-23a) the  $M_i$  can be written as

$$M_i = -A_i e^{-x_i \tau} + B_i e^{x_i \tau} + \sum_{j=1}^4 j a_{ij} \tau^{j-1} \quad (E-29)$$

For no downward flux at the boundary at  $\tau=0$

$$P_{i0} = M_{i0} \quad (E-30)$$

and

$$A_i = (a_{i1}/x_i - a_{i0})/2 \quad (E-31)$$

Furthermore, fixing the convective flux to be zero at  $\tau=0$  forces

$$\sum P_{i0} = \sum M_{i0} = S_0 \quad (E-32)$$

which requires

$$\sum B_i = S_0 - \sum_i (a_{i1}/x_i + a_{i0})/2 \quad (E-33)$$

Thus the remaining unknowns are  $T_0$  and  $B_1$ . (From Equation E-33  $B_1 + B_2$  can be written in terms of  $T_0$ . So it is only the split between the  $B_i$  which is unknown.)

The convective flux can be found by integrating Equation E-24, giving

$$\begin{aligned} F = S_0(e^{-x_s \tau} - 1) - \left[ \sum_i A_i(e^{-x_i \tau} - 1) + \sum_i B_i(e^{x_i \tau} - 1) \right. \\ \left. + \sum_i \sum_{j=2}^4 j \left( \frac{a_{ij}}{x_i} \right) \tau^{j-1} \right] \end{aligned} \quad (E-34)$$

where the condition  $F=0$  at  $\tau=0$  is imposed giving no convective flux at the boundary.

Figure E-3 indicates that in the absence of convection there will be a finite region with a temperature gradient exceeding the critical lapse rate. Since this region is unstable to convection, it will be

altered through convection, perhaps including a mixing with the inactive region above and also perhaps dynamically changing the previously stable region below. Without exploring the dynamics of such processes, we shall now consider the possibility that there may exist a different steady state equilibrium in which convection holds the upper region at a gradient  $\beta$  while the semi-infinite lower region is unaltered except for possible changes in boundary conditions at the interface. This new configuration is to allow the possibility that, through mixing, the upper region is uniformly stretched, if necessary, to provide a solution which matches the boundary conditions at the interface. This stretching will be carried out by a uniform reduction of the  $\chi$ 's in the upper region such that their ratios are fixed.

The conditions to be met are as follows:

The convective flux,  $F$ , is to vanish at the top ( $\tau=0$ ) and at the interface,  $\tau_0$ .

The gradient of the convective flux,  $\partial F/\partial \tau$ , is to vanish at the interface--this forces the temperature to be continuous.

All IR fluxes  $M_i$  and  $P_i$  are to be continuous at the interface--actually only one of the four conditions is independent.

The maximum temperature gradient in the lower non-convective region must be no greater than  $\beta$ .

In general, it is found that parameters  $\tau_0$ ,  $T_0$ , and  $B_1$  (or, equivalently, the mix between  $B_1$  and  $B_2$ ) can be found which satisfy the above conditions without any stretching or mixing of the upper convective region.

It is further found that there exist solutions with a stretching up to some maximum value beyond which the temperature gradient at the top of the nonconvective lower region exceeds  $\beta$ . The maximum allowed stretching is generally no more than about 50 percent for typical parameters. Any degree of stretching less than this maximum results in a discontinuity in the temperature gradient at the interface. While there is no physical reason to rule out such a possibility, it seems likely that the dynamics of the change from an unstable profile to one maintained by convection would not leave such a discontinuity. This reasoning is further supported by the example in Figure E-4, which indicates that the final convective region is much larger than the original region for which  $dT/d\tau > \beta$ .

Figure E-4 shows three temperature profiles which result from opacities which approximate those for a soot layer. The profiles are for a fully nonconvective equilibrium (ORIGINAL), for an unstretched convective layer above a stable layer (UNSTRETCHED), and for a stretched convective layer above a stable layer such that the temperature gradient is continuous across the interface (STRETCHED).

The effect of introduction of a convectively stabilized layer is generally a reduction in temperatures at the peak and at the bottom of the region with an attendant sharp increase in the temperature at the top of the layer. The temperature peak of the original region is at a solar optical depth,  $x_s\tau$ , of about 1/2 while the convection induced peak is at an optical depth of about 2.

#### REMARKS

The goal of the, currently incomplete, work described in this appendix is to understand the development of the instability at the top of the soot layer when no condensation cloud is present. The most obvious conclusion of the work so far is that it is necessary to resolve the IR

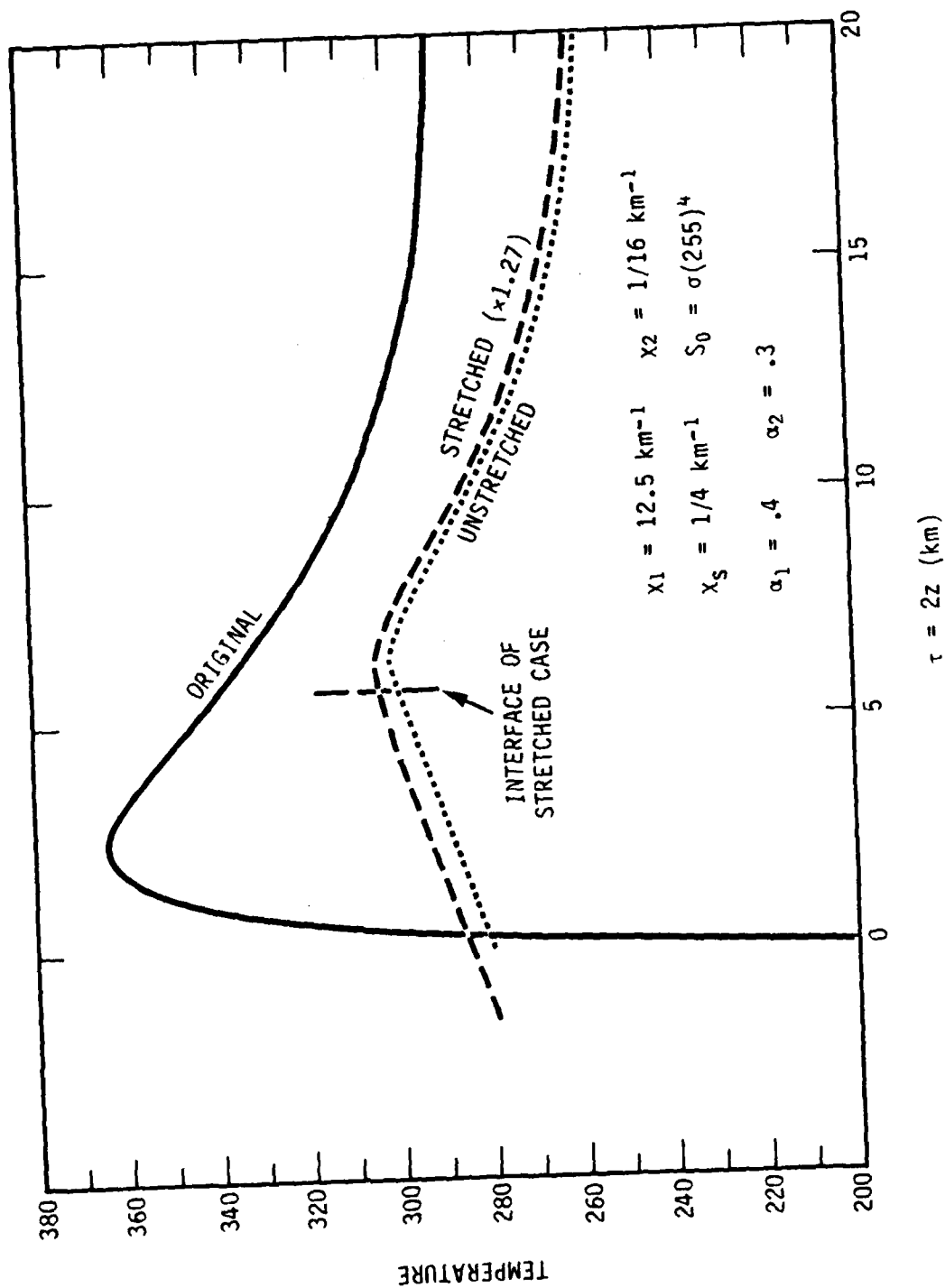


Figure E-4. Temperature profiles for two IR group approximation in a soot layer (ORIGINAL), under convective equilibrium (UNSTRETCHED) and following a mixing with the layer above (STRETCHED).

opacity of  $H_2O$  into more than one band unlike was done in Chapter 3. If there are portions of the IR band where the opacity is higher than is the solar opacity and portions where it is lower than the solar one obtains behavior--the details of which cannot be simulated by any single IR band. These details are not of great importance for estimating the maximum temperature or the temperature level in the cloud, such as at the earth's surface, but they are very important for understanding stability properties. The opacity of water-vapor is so high in the ten to twenty percent of the IR band which has the highest opacity and so low in the thirty percent which is lower that we believe there will always be substantial parts of the IR band when the opacity is on either side of the solar. For these reasons amounts of water-vapor which are too small to affect the main character of the temperature profile as calculated in Chapter 3 can be important to the development of the instability. Note that the IR opacity of condensed water is quite constant as a function of frequency so the problem under discussion here must affect the stability calculations of Chapter 3 which were for condensed water.



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